# STUDIES ON WATER MOVEMENTS AND SEDIMENTS IN SOUTHERN LAKE MICHIGAN

Part I. Water-Volume Transports Across the Midlake Sill, and Current Structure Over the Sill

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#### PREFACE TO THE ENTIRE REPORT

Several factors have dictated that this final report should be in separate parts.

The contract covered studies of different sorts. By the nature of the studies, the times required for work-up and analysis of data have varied widely, some parts being completed long before others could be finished. The different studies have required greatly varying amounts of ship-time and some, which required unexpectedly large amounts of ship-time, are being augmented by data obtained during cruises for other projects when vessels are in suitable regions. Finally, it is believed that assimilation by the reader is aided by brevity and unit reporting.

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#### INTRODUCTION

Lake Michigan is divided into northern and southern basins by an area of elevated and irregular bottom that lies in the region between Milwaukee, Wisconsin, and Muskegon, Michigan. While this elevated area is not a complete sill, being cut through by deep water near the Michigan shore and just off Milwaukee, it has sufficiently sill-like characteristics to raise questions as to the effect it may exert on the flushing out of the southern basin.

This study was undertaken to ascertain whether significant volumes of water were being exchanged between the northern and southern basins across the sill. If volume-transport across the sill exists, its magnitude (plus that of river inflows) in comparison to the volume of water in the southern basin should give a clue as to whether the southern basin is well or poorly flushed.

Details about the physical structure of water currents over the sill were not expected, but have come to light.

#### **METHODS**

The basic method of the study was the determination of current direction, current velocity, and water volume transport by the dynamic height method of Ayers (1956) and Ayers and Bachman (1957).

Bathythermograph lowerings at about two-mile intervals (ca 2.5 miles on 10 August 1962) were made underway on courses parallel to the sill and, in all but one case, over the sill.

Navigation was by radar bearing and range out to about 20 miles from the shore being departed, by dead-reckoning in mid-lake, and again by radar from about 20 miles off the shore being approached.

The first BT sounding was in each case from 1/2 mile to 2.5 miles from the shore being departed and the last at two miles, more or less, from the shore being approached.

Vertical temperature profiles were read from the bathythermograph trace, in effect reducing the trace to a series of straight-line segments of various lengths.

Corrected depth and temperature data were fed to an IBM 7090 computer which was programed to make all the necessary computations.

As a check, the section from Racine, Wisconsin, to Grand Haven, Michigan, 9 November 1962 was calculated by hand. Agreement between hand calculation and computer calculation was satisfactory.

Current direction (component normal to ship's course), and velocity were obtained at each 10 decibar level from 0 to 60.

A reference level at 60 decibars was chosen as giving a minimum interference from the bottom.

At the ends of each section, where the bottom was at less than 60 meters, substitution was made from the lower part of the nearest full-depth station according to the method of Helland-Hansen (1934).

Lake Michigan winds at each of the synoptic hours were obtained either 1) from microfilmed copies of ships' weather logs obtained from the National Weather Records Center in Asheville, North Carolina, or 2) from teletype reports transmitted by selected Weather Bureau stations near the lake and received at the station at Willow Run Airport.

Mean ships' winds for each sector (west and east, using the 87th meridian as the dividing line) were obtained and entered as the wind for that sector, whenever ships' observations were available. On some occasions ship observations along the 87th meridian were used as the winds of both sectors.

At times when no ships' observations were available, Weather Bureau observations on land were utilized in the following manner:

In the west sector, the vector mean wind of the following stations was used: Milwaukee (MKE), Glenview, Illinois, (NBU), Joliet (JOT), Midway Airport, Chicago (MDW), O'Hare International Airport, Chicago (ORD), and Meigs Field, Chicago (CGX).

In the east sector, the vector mean wind of the following stations was used: Grand Rapids (GRR), Kalamazoo (AZO), Muskegon (MKG), and South Bend (SBN).

#### RESULTS

Eight transects have been obtained and analysed. In chronological order they are:

- 10 August 1962; Muskegon to Milwaukee
- 20 August 1962; Grand Haven to Milwaukee
- 3 November 1962; Grand Haven to Milwaukee
- 9 November 1962; Racine to Grand Haven
- 17 April 1963; Milwaukee to Grand Haven
- 20 May 1963; Grand Haven to Milwaukee
- 24 June 1963; Grand Haven to Port Washington
- 24 July 1963; Muskegon to Milwaukee

The bathythermograph data of these transects are given in the Appendix.

Tables 1 through 24 present the wind regimens of the days of the transects and of the preceding days; also presented in these tables are the gross volume transports of water across the transects, as well as the net volume transports and the indicated currents involved in the volume transports.

## Volume Transports

Tables 2, 5, 8, 11, 14, 17, 20, and 23 present the gross and net water volume transports of the eight transects. These volumes were computed in terms of cubic meters per second of water moving through each of the 2-mile-by-60-meter blocks (2.5-mile-by-60-meter on 10 August 1962) composing the transect.

Summation of the individual transects gave net volume transport for each transect. Net transports obtained were as

#### follows:

| io vIII 62      |                                  | 47,280 m <sup>3</sup> /sec South |
|-----------------|----------------------------------|----------------------------------|
| 20 VIII 62      | 44,090 m <sup>3</sup> /sec North |                                  |
| 3 XI 62         | 7 <b>,0</b> 75                   |                                  |
| 9 <b>X</b> I 62 | 34,285                           |                                  |
| 17 IV 63        |                                  | 5,016                            |
| 20 V 63         | 5,981                            |                                  |
| 24 VI 63        |                                  | 3,883                            |
| 24 VII 63       | 5,927                            | 1-                               |
|                 | 97,358 North                     | 56,179 South                     |

Grand Net: 41,179 m<sup>3</sup>/sec North

## Indicated Structure of Currents

Tables 3, 6, 9, 12, 15, 18, 21, and 24 present the indicated currents involved in the water transports. These indicated currents were obtained by dividing the net volume transport of each 2-mile-by-10-meter block (2.5-mile-by-10 meter on 10 August 1962) in the 60-meter-deep transect by the area of each 10-meter-deep block.

The original purpose of this step was to provide an approximation of the velocities and directions of 2-to-5-day-average relative currents that might be compared to 2-to-5-day-average currents recorded by the USPH metered buoys installed along the Muskegon to Milwaukee line.

To actually make this comparison is beyond the scope of the contract, and will not be possible until the current data from appropriate levels in the metered buoy systems are read out.

The tables give the possibility of making the comparison if it

should be desired.

The indicated currents varied from zero to tens of centimeters per second. In general the greatest indicated currents occurred in the surface layer and along either the east or west shore of the lake.

In general, the velocities of the indicated currents decreased toward the bottom and in the central portion of the lake.

## Streaked Nature of the Indicated Currents

Quite unexpected was the fact that the indicated currents were arranged in alternate streaks of northward and southward current.

The widths of the alternating current streaks varied, apparently in response to the wind regimen. The locations of the streaks also appeared to vary under different winds.

The streaks of current in most cases reached to the 60-meter level, although there were some instances where they did not.

The indicated structure of the currents is similar to the horizontal current-countercurrent arrangement suggested by Fuglister (1951, 1955) for the Gulf Stream, and confirmed by von Arx, Bumpus, and Richardson (1955). Fuglister's initial presentation of this current arrangement is shown in Figure 1.

The alternation of northward and southward current bands shows clearly in the underlined (north) and not underlined (south) indicated currents of Tables 3, 6, 9, 12, 15, 18, 21, and 24.

As a direct test of the reality of the bands or streaks of

indicated current, ten current drogues were set in a line past USPHS buoy #20 off Muskegon, Michigan, on 29 October 1963. The series of drogues began at the U. S. Weather Bureau-U. S. Public Health Service-University of Michigan weather tower one mile off the beach, continued at 2-mile intervals along a course to the south of west, passed about three-quarters of a mile north of USPHS buoy #20, and ended about six miles west of buoy #20.

These drogues were set in the period between 0911 and 1050 EDT under north wind which continued until after the period of drogue runs. The drogue movements that took place in 3-3/4 to 5 hours are shown in Figure 2.

All of the drogues, except the one immediately east of buoy #20, moved southward. Drogue #8, immediately east of the buoy, moved northward, almost directly upwind.

All the drogues were set to be influenced by the upper five feet of the water (surface drogues).

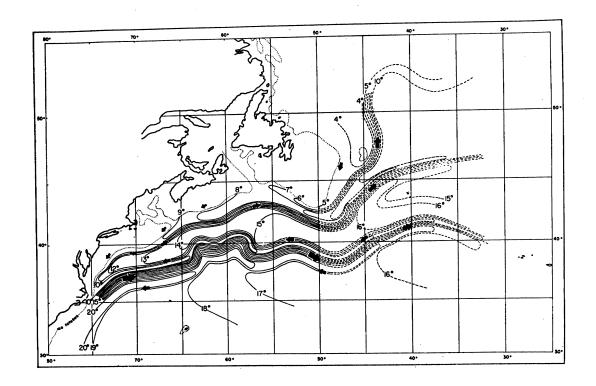


Fig. 1. Schematic chart of temperatures (°C.) at a depth of 200 meters in the Gulf Stream Area.

#### DISCUSSION

## Drogue Sets of 29 October

Care must be taken to use this drogue study for no more than it is valid for. To command this number of drogues it was necessary to use some drogue floats that were known to be somewhat effected by wind. These were the floats of drogues 1 through 5. To contribute toward an assessment of the effect of windage on these floats, they were set alternately with low-riding low-windage floats (numbers 6 through 10).

Drogues 3 and 4 moved southward 0.75 and 0.4 miles in 4 hrs 22 min and 4 hrs 33 min, all respectively. At the time of writing the author is inclined to attribute the 0.4 mile movement of drogue 4 entirely to windage on its float. Perhaps readout of the data from the 30-foot current meter of buoy #20 for the period 1017 through 1450 will enable a better assessment of the movement of drogue 4.

Drogue 8 was carried by a low-windage float, and cannot be denied.

Drogues 6, 7, 8, 9, and 10 were all carried by low-windage floats. They tell the essential story of the results, while drogues 1 through 5 augment the story with detail containing an incompletely-assessed windage error.

Current velocities indicted by the low-windage drogues were:

| <b>#</b> 6 | 0.4 mph southward  |
|------------|--------------------|
| <b>#</b> 7 | 0.4 mph southward  |
| #8         | 0.07 mph northward |
| <b>#</b> 9 | 0.13 mph southward |

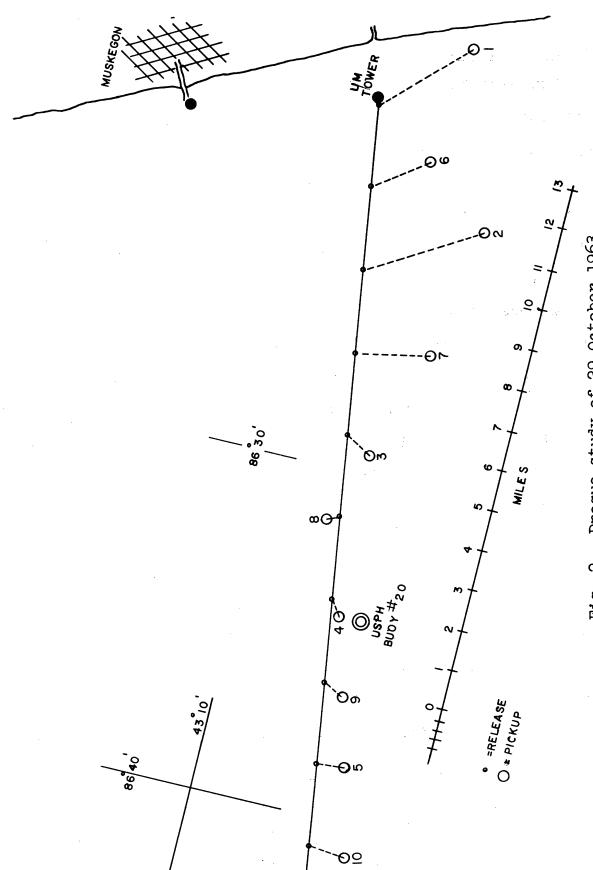


Fig. 2. Drogue study of 29 October 1963.

## #10 0.18 mph southward

The drogue experiment of 29 October contributes to a degree of faith in the reality of the streaked current structure that was indicted by the computed currents.

## Indirect Evidence for Current Streaks

Drift bottles released along the Racine to Grand Haven transect by the then U. S. Bureau of Fisheries on 17 July 1931 showed (Figure 3) an alternation of recoveries from north and south of the line of releases. This is at least compatible with the idea that initial bottle movements governed by current streaks may have determined the ultimate northward or southward location of recovery points. These studies are reported by Van Oosten (1963).

Johnson (1960) reported on multiple drift bottle releases at stations along the Grand Haven-Milwaukee line during July, August and September of 1954. His results are summarized in Figure 4. Varying degrees of alternation between northern and southern (and vice versa) recovery points are shown. In numerous instances bottles from a single release point had both northern and southern recoveries, as though these releases might have been at the interface between oppositely-flowing current streaks.

Both of the above reports show evidences of alternation in north and south recovery points in the southern basin of Lake Michigan. North of Frankfort, Michigan, these evidences become less abundant but do not disappear.

The meaning of the streaked current structure is at present not known.

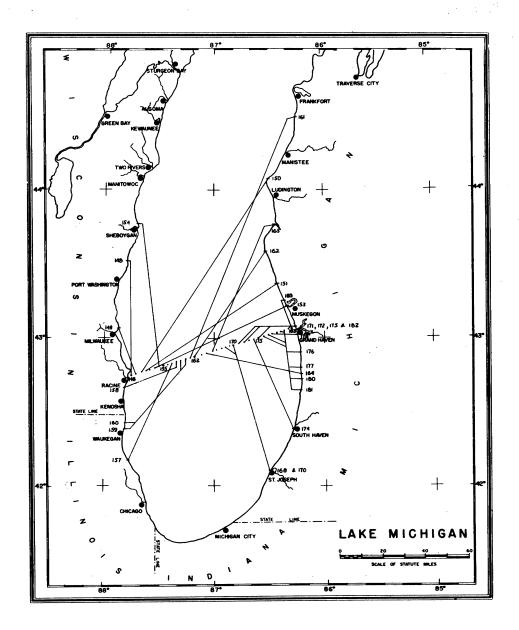


Fig. 3. Movements of bottles released along the transect, Racine to Grand Haven, July 17, 1931,

## Volume Transport and Flushing Time

Although the dynamic height method of determining volume transport is still subject to some unanswered questions, it remains to date the fastest and most feasible means of obtaining such information where distances are great and/or where relative wealth of indicative detail is needed.

Perhaps the best assessment is still that of Sverdrup,

Johnson and Fleming (1942, p. 394): "So many reservations have
been made that it may appear as if the computed currents have
little or no relation to the actual currents. Fortunately,
however, most of the assumptions made lead only to minor errors,
and currents can be correctly represented in the first approximation by means of the slopes of a series of isobaric surfaces
relative to one reference surface."

To take the present volume transport results as first approximations is apparently within the validity of the method.

It is certainly compatible with the intent with which these preliminary investigations are presented.

Even as first approximations, the present results allow us to take an initial step toward a more realistic determination of the flushing time of the southern basin of Lake Michigan.

Large volumes of water cross the mid-lake sill, both into and out of the southern basin. Water crossing the sill and entering the southern basin joins with the inflows from the rivers tributary to the southern basin in replacing the volume of water that is contained in the basin at a given instant. Continuity requires that the combined inflows be countermatched

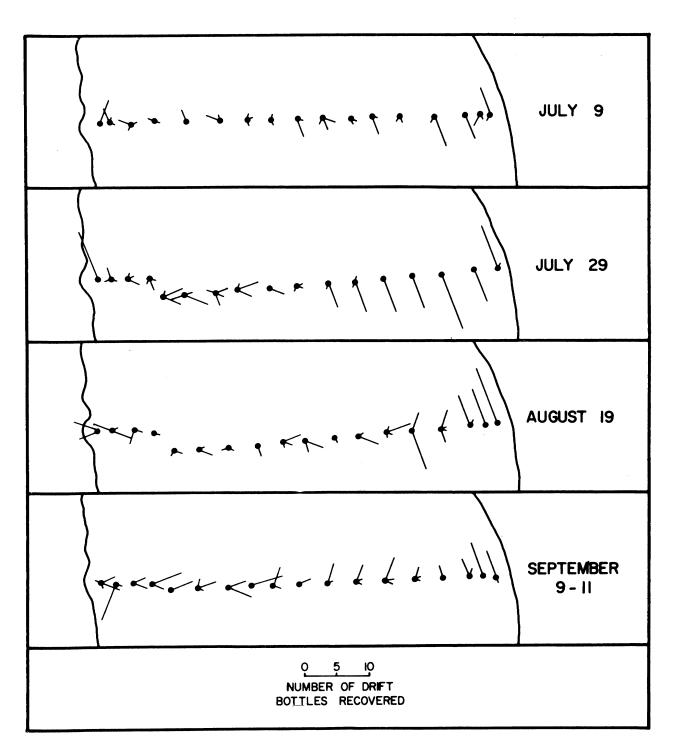


Fig. 4. Release stations, numbers recovered, and directions of recovery points of drift bottles that were released in 1954 on the Grand Haven-Milwaukee transect. For the transect in September bottles were released at the two easternmost stations on September 9 and the remaining stations on September 11.

by equal-volume net outflow from the southern basin. At present it is not known whether the compensatory outflow is subsurface and through the deep-water channels along the Michigan and Wisconsin shores, or whether it ocurrs as a counter-oscillation of the surface layers after release of set-up along shore, or as a combination of the two.

Water crossing the sill from southern basin to northern basin constitutes a direct subtraction from the volume content of the southern basin. In this case a compensatory net inflow is required, though its location and nature cannot be specified at present. The compensatory inflow, plus inflow from the rivers, works to replace a given instant's volume content of the southern basin.

It appears at present that the functional mechanism for the flushing of the southern basin is a combination of the addition of river inflows and a large-volume net transport over the sill.

From about May to about January, winds at Chicago, Muskegon and Milwaukee are dominantly from the south of west; in the rest of the months winds are chiefly from the north of west (U. S. Weather Bureau Tech. Paper 35, 1959, figs 8 through 19). These wind regimes may be expected to induce a northward net transport over the sill during summer and fall, and a net southward transport over the sill in mid-winter and spring.

The net transports over the sill should be accompanied in summer and fall by net southward compensatory counter-movement. In winter and spring the reverse condition should prevail.

Inflows entering a lake basin encounter several turbulent

mixing mechanisms among which waves, currents, and internal waves appear to be dominant, and to which are added local or periodic sinkings, upwellings, surface seiches, and periods of overturning. As a result of these turbulent phenomena inflowing waters more or less quickly lose their identity by being mixed into the receiving water.

Outflow sites are generally at distance from sites of inflow. In general, outflowing waters consist of more or less homogeneous mixtures of inflow and receiving water. Outflows balance the volume-content budget of a lake or basin. It is done, however, by removing compensatory volumes of "mixed" waters, not of "pure" receiving water.

Because influent waters become mixed with the receiving water, and because outflows are of mixed water, the flushing-out of the water that fills a lake or basin at a given instant is an exponential "die-away" process in which the rate of removal of original water at any time after the given instant is dependent upon the proportion of the original water mass that is still present.

The U. S. Geological Survey Water Supply Papers give the mean annual runoff of the rivers tributary to the lower basin of Lake Michigan as  $4.2 \times 10^{11}$  cubic feet, or about 14,000 cubic feet per second through the year.

Maximum net transport over the sill into the southern basin of the lake, in this study, is about  $47,000 \text{ m}^3/\text{sec}$  or  $1.65 \times 10^6$  cfs.

The sum of river and over-the-sill inflows under these

conditions is about  $1.7 \times 10^6$  cfs which, divided into the 460 x  $10^{11}$ cubic foot volume of the southern basin, gives  $271 \times 10^5$  seconds or 314 days to bring in a volume of water equal to the volume of the southern basin.

Continuity would require under these conditions that 1/314th of the basin volume be discharged from the basin per day, an exchange ratio of 0.0032 per day. This maximum exchange ratio is used in the "die-away" equation

$$V_{t} = V_{o}e^{-.0032x}$$

where the subscripts o and t mean "original" and "at time" and  $\mathbf{x}$  is number of days.

Considering flushing-out to be complete when 99% of the original basin water-content has been removed gives

$$V_t/V_o = 0.01 = e^{-.0032x}$$
  
ln 0.01 = -.0032x  
-4.60517 = -.0032x  
 $x = 1439$  days or 3.9 years

Minimum net transport over the sill, found in this study, was  $3,800 \text{ m}^3/\text{sec}$  or  $0.13 \times 10^6 \text{ cfs}$ . Combined with river inputs this gives  $0.14 \times 10^6 \text{ cfs}$  total input. Dividing the basin volume by total input gives  $3286 \times 10^5 \text{ seconds}$  or 3803 days to supply a volume of water equal to the basin content.

Volume-content balance requires under these conditions, the discharge of 1/3803th of basin volume per day or an exchange ratio of 0.00026 per day. With this minimum exchange ratio the die-away equation gives

$$v_t/v_o = 0.01 = e^{-.00026x}$$

 $ln \ 0.01 = -.00026x$ 

x = 17,712 days or 48.5 years

to flush out 99% of the southern basin volume.

Taking these two values as indicative of minimum and maximum flushing times, we may indicate a mean first approximation flushing time for the southern basin of Lake Michigan as being of the order of 26 years.

### Comparison to Solute Accumulations

With regard to flushing characteristics three major types of water bodies may be recognized. One, typified by Great Salt Lake which has no outlet, may be called "basins of almost total accumulation." A second, typified by the usual river or stream, may be called "basins of almost no accumulations." The third, typified by the usual lake with an outlet and inlet(s), may be called "basins of partial accumulation."

Each basin is considered to lose some of the solutes contributed to it by 1) incorporation of solutes in its sediments and by 2) incorporation of solutes into biological products completely removed by man or predators.

In basins of almost total accumulation the sum of solutes present, plus those lost by the two means indicated, is about the total that has been contributed, and flushing time approaches infinity.

In basins of almost no accumulation (streams) the watervolume and solute contents of the basin (bed) are essentially equaled by those of the influent coming in in the next unit of time and flushing time is close to one.

Basins of partial accumulation receive solutes via influent waters and discharge solutes via their effluents. Solute concentrations in the influent and effluent waters are usually different, and the concentrations of solutes observed in the basin waters is a reflection of

influx - (losses + efflux).

Since rates of loss to sediments and by removed biological products are relatively small, the concentration of solutes in a basin compared to the rate of their influx is a rough measure of the basin's effective accumulation-time.

Accumulation-time is also the effective number of time units that a given time-unit's contribution of solutes might be expected to remain in the basin.

Flushing time is the number of time-units that are necessary to remove a given instant's volume-content and its solutes from a basin.

The two concepts are essentially two views of the same process and computed times based on the two concepts are essentially comparable.

Unpublished results of USPHS Grant WP-00226-03 provide some accumulation-time estimates for comparison. From studies of solute concentrations in the southern basin of Lake Michigan and from the volume of the basin, the quantities of some solutes contained in the basin's water have been computed.

From studies of the solute concentrations in rivers tributary to the southern basin the annual contributions of

solutes to the basin have been computed.

For each of the solutes considered, the accumulation-time has been computed by

Pounds of solute in basin water
Pounds of solute contributed by rivers yearly = Accumulation time

The accumulation times available to be compared to the computed flushing times are:

Chloride 29 years

Sulfate 38 years

Phosphorus 6 years

If these are treated as first approximations, as were the flushing times, we may take the mean of the maximum and minimum values as a mean first approximation to compare with the mean first approximation flushing time.

Mean 1st approx. flushing time 26 years

Mean 1st approx. accumulation time 22 years

The agreement is good, though both types of results need to be refined by further repetitions.

As an initial working hypothesis we must consider Lake Michigan's southern basin to be flushed out only four times per century.

#### SUMMARY

This report is the first of a series which altogether comprise the final report on work done under the contract.

The primary goals of this section were the determination of volumes of water transported across the central sill of Lake Michigan and the effect of these water volumes on the flushing out of the lake's southern basin.

Large volumes of water were found to be crossing the sill in the period April through November. Maximum volume transports found were  $44,000 \text{ m}^3/\text{sec}$  northward and  $47,000 \text{ m}^3/\text{sec}$  southward. Minimum transports were  $5,900 \text{ m}^3/\text{sec}$  northward and  $3,900 \text{ m}^3/\text{sec}$  southward.

Volume transports across the sill are controlled by wind.

Volume transports across the sill are from 10 to 100 times the inflow via rivers, and constitute the primary means of flushing out the southern basin.

Computed flushing times of the southern basin, and computed solute-accumulations in the southern basin, both indicate that about 25 years must be taken as the first approximation of the flushing time of the southern basin.

Wind-induced currents involved in the volume transports across the sill occur in alternate streaks of northward and southward current. The meaning of the streaked nature of these currents is not yet known.

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Table 1 Lake Michigan Winds on Day of Transect and Preceding Days.

# Transect of 10 August 1962

|                             | 0000                                      | GMT                            | 060  | OGMT                          | 120  | OGMT                         | 1800GMT  |                              |
|-----------------------------|---|--------------------------------|--|-------------------------------|--|------------------------------|--|------------------------------|
| Date                        | Wind<br>from                              | Speed<br>knots                 | Wind<br>from                                       | Speed<br>knots                | Wind<br>from                                       | Speed<br>knots               | Wind<br>from                                       | Speed<br>knots               |
| August                      | 1962                                      |                                |  |                               |  |                              |  |                              |
|                             |   |                                |  | East Sec                      | ctor   |                              |  | •                            |
| 5<br>6<br>7<br>8<br>9<br>10 | *080°<br>*060°<br>*320°<br>*340°<br>*050° | 4<br>2<br>8<br>12<br>10        | *350°<br>*120°<br>*290°<br>*260°<br>'050°<br>*070° | 4<br>7<br>1<br>2<br>24<br>6   | *040°<br>*110°<br>*190°<br>'270°<br>*020°<br>*070° | 26<br>14<br>94               | *160°<br>*050°<br>'260°<br>*290°<br>*060°<br>*080° | 2<br>5<br>13<br>12<br>10     |
|                             |   |                                |  | West Sec                      | etor   |                              |  |                              |
| 56<br>7<br>8<br>9           | '010° '110° '160° '060° '030° *040°       | 15<br>7<br>10<br>6<br>28<br>12 | '180°<br>'090°<br>'230°<br>'260°<br>'020°<br>*340° | 2<br>14<br>10<br>9<br>28<br>2 | *050°<br>*120°<br>'260°<br>'270°<br>*040°<br>*140° | 4<br>12<br>13<br>4<br>8<br>2 | *090° '150° '220° *300° *090°                      | 5<br>10<br>6<br>8<br>13<br>8 |

<sup>&#</sup>x27; Ship Weather Reports \* Weather Bureau land-station data, when ship reports not available

10 August 1962

Water-Volume Transports in the 2.5-mile x 60-meter Blocks,  $\mathrm{m}^3/\mathrm{sec}$ 

| Block | North Transport | South Transport | Net Transport |
|-------|-----------------|-----------------|---------------|
| 1     | 2194            | 0               | 2194 North    |
| 2     | 2149            | 0               | 2149 North    |
| 3     | 280             | 1821            | 1541 South    |
| 4     | 0               | 6168            | 6168 South    |
| 5     | 110             | 5054            | 4944 South    |
| 6     | 0               | 12533           | 12533 South   |
| 7     | 0               | 4971            | 4971 South    |
| 8     | 4241            | 33              | 4208 North    |
| 9     | 2614            | 11              | 2603 North    |
| 10    | 70              | 3330            | 3260 South    |
| 11    | 8030            | 20              | 8010 North    |
| 12    | 2075            | 0               | 2075 North    |
| 13    | 6               | 3277            | 3271 South    |
| 14    | 56              | 1028            | 972 South     |
| 15    | 8761            | 0               | 8761 North    |
| 16    | 1643            | 0               | 1643 North    |
| 17    | 53              | 125             | 72 South      |
| 18    | 0               | 5245            | 5245 South    |
| 19    | 0               | 2139            | 2139 South    |
| 20    | 3460            | 104             | 3356 North    |
| 21    | 71              | 1688            | 1617 South    |
| 22    | 6604            | 0               | 6604 Morth    |
| 23    | 543             | 0               | 543 North     |
| 24    | 2390            | 287             | 2103 Morth    |
| 25    | 465             | 773             | 308 South     |
| 26    | 0 0 0           | 4433            | 4433 South    |
| 27    |                 | 937             | 937 South     |
| 28    |                 | 12037           | 12037 South   |
| 29    |                 | 18615           | 18615 South   |
| 30    |                 | 7212            | 7212 South    |
| 31    | 0               | 1254            | 1254 South    |
|       | 45815           | 93095           | 47280 South   |

Table 3

Muskegon - Milwaukee

10 August 1962

Mean Velocities in Each of the 2.5-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                      | 0-10m                                      | 10-20m                                    | 20-30m                                     | 30-40m                                       | 40-50m  | 50-60m  |
|----------------------------|--|---|--|--|---|---|
| 1<br>2<br>3<br>4<br>5      | .0548<br>.026N<br>.039S<br>.255S<br>.050S  | 0<br>.023N<br>.006S<br>.138S<br>.050S     | 0<br>.003N<br>.004N<br>.010S<br>.020S      | 0<br>0<br>.003N<br>.002S<br>.001N            | 0<br>0<br>0<br>.0015S<br>.001N                  | 0<br>0<br>0<br>.0002S<br>.0004N               |
| 6<br>7<br>8<br>9<br>10     | .0728<br>.0578<br>.031N<br>.024N<br>.0358  | .070S<br>.047S<br>.044N<br>.027N          | .041S<br>.019S<br>.028N<br>.014N           | .006s<br>.0007s<br>.003N<br>.00006s<br>.001N | .00058<br>.00078<br>.00068<br>.00028<br>.0005N  | .00003S<br>.0003S<br>.0003S<br>.00001S        |
| 11<br>12<br>13<br>14<br>15 | .086N<br>.009N<br>.017S<br>.001S<br>.097N  | .079N<br>.024N<br>.039S<br>.014S<br>.083N | .035N<br>.017N<br>.025S<br>.010S<br>.037N  | .0003S<br>.001N<br>.0006S<br>.001N           | .0002S<br>.0006N<br>.0001N<br>.0003N            | .00003S<br>.0001N<br>.00006N<br>.00001N       |
| 16<br>17<br>18<br>19<br>20 | .020N<br>.0003S<br>.076S<br>.020S<br>.050N | .016N<br>.001S<br>.044S<br>.018S<br>.030N | .003N<br>.0009S<br>.011S<br>.012S<br>.006N | .0007N<br>.001S<br>.0007S<br>.003S<br>.002S  | .0008N<br>.0006S<br>.00007S<br>.0005S<br>.0008S | .0003N<br>.0002S<br>0<br>.00003S<br>.0002S    |
| 21<br>22<br>23<br>24<br>25 | .0198<br>.079N<br>.001N<br>.037N<br>.016S  | .018s<br>.059N<br>.002N<br>.023N<br>.003S | .0058<br>.023N<br>.006N<br>.0002S<br>.004N | .002N<br>.003N<br>.002N<br>.003S<br>.004N    | .0003N<br>.0006N<br>.002N<br>.003S<br>.003N     | .0002S<br>.0002N<br>.0006N<br>.0009S<br>.001N |
| 26<br>27<br>28<br>29<br>30 | .062S<br>.011S<br>.137S<br>.222S<br>.101S  | .036s<br>.007s<br>.116s<br>.168s<br>.079s | .008s<br>.002s<br>.047s<br>.073s           | .004s<br>.002s<br>.001s<br>.003s             | .001S<br>.001S<br>.00006S<br>0                  | .0003S<br>.0005S<br>.00009S<br>0              |
| 31                         | .0318                                      | 0   | 0  | 0  | 0   | 0   |

ake Michigan Winds on Day of Transect and Preceding Days.

Transect of 20 August 1962

Table 4

|  | 000  | OGMT   | 060  | OGMT                                   | 120   | OGMT   | 18  | OOGMT    |
|--|--|--|--|--|---|--|---|----------|
| ate  | Wind<br>from   | Speed<br>knots                                       | Wind<br>from   | Speed<br>knots                         | Wind<br>from  | Speed<br>knots                                       | Wind<br>from  | Sp<br>kn |
| ugu  | ıst 1962   |  |  |  |   |  |   |          |
|  |  |  |  | East Sec                               | ctor  |  |   |          |
| 11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20 | *050°<br>*190°<br>'270°<br>'340°<br>*340°<br>*240°<br>*310°<br>*320°<br>*260°          | 4<br>8<br>17<br>30<br>10<br>8<br>9<br>7<br>4<br>3    | *100°<br>*160°<br>'330°<br>*360°<br>'150°<br>*210°<br>'060°<br>*090°<br>'120°<br>*230° | 2<br>7<br>22<br>8<br>6<br>9<br>13<br>1 | *150° '200° *300° '020° *170° '250° *070° '170° *260° | 2<br>17<br>9<br>19<br>3<br>8<br>4<br>5<br>17<br>12   | *180° *210° *340° *210° *280° *230° *210° *280°       |          |
|  |  |  |  | West Se                                | ctor  |  |   |          |
| 11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>19<br>20 | *090°<br>*170°<br>'280°<br>'340°<br>*050°<br>*170°<br>*040°<br>'180°<br>'090°<br>'200° | 6<br>11<br>16<br>30<br>5<br>7<br>6<br>13<br>14<br>10 | *080°<br>*180°<br>'300°<br>*010°<br>'150°<br>'200°<br>*340°<br>'300°<br>'160°<br>*230° | 1<br>92<br>8<br>6<br>17<br>26<br>18    | *170° '200° '290° '020° *220° '140° '280° '170° '310° | 4<br>14<br>16<br>19<br>2<br>8<br>12<br>5<br>17<br>13 | *160° '190° '340° *020° *210° *070° '290° '210° '080° |          |

<sup>&#</sup>x27; Ship Weather Reports
\* Weather Bureau land-station data, when ship reports not available

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $\rm m^3/\rm sec.$ 

| Block            | North Transport            | South Transport                   | Net Transport  |
|------------------|----------------------------|-----------------------------------|--|
| 1                | 7118                       | 0                                 | 7118 North   |
| 2                | 22218                      | 0                                 | 22218 North  |
| 3                | 3263                       | 0                                 | 3263 North   |
| 4                | 3372                       | 156                               | 3216 North   |
| 5                | 7532                       | 0                                 | 7532 North   |
| 6<br>7<br>8<br>9 | 0<br>137<br>0<br>0<br>3705 | 3552<br>3087<br>9444<br>7266<br>8 | 3552 South<br>2950 South<br>9444 South<br>7266 South<br>3697 North |
| 11               | 11                         | 1379                              | 1368 South   |
| 12               | 0                          | 3860                              | 3860 South   |
| 13               | 0                          | 5169                              | 5169 South   |
| 14               | 4896                       | 5                                 | 4891 North   |
| 15               | 140                        | 379                               | 239 South  |
| 16               | 0                          | 4704                              | 4704 South   |
| 17               | 4143                       | 48                                | 4095 North   |
| 18               | 0                          | 2080                              | 2080 South   |
| 19               | 1022                       | 0                                 | 1022 North   |
| 20               | 0                          | 913                               | 913 South  |
| 21               | 53                         | 391 <sup>4</sup>                  | 3861 South   |
| 22               | 0                          | 5386                              | 5386 South   |
| 23               | 6835                       | 0                                 | 6835 North   |
| 24               | 8419                       | 0                                 | 8419 North   |
| 25               | 5379                       | 0                                 | 5379 North   |
| 26               | 4307                       | 218                               | 4089 North 650 North 1630 South 1945 South 3893 South              |
| 27               | 650                        | 0                                 |  |
| 28               | 18                         | 1648                              |  |
| 29               | 0                          | 1945                              |  |
| 30               | 202                        | 4095                              |  |
| 31               | 2738                       | 33                                | 2705 North   |
| 32               | 5142                       | 0                                 | 5142 North   |
| 33               | 2606                       | 135                               | 2471 North   |
| 34               | 36                         | 1381                              | 1345 South   |
| 35               | 54                         | 703                               | 649 South  |
| 36               | 2                          | 2833                              | 2831 South   |
| 37               | 6531                       | 0                                 | 6531 North   |
| 38               | 4670                       | 0                                 | 4670 North   |
| 39               | 3232                       | 0                                 | 3232 North   |
|                  | 108431                     | 64341                             | 44090 North  |

Table 6

#### Grand Haven - Milwaukee

20 August 1962

Mean Velocities in Each of the 2-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                          | 0-10m                           | 10-20m                                  | 20-30m                          | 30-40m   | 40-50m   | 50-60m                      |
|--------------------------------|---------------------------------|---|---------------------------------|--|--|-----------------------------|
| 1<br>2<br><b>3</b><br>4        | .129N<br>.282N<br>.023N         | .092N<br>.234N<br>.043N                 | 0<br>.135N<br>.028N             | 0<br>.039N<br>.005N                                | .002N<br>0   | 0                           |
| <b>4</b><br>5                  | .072N<br>.111N                  | .033 <b>N</b><br>.089 <b>N</b>          | .0058<br>.033N                  | .00008s<br>.0009N                                  | .0003s<br>.0003N                                   | 0                           |
| 6<br>7<br>8                    | .070 <b>s</b><br>.065 <b>s</b>  | .036 <b>s</b><br>.031s                  | .003S                           | .001S  | .00058<br>.0005N                                   | 0<br>.0002N                 |
| 8<br>9<br>10                   | .152 <b>S</b><br>.103S<br>.054N | .107 <b>S</b><br>.084 <b>S</b><br>.043N | .0345<br>.037 <b>5</b><br>.018N | .001S<br>.002S<br>.0005N                           | 0<br>0<br>.0002S                                   | 0<br>0<br>.0 <b>001S</b>    |
| 11<br>12                       | .017S                           | .0178<br>.046 <b>S</b>                  | .0098                           | .00028   | .0003N   | .0001N                      |
| 13<br>14                       | .0758<br>.068N                  | .061 <b>S</b><br>.059N                  | .024s<br>.026n                  | .0000058<br>.00028                                 | .00048   | .0002S                      |
| 15                             | 70038                           | .006S                                   | .0038                           | .003N  | .001N  | .0003N                      |
| 16<br>17<br>18                 | .0658<br>.059N<br>.0298         | .0568<br>.050N<br>.0248                 | .025S<br>.021N<br>.0115         | .0008 <b>s</b><br>.0006 <b>s</b><br>.0009 <b>s</b> | .000 <b>23</b><br>.0007 <b>S</b><br>.0005 <b>S</b> | .00001N<br>.0003S<br>.0002S |
| 19<br>20                       | .019N<br>.018S                  | .010N<br>.007S                          | .0007N<br>.001S                 | .001N<br>.001S                                     | .0005N<br>.0008S                                   | .0002S                      |
| 21<br>22                       | .054 <b>s</b><br>.08 <b>os</b>  | .0478<br>.0568                          | .022S                           | .0006N   | .0009N   | .0002N                      |
| 23<br>24                       | .089N                           | .080N<br>.103N                          | .040N<br>.046N                  | .003n<br>.0006n                                    | .0009N<br>.00008N                                  | .0003N                      |
| 25<br>26                       | .074N                           | .057N<br>.048N                          | .028N                           | .005N  | .003N  | .0008N                      |
| 27<br>28                       | .073N<br>.005N<br>.019S         | .009N<br>.021S                          | .013N<br>.004N<br>.011S         | .004S<br>.001N<br>.0001S                           | .0028<br>.0009N<br>.0004N                          | .00098<br>.0004N<br>.0002N  |
| 29<br>30                       | .0298<br>.0608                  | .021S<br>.048S                          | .0078<br>.01 <b>9</b> 8         | .001S<br>.003N                                     | .001S<br>.003N                                     | .00048<br>.0009N            |
| 31<br>32                       | .029N                           | .036N<br>.056S                          | .020N                           | .0003 <b>s</b><br>.002S                            | .00078   | .0001S                      |
| 33<br><b>3</b> 4               | .048N<br>.015 <b>S</b>          | .030N                                   | .003N<br>.007S                  | .0048  | .00005N  | .0002N                      |
| <b>3</b> 5                     | .0108                           | .009\$                                  | .0025                           | .002N  | 0  | 0                           |
| <b>3</b> 6<br><b>3</b> 7<br>38 | .0548<br>.081N<br>.086N         | .027S<br>.082N<br>.060N                 | .007S<br>.041N                  | .00009N<br>0<br>0                                  | 0  | 0<br>0<br>0                 |
| <b>3</b> 9                     | .067N                           | .033N                                   | ŏ                               | ŏ  | ŏ  | 0                           |

Table 7 ake Michigan Winds on Day of Transect and Preceding Days. Transect of 3 November 1962

|                          | 0000                                      | GMT                      | 060  | 0600GMT 1200GMT 1800            |  | OOGMT                           |  |             |
|--------------------------|---|--------------------------|--|---------------------------------|--|---------------------------------|--|-------------|
| ite                      | Wind<br>from                              | Speed<br>knots           | Wind<br>from                                       | Speed<br>knots                  | Wind<br>from                                       | Speed<br>knots                  | Wind<br>from                                       | Spe<br>kno  |
| tobe                     | er - Nove                                 | mber 1962                | 2  |                                 |  |                                 |  | 19          |
|                          |   |                          |  | East Se                         | ctor   |                                 |  | 0           |
| 39<br>30<br>31<br>1<br>2 | *220°<br>'330°<br>'330°<br>*350°<br>*090° | 21<br>7<br>7<br>9<br>16  | *040°<br>*230°<br>*350°<br>*340°<br>*020°          | 19<br>23<br>24<br>16<br>12      | '090°<br>*330°<br>*350°<br>'<br>*210°<br>*070°     | 3<br>22<br>28<br><br>8<br>18    | '220°<br>'340°<br>*330°<br>*350°<br>*070°<br>*050° | 1 2 1       |
|                          |   |                          |  | West Sec                        | etor   |                                 |  |             |
| 29<br>30<br>31<br>1<br>2 | *220°<br>*360°<br>'350°<br>*350°<br>*090° | 21<br>16<br>9<br>9<br>16 | *020°<br>*230°<br>*350°<br>*340°<br>*110°<br>*090° | 18<br>23<br>24<br>19<br>4<br>17 | *070°<br>*310°<br>*010°<br>*300°<br>*060°<br>*080° | 6<br>26<br>28<br>12<br>09<br>11 | *210°<br>*350°<br>*330°<br>*350°<br>*230°<br>*030° | 1<br>2<br>2 |

<sup>&#</sup>x27; Ship Weather Reports
\* Weather Bureau land-station data, when ship reports not available

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/\text{sec}$ .

| Block                      | North Transport                   | South Transport                           | Net Transport   |
|----------------------------|-----------------------------------|---|---|
| 1 2 3 4 5                  | 0<br>1394<br>24244<br>13207<br>0  | 712<br>0<br>0<br>10<br>31 <sup>4</sup> 7  | 712 South 1394 North 24244 North 13197 North 3147 South             |
| 6<br>7<br>8<br>9<br>10     | 7213<br>0<br>6483<br>5829<br>0    | 41<br>6312<br>0<br>21<br>6258             | 7172 North<br>6312 South<br>6483 North<br>5808 North<br>6258 South  |
| 11<br>12<br>13<br>14<br>15 | 35<br>0<br>2540<br>2871<br>13499  | 1302<br>7168<br>227<br>0                  | 1267 South<br>7168 South<br>2313 North<br>2871 North<br>13499 North |
| 16<br>17<br>18<br>19<br>20 | 20<br>1873<br>1177<br>6391<br>734 | 7443<br>0<br>481<br>0<br>5                | 7423 South<br>1873 North<br>596 North<br>6391 North<br>729 North    |
| 21<br>22<br>23<br>24<br>25 | 0<br>4637<br>31<br>322<br>5953    | 9 <b>22</b> 1<br>0<br>622<br>1338<br>0    | 9221 South<br>4637 North<br>591 South<br>1016 South<br>5953 North   |
| 26<br>27<br>28<br>29<br>30 | 0<br>0<br>196<br>0<br>0           | 9275<br>7392<br>627<br>1780<br>4087       | 9275 South<br>7392 South<br>431 South<br>1780 South<br>4087 South   |
| 31<br>32<br>33<br>34<br>35 | 0<br>4562<br>0<br>0               | 11493<br>0<br>4995<br><b>6045</b><br>8126 | 11493 South<br>4562 North<br>4995 South<br>6045 South<br>8126 South |
| 36<br>37<br>38<br>39       | 0<br>0<br>1229<br>2289            | 330<br>1196<br>0                          | 330 South<br>1196 South<br>1229 North<br>2289 North                 |
|                            | 1067 <del>2</del> 9               | 99654                                     | 7075 North  |

Grand Haven - Milwaukee

3 November 1962

Mean Velocities in Each of the 2-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block<br>1<br>2<br>3<br>4<br>5 | 0-10m<br>.022S<br>.020N<br>.195N<br>.100N | 0<br>.012N<br>.175N<br>.103N<br>.028S     | 0<br>.007N<br>.151N<br>.105N              | 30-40m<br>0<br>.004N<br>.126N<br>.078N    | 0<br>0<br>0<br>.081N<br>.025N             | 50-60m<br>0<br>0<br>.024N<br>.003s<br>.001s |
|--------------------------------|---|---|---|---|---|---|
| 6<br>7<br>8<br>9               | .074N<br>.0488<br>.085N<br>.090N<br>.0658 | .071N<br>.055S<br>.067N<br>.051N          | .057N<br>.053S<br>.035N<br>.021N<br>.040S | .021N<br>.040S<br>.015N<br>.013N<br>.023S | .001S<br>0<br>0<br>.006N                  | .001N<br>0<br>0<br>.001S<br>.001S           |
| 11<br>12<br>13<br>14<br>15     | .0068<br>.0448<br>.034N<br>.014N<br>.126N | .012S<br>.044S<br>.024N<br>.020N<br>.112N | .0148<br>.0448<br>.015N<br>.025N          | .008s<br>.046s<br>.006N<br>.018N          | 0<br>.0348<br>.0038<br>.008N              | .001N<br>.009S<br>.004S<br>.004N            |
| 16<br>17<br>18<br>19<br>20     | .0698<br>.025N<br>.0128<br>.059N<br>.002N | .0658<br>.015N<br>.0038<br>.056N          | .056s<br>.010N<br>.006N<br>.050N<br>.009N | .034S<br>.006N<br>.016N<br>.028N<br>.006N | .008s<br>.001N<br>.013N<br>.005N          | .001N<br>0<br>.002N<br>0                    |
| 21<br>22<br>23<br>24<br>25     | .066s<br>.035N<br>.011s<br>.008N<br>.046N | .071S<br>.035N<br>.006S<br>.002N          | .076s<br>.033N<br>.002s<br>.008s<br>.042N | .056s<br>.029N<br>0<br>.019s<br>.038N     | .018s<br>.013N<br>0<br>.013s<br>.017N     | .001S<br>0<br>0<br>.001S<br>.001N           |
| 26<br>27<br>28<br>29<br>30     | .0778<br>.0608<br>.0088<br>.0058<br>.0198 | .0738<br>.0528<br>.0078<br>.0088<br>.0198 | .069S<br>.047S<br>.005S<br>.011S<br>.022S | .050S<br>.043S<br>.001N<br>.016S<br>.026S | .018s<br>.028s<br>.005N<br>.016s<br>.028s | .001S<br>0<br>0<br>0<br>0<br>.013S          |
| 31<br>32<br>33<br>34<br>35     | .108S<br>.002N<br>.015S<br>.037S<br>.069S | .0918<br>.016N<br>.0228<br>.0368<br>.0638 | .0718<br>.028N<br>.0298<br>.0358<br>.0558 | .0498<br>.037N<br>.0368<br>.0348<br>.0428 | .0298<br>.040N<br>.0368<br>.0318<br>.0248 | .010S<br>.020N<br>.016S<br>.015S            |
| 36<br>37<br>38<br>39           | .006S<br>.016S<br>.022N<br>.071N          | .003S<br>.013S<br>.016N                   | .001S<br>.008S<br>0                       | 0<br>0<br>0                               | 0<br>0<br>0                               | 0<br>0<br>0                                 |

Table 10 Lake Michigan Winds on Day of Transect and Preceding Days.

|           | 0000   | OGMT                            | 060  | OGMT                             | 120  | OGMT                           | 180  | OGMT                             |
|-----------|--|---------------------------------|--|----------------------------------|--|--------------------------------|--|----------------------------------|
| Date      | Wind<br>from                                       | Speed<br>knots                  | Wind<br>from                                       | Speed<br>knots                   | Wind<br>from                                       | Speed<br>knots                 | Wind<br>from                                       | Speed<br>knots                   |
| Novemb    | er 1962  |                                 |  |                                  |  |                                |  |                                  |
|           |  |                                 |  | East Sec                         | etor   |                                |  |                                  |
| 4 56 78 9 | *100°<br>*320°<br>*170°<br>*280°<br>*040°          | 8<br>4<br>12<br>12<br>3         | '320°<br>'050°<br>*080°<br>'210°<br>'350°<br>*050° | 16<br>21<br>4<br>29<br>16<br>2   | *230°<br>*040°<br>'170°<br>*250°<br>*330°<br>*090° | 17<br>20<br>21<br>24<br>7<br>1 | *240°<br>*020°<br>*190°<br>*270°<br>!350°<br>*130° | 11<br>14<br>28<br>24<br>19<br>10 |
|           |  |                                 |  | West Sec                         | ctor   |                                | •  | •                                |
| 4 56 78 9 | '360°<br>'300°<br>'040°<br>'180°<br>'290°<br>*360° | 15<br>34<br>14<br>30<br>28<br>7 | '320°<br>'050°<br>'160°<br>'210°<br>'350°<br>'080° | 16<br>21<br>11<br>26<br>16<br>10 | 1230°<br>1040°<br>1170°<br>1250°<br>*330°<br>*090° | 17<br>20<br>21<br>24<br>7      | *240° '020° '190° '270° '350° '130°                | 11<br>14<br>28<br>24<br>19       |

Transect of 9 November 1962

<sup>&#</sup>x27; Ship Weather Reports
\* Weather Bureau land-station data, when ship reports not available

9 November 1962

Racine - Grand Haven

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/\text{sec}$ .

| Block                      | South Transport  0 164 296 2486 3180 | North Transport 4707 0 0 0 0 | Net Transport  4707 North 164 South 296 South 2486 South 3180 South |
|----------------------------|--------------------------------------|------------------------------|---|
| 6                          | 6448                                 | 0                            | 6448 South  |
| 7                          | 1297                                 | 24                           | 1273 South  |
| 8                          | 2933                                 | 0                            | 2933 South  |
| 9                          | 281                                  | 477                          | 196 North   |
| 10                         | 4007                                 | 3                            | 4004 South  |
| 11                         | 3653                                 | 0                            | 3653 South 7 North 2057 South 332 North 4310 North                  |
| 12                         | 303                                  | 310                          |   |
| 13                         | 2057                                 | 0                            |   |
| 14                         | 556                                  | 888                          |   |
| 15                         | 0                                    | 4310                         |   |
| 16<br>17<br>18<br>19<br>20 | 0<br>0<br>0<br>6510<br>7450          | 2915<br>2406<br>5844<br>0    | 2915 North<br>2406 North<br>5844 North<br>6510 South<br>7450 South  |
| 21                         | 8                                    | 581                          | 573 North   |
| 22                         | 0                                    | 6404                         | 6404 North  |
| 23                         | 0                                    | 4477                         | 4477 North  |
| 24                         | 0                                    | 6543                         | 6543 North  |
| 25                         | 4835                                 | 0                            | 4835 South  |
| 26                         | 3702                                 | 0                            | 3702 South  |
| 27                         | 0                                    | 4625                         | 4625 North  |
| 28                         | 0                                    | 4009                         | 4009 North  |
| 29                         | 376                                  | 2644                         | 2268 North  |
| 30                         | 6719                                 | 0                            | 6719 South  |
| 31                         | 7026                                 | 0                            | 7026 South  |
| 32                         | 0                                    | 12357                        | 12357 North   |
| 33                         | 0                                    | :3509                        | 3509 North  |
| 34                         | 0                                    | 31730                        | 31730 North   |
| 35                         | 0                                    | 21102                        | 21102 North   |
| 36                         | 19112                                | 0                            | 19112 South   |
| 37                         | 2181                                 |                              | 2181 South  |
|                            | 85580                                | 119865                       | 34285 North   |

Mean Velocities in Each of the 2-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                      | <u> </u>                                  | <u>10-20m</u>                             | 20-30m                                     | 30-40m                                    | 40-50m                                     | 50-60m                                       |
|----------------------------|---|---|--|---|--|--|
| 1<br>2<br>3<br>4<br>5      | .146s<br>.005N<br>.006N<br>.036N<br>.036N | 0<br>0<br>.003N<br>.026N<br>.028N         | 0<br>0<br>0<br>.015N<br>.021N              | 0<br>0<br>0<br>0<br>.014N                 | 0 0 0                                      | 0<br>0<br>0<br>0                             |
| 6<br>7<br>8<br>9<br>10     | .043N<br>.016N<br>.024N<br>.006S<br>.046N | .041N<br>.011N<br>.021N<br>.006S<br>.036N | .038N<br>.008N<br>.018N<br>.003S<br>.025N  | .034N<br>.005N<br>.013N<br>.002N<br>.014N | .030N<br>.001N<br>.010N<br>.005N<br>.004N  | .014N<br>.0008s<br>.004N<br>.003N            |
| 11<br>12<br>13<br>14<br>15 | .028N<br>.006S<br>.022N<br>.017S<br>.035S | .025N<br>.003S<br>.017N<br>.009S<br>.032S | .023N<br>.0007S<br>.013N<br>.001S<br>.028S | .019N<br>.003N<br>.007N<br>.007N<br>.024S | .014N<br>.004N<br>.004N<br>.008N<br>.013S  | .005N<br>.002N<br>.002N<br>.003N<br>.002S    |
| 16<br>17<br>18<br>19<br>20 | .020S<br>.023S<br>.037S<br>.041N          | .018s<br>.018s<br>.037s<br>.043N<br>.040N | .016s<br>.013s<br>.037s<br>.043N<br>.044N  | .016s<br>.009s<br>.034s<br>.038n<br>.053N | .014s<br>.008s<br>.026s<br>.027N           | .0078<br>.0058<br>.0108<br>.010N             |
| 21<br>22<br>23<br>24<br>25 | .006s<br>.059s<br>.024s<br>.038s<br>.041N | .004s<br>.051s<br>.027s<br>.038s<br>.036N | .004s<br>.042s<br>.029s<br>.038s<br>.030N  | .0038<br>.0328<br>.0328<br>.0388<br>.023N | .00098<br>.0148<br>.0228<br>.0368<br>.015N | .0003N<br>.005S<br>.005S<br>.017S<br>.006N   |
| 26<br>27<br>28<br>29<br>30 | .028N<br>.062S<br>.050S<br>.047S<br>.030N | .026N<br>.035S<br>.031S<br>.027S<br>.021N | .023N<br>.020S<br>.015S<br>.008S<br>.029N  | .019N<br>.015S<br>.010S<br>.002N<br>.060N | .014N<br>.009S<br>.012S<br>.006N<br>.054N  | .006N<br>.003S<br>.007S<br>.004N<br>.015N    |
| 31<br>32<br>33<br>34<br>35 | .072N<br>.105S<br>.024S<br>.252S<br>.191S | .064N<br>.099S<br>.026S<br>.217S<br>.162S | .048N<br>.088S<br>.027S<br>.188S<br>.129S  | .026N<br>.066S<br>.023S<br>.163S<br>.093S | .008N<br>.026S<br>.009S<br>.121S<br>.059S  | .001N<br>.0002S<br>.00003S<br>.045S<br>.021S |
| 36<br>37                   | .244N<br>.037N                            | .198N<br>.030N                            | .152N                                      | 0   | 0  | O<br>O                                       |

Table 13 Lake Michigan Winds on Day of Transect and Preceding Days.

|                                  | 000  | OGMT                         | 060  | OGMT                           | 120  | OGMT                        | 180  | OGMT                           |
|----------------------------------|--|------------------------------|--|--------------------------------|--|-----------------------------|--|--------------------------------|
| Date                             | Wind<br>from                                       | Speed<br>knots               | Wind<br>from                                       | Speed<br>knots                 | Wind<br>from                                       | Speed<br>knots              | Wind<br>from                                       | Speed<br>knots                 |
| April                            | 1963   |                              |  |                                |  |                             |  | •                              |
|                                  |  |                              |  | East Sec                       | etor   |                             |  |                                |
| 12<br>13<br>14<br>15<br>16<br>17 | *040°<br>*340°<br>*030°<br>*340°<br>*210°<br>*180° | 549955<br>15                 | '010°<br>*050°<br>'320°<br>*360°<br>*170°<br>*180° | 15<br>6<br>13<br>1<br>10<br>11 | '340°<br>*330°<br>*310°<br>*320°<br>*170°<br>*150° | 7<br>5<br>1<br>14<br>9      | *310°<br>*340°<br>*320°<br>*220°<br>!160°<br>!180° | 9<br>13<br>14<br>3<br>30<br>17 |
|                                  |  |                              |  | West Se                        | ctor   |                             |  |                                |
| 12<br>13<br>14<br>15<br>16<br>17 | *070°<br>*070°<br>'360°<br>*080°<br>*160°<br>*230° | 5<br>5<br>9<br>8<br>10<br>10 | '010°<br>'330°<br>*270°<br>*200°<br>*160°<br>*180° | 15<br>9<br>2<br>2<br>12<br>11  | 1340°<br>1340°<br>*260°<br>*200°<br>*160°<br>*210° | 7<br>8<br>4<br>9<br>16<br>6 | '120°<br>'360°<br>*020°<br>*170°<br>!160°<br>'200° | 13<br>9<br>12<br>8<br>30<br>20 |

Transect of 17 April 1963

<sup>&#</sup>x27; Ship Weather Reports
\* Weather Bureau land-station data, when ship reports not available

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/sec$ .

| Block                      | North Transport  | South Transport | Net Transport                 |
|----------------------------|------------------|-----------------|-------------------------------|
| 1<br>2                     | 680<br>1445      | 0<br>0<br>0     | 680 North                     |
| 1<br>2<br>3<br>4<br>5      | 0<br>1620        | 0               | 0<br>1620 North               |
| 5                          | 0                | 1620            | 1620 South                    |
| 6                          | 590              | 0<br>2116       | 590 North<br>2116 South       |
| 8                          | 0                | 0               | 0                             |
| 6<br>7<br>8<br>9<br>10     | 0<br>671         | 671<br>0        | 671 South<br><u>671 North</u> |
| 11                         | 0                | 0               | 0<br>468 North                |
| 12<br>13<br>14             | 468<br>0         | 0<br>310<br>828 | 310 South                     |
| 14<br>15                   | 0<br>346         | 828<br>0        | 828 South<br>346 North        |
| 16                         | 0                | 346             | 346 South<br>1419 North       |
| 17<br>18                   | 1419             | 0               | 0                             |
| 19<br>20                   | 654<br>0         | 0<br>0<br>0     | 654 North                     |
| 21                         | 0                | 523<br>0        | 523 South<br>910 North        |
| 22 ·<br>23                 | 910<br>0         | 386             | 386 South                     |
| 23<br>24<br>25             | 386<br>Ģ         | 0               | 386 North<br>0                |
| 26                         | 0                | 0<br>386        | 0<br>386 South                |
| 28                         | 0<br>0<br>0<br>0 | 0               | 0                             |
| 27<br>28<br>29<br>30       | 0                | 2922<br>317     | 2922 South 317 South          |
| 31                         | 0                | 0               | 0                             |
| 32<br>33                   | 0<br>0<br>0      | 0               | 0                             |
| 31<br>32<br>33<br>34<br>35 | 0                | 0<br>1477       | 0<br>1477 South               |
| 36                         | 6                | 1172            | 1166 South                    |
| 36<br>37<br>38             | 0                | 748<br>389      | 748 South<br>389 South        |
|                            | 9145             | 14211           | 5016 South                    |

Table 15

Milwaukee - Grand Haven

17 April 1963

Mean Velocities in Each of the 2-mile x 10-meter Blocks.
Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block<br>1                 | 0-10m<br>.008N          | 10-20m                     | 20-30m<br>.005N         | 30-40m<br>.002N             | 40-50m<br>0             | 50-60m                  |
|----------------------------|-------------------------|----------------------------|-------------------------|-----------------------------|-------------------------|-------------------------|
| 2<br>3<br>4                | .010N<br>0<br>.015N     | .010N<br>0<br>.013N        | .009N<br>0<br>.010N     | .008 <u>N</u><br>0<br>.007N | .005N<br>0<br>.004N     | .002N<br>0<br>.001N     |
| 5                          | .0158                   | .013S                      | .010S                   | .007S                       | .004S                   | .001S                   |
| 6<br>7<br>8                | .004N<br>.020S          | .004N<br>.016S             | .004N<br>.013S          | .003N<br>.009S              | .002N<br>.0058          | .001N<br>.002S          |
| 8<br>9<br>10               | 0<br>.005S<br>.005N     | 0<br>.005S<br>.005N        | 0<br>.0058<br>.005N     | 0<br>.004s<br>.004n         | 0<br>.002S<br>.002N     | 0<br>.001S<br>.001N     |
| 11<br>12                   | 0<br>.005N              | 0<br>.003N                 | 0<br>.002N              | 0<br>.002N                  | 0<br>.002N              | 0<br>.001N              |
| 13<br>14<br>15             | .002S<br>.008S<br>.002N | .002S<br>.006S<br>.002N    | .002S<br>.005S<br>.002N | .0028<br>.0048<br>.002N     | .002S<br>.002S<br>.002N | .001S<br>.001S<br>.001N |
| 16<br>17                   | .002S                   | .002S<br>.011N             | .002S<br>.009N          | .002S<br>.007N              | .002S<br>.004N          | .001S                   |
| 18<br>19<br>20             | 0<br>006N               | 0<br>.005N<br>0            | 0<br>.004N<br>0         | 0<br>.003N<br>0             | 0<br>.002N<br>0         | 0<br>.001N<br>0         |
| 21<br>22                   | .004S                   | .004S                      | .004s<br>.006N          | .003S<br>.005N              | .002S<br>.003N          | .001S<br>.001N          |
| 23<br>24<br>25             | .003S<br>.003N<br>0     | .003S<br>.003N<br>0        | .002S<br>.002N<br>0     | .002S<br>.002N              | .002S<br>.002N<br>0     | .001S<br>.001N          |
| 26<br>27                   | 0<br>.003S              | 0<br>.003S                 | 0<br>.002S              | 0<br>.002S                  | 0<br>.002S              | 0<br>.001S              |
| 28<br>29<br>30             | 0<br>.028s<br>.003s     | 0<br>.023<br>.003 <b>s</b> | 0<br>.018s<br>.002s     | 0<br>.012S<br>.001S         | 0<br>.007S<br>0         | 0<br>.002S<br>0         |
|                            | 0                       | 0                          | 0                       | 0                           | 0                       | 0                       |
| 31<br>32<br>33<br>34<br>35 | 0<br>0<br>0             | 0<br>0<br>0                | 0<br>0<br>0             | 0<br>0<br>0                 | 0<br>0<br>0             | 0<br>0<br>0             |
| 35                         | .014s                   | .012S                      | .009s                   | .006s                       | .0048                   | .0018                   |
| 36<br>37<br>38             | .013S<br>.010S<br>.002S | .010S<br>.007S<br>.002S    | .008s<br>.004s<br>.002s | .004S<br>.001S<br>.002S     | .001S<br>0<br>.002S     | 0<br>0<br>.001S         |

Table 16

Lake Michigan Winds on Day of Transect and Preceding Days.

Transect of 20 May 1963

|                                  | 000  | OGMT                           | 060                                       | OGMT                       | 120  | OGMT                          | 1800  | OGMT                          |
|----------------------------------|--|--------------------------------|---|----------------------------|--|-------------------------------|---|-------------------------------|
| Date                             | Wind<br>from                                       | Speed<br>knots                 | Wind<br>from                              | Speed<br>knots             | Wind<br>from                                       | Speed<br>knots                | Wind<br>from  | Speed<br>knots                |
| May 19                           | 63   |                                |   |                            |  |                               |   |                               |
|                                  |  |                                |   | East Sec                   | ctor   |                               |   |                               |
| 15<br>16<br>17<br>18<br>19<br>20 | 1090°<br>*150°<br>*050°<br>*330°<br>*270°<br>*300° | 34<br>5<br>3<br>7<br>14<br>10  | *010°<br>*010°<br>*090°<br>*260°<br>*300  | 547596                     | *070° '360° '110° *230° *260° *280°                | 2<br>13<br>17<br>10<br>4<br>9 | *200°<br>* Calm<br>*040°<br>*290°<br>*210°<br>'180° | 4<br>6<br>15<br>14<br>14      |
|                                  |  |                                |   | West Se                    | ctor   |                               |   |                               |
| 15<br>16<br>17<br>18<br>19<br>20 | '090°<br>'030°<br>*030°<br>'210°<br>'010°<br>*280° | 34<br>10<br>9<br>12<br>6<br>12 | *060°<br>'220°<br>*050°<br>*200°<br>*320° | 4<br>8<br>4<br>5<br>7<br>4 | *340°<br>'010°<br>'270°<br>'250°<br>*190°<br>*290° | 3<br>12<br>13<br>9<br>6<br>7  | *070°<br>*050°<br>*010°<br>*270°<br>*240°<br>*270°  | 8<br>7<br>9<br>16<br>13<br>11 |

<sup>&#</sup>x27; Ship Weather Reports

<sup>\*</sup> Weather Bureau land-station data, when ship reports not available

Table 17

Grand Haven - Milwaukee

20 May 1963

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/sec$ .

| Block                      | North Transport        | South Transport         | Net Transport                                     |
|----------------------------|------------------------|-------------------------|---|
| 1                          | 648                    | 0 0 0 0 0               | 648 North   |
| 2                          | 2910                   |                         | 2910 North  |
| 3                          | 2241                   |                         | 2241 North  |
| 4                          | 625                    |                         | 625 North   |
| 5                          | 333                    |                         | 333 North   |
| 6                          | 0                      | 883                     | 883 South 78 North 67 North 571 South 258 South   |
| 7                          | 78                     | 0                       |   |
| 8                          | 67                     | 0                       |   |
| 9                          | 0                      | 571                     |   |
| 10                         | 0                      | 258                     |   |
| 11                         | 0                      | 0                       | 0   |
| 12                         | 50                     | 0                       | 50 North  |
| 13                         | 27                     | 0                       | 27 North  |
| 14                         | 180                    | 0                       | 180 North   |
| 15                         | 0                      | 28                      | 28 South  |
| 16<br>17<br>18<br>19<br>20 | 469<br>333<br>215<br>0 | 0<br>0<br>0<br>88<br>51 | 469 North 333 North 215 North 88 South 51 South   |
| 21                         | 0                      | 604                     | 604 South 655 North 357 South 306 North 271 South |
| 22                         | 655                    | 0                       |   |
| 23                         | 0                      | 357                     |   |
| 24                         | 306                    | 0                       |   |
| 25                         | 0                      | 271                     |   |
| 26                         | 0                      | 35                      | 35 South  |
| 27                         | 0                      | 107                     | 107 South   |
| 28                         | 281                    | 0                       | 281 North   |
| 29                         | 382                    | 0                       | 382 North   |
| 30                         | 0                      | 50                      | 50 South  |
| 31                         | 180                    | 0                       | 180 North   |
| 32                         | : 0                    | 145                     | 145 South   |
| 33                         | 86                     | 0                       | 86 North  |
| 34                         | 75                     | 0                       | 75 North  |
| 35                         | 0                      | 218                     | 218 South   |
| 36<br>37                   | 0                      | 494<br>O                | 494 South   |
|                            | 10141                  | 4160                    | 5981 North  |

Table 18

Grand Haven - Milwaukee

20 May 1963

Mean Velocities in Each of the 2-mile x 10-meter Blocks.
Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                      | <u> </u>                                  | 10-20m                                    | 20-30m                                    | <u>30-40m</u>                     | <u>40-50m</u>                     | <u>50-60m</u>             |
|----------------------------|---|---|---|-----------------------------------|-----------------------------------|---------------------------|
| 1<br>2<br>3<br>4<br>5      | .013N<br>.061N<br>.031N<br>.007N<br>.004N | .007N<br>.025N<br>.020N<br>.005N<br>.003N | .001N<br>.004N<br>.011N<br>.004N<br>.002N | 0<br>0<br>.005N<br>.002N<br>.001N | 0<br>0<br>.002N<br>.001N<br>.001N | 0<br>0<br>.001N<br>0<br>0 |
| 6<br>7<br>8<br>9<br>10     | .008s<br>0<br>0<br>.005s<br>.003s         | .007S<br>0<br>0<br>.005S<br>.002S         | .005S<br>0<br>0<br>.004S<br>.001S         | .004S<br>0<br>0<br>.002S<br>.001S | .003S<br>0<br>0<br>.001S<br>.001S | .001S<br>0<br>0<br>0      |
| 11<br>12<br>13<br>14<br>15 | 0<br>0<br>0<br>.002N                      | 0<br>0<br>.001N                           | 0<br>0<br>0<br>.001N                      | 0<br>0<br>0<br>.001N              | 0 0 0                             | 0 0 0 0                   |
| 16<br>17<br>18<br>19<br>20 | .005N<br>.003N<br>.002N<br>.001S          | .004N<br>.003N<br>.002N<br>.001S          | .003N<br>.002N<br>.001N<br>0              | .002N<br>.001N<br>.001N<br>0      | .001N<br>.001N<br>0<br>0          | 0 0 0 0                   |
| 21<br>22<br>23<br>24<br>25 | .0058<br>.006N<br>.003S<br>.003N          | .005S<br>.005N<br>.003S<br>.002N          | .0048<br>.004N<br>.0028<br>.002N          | .003S<br>.003N<br>.002S<br>.001N  | .002S<br>.002N<br>.001S<br>.001N  | .001S<br>.001N<br>0<br>0  |
| 26<br>27<br>28<br>29<br>30 | 0<br>.001S<br>.003N<br>.003N              | 0<br>.001S<br>.002N<br>.003N              | 0<br>.001S<br>.002N<br>.002N              | 0<br>.001S<br>.001N<br>.002N      | 0<br>0<br>.001N<br>.001N          | 0<br>0<br>0<br>.001N      |
| 31<br>32<br>33<br>34<br>35 | .002N<br>.001S<br>.001N<br>.001N          | .001N<br>.001S<br>.001N<br>.001N          | .001N<br>.001S<br>.001N<br>.001N          | .001N<br>.001S<br>0<br>0          | 0 0 0 0                           | 0<br>0<br>0<br>0          |
| 36<br>37                   | .015S<br>0                                | 0<br>0                                    | O<br>O                                    | 0<br>0                            | 0<br>0                            | 0                         |

Table 19

Lake Michigan Winds on Day of Transect and Preceding Days.

1800GMT OOOOGMT 0600GMT 1200GMT Speed Wind Speed Wind Speed Wind Speed Wind knots Date from from knots from knots from knots June 1963 East Sector \*170° \*310° 2 18 Calm \*170° \*220° \*220° \*210° 74 4 8 14 19 \*290° \*210° \*330° \*340° 20 14 11 10 \*020° \*350° \*340° 4 \*330° 11 21 11 \*330° \*290° \*01:0° 954 \*180° \*340° 354 55 2 \*150° \*060° \*110° 2 23 24 \*140° \*110° \*090° \*190° West Sector \*110° 18 \*230° \*010° 2 2 3 13 14 8 6 8 \*130° \*200° 6 \*200° \*220° 19 \*190° \*330° \*030° 14 \*020° 2 20 10 \*050° \*360° 72 \*010° 5 \*030° 21 976 \*070° \*230° \*000° \*110° 22 Calm \*100° 23 \*060° 4 \*140° 2 \*110°

3

\*060°

2

\*110°

Transect of 24 June 1963

\*050°

\*070°

24

<sup>\*</sup> Weather Bureau land-station data.

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/sec$ .

| Block                      | North Transport                   | South Transport           | Net Transport  |
|----------------------------|-----------------------------------|---------------------------|--|
| 1<br>2<br>3<br>4<br>5      | 100<br>0<br>0<br>718<br>407       | 1292<br>1394<br>11<br>120 | 100 North<br>1292 South<br>1394 South<br>707 North<br>287 North  |
| 6                          | 0                                 | 1464                      | 1464 South   |
| 7                          | 0                                 | 4090                      | 4090 South   |
| 8                          | 5352                              | 0                         | 5352 North   |
| 9                          | 112                               | 0                         | 112 North  |
| 10                         | 0                                 | 489                       | 489 South  |
| 11                         | 1513                              | 0                         | 1513 North   |
| 12                         | 593                               | 0                         | 593 North  |
| 13                         | 0                                 | 644                       | 644 South  |
| 14                         | 247                               | 13                        | 234 North  |
| 15                         | 0                                 | 981                       | 981 South  |
| 16<br>17<br>18<br>19<br>20 | 448<br>650<br>407<br>1597<br>186  | 779<br>621<br>0<br>223    | 331 South 650 North 215 South 1597 North 37 South                |
| 21                         | 87                                | 1581                      | 1494 South   |
| 22                         | 2                                 | 837                       | 835 South  |
| 23                         | 2391                              | 0                         | 2391 North   |
| 24                         | 0                                 | 1071                      | 1071 South   |
| 25*                        | 0                                 | 0                         | 0  |
| 26                         | 0                                 | 1495                      | 1495 South   |
| 27                         | 0                                 | 4252                      | 4252 South   |
| 28                         | 6391                              | 0                         | 6391 North   |
| 29                         | 353                               | 28                        | 326 North  |
| 30                         | 0                                 | 3499                      | 3499 South   |
| 31<br>32<br>33<br>34<br>35 | 125<br>2587<br>1537<br>736<br>784 | 1611<br>0<br>329<br>0     | 1486 South<br>2587 North<br>1209 North<br>736 North<br>784 North |
| 36                         | 0                                 | 1607                      | 1607 South   |
| 37                         | 0                                 | 1051                      | 1051 South   |
| 38                         | 280                               | 195                       | 85 North   |
| 39                         | 0                                 | 601                       | 601 South  |
|                            | 27603                             | 30278                     | 2675 South   |

<sup>\*</sup>Leg runs north-south

Table 21

Grand Haven - Port Washington

24 June 1963

Mean Velocities in Each of the 2-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                       | 0-10m                                     | 10-20m                                    | 20-30m                                    | 30-40m                                    | 40-50m                                    | <u>50-60m</u>                     |
|-----------------------------|---|---|---|---|---|-----------------------------------|
| 1<br>2<br>3<br>4<br>5       | .002N<br>.022S<br>.024S<br>.013N<br>.004S | .001N<br>.014S<br>.015S<br>.007N          | 0<br>.0048<br>.0048<br>.002N<br>.004N     | 0<br>0<br>0<br>0<br>.001N                 | 0<br>0<br>0<br>0                          | 0<br>0<br>0<br>0                  |
| 6<br>7<br>8<br>9            | .021S<br>.036S<br>.071S<br>.002S<br>.008S | .017S<br>.043S<br>.051S<br>.001S<br>.004S | .007S<br>.032S<br>.032S<br>.002S          | .001S<br>.014S<br>.012S<br>.001S          | 0<br>.002S<br>.001S<br>0                  | 0<br>0<br>0<br>0                  |
| 11<br>12<br>13<br>14<br>15  | .014N<br>.012N<br>.008S<br>0<br>.011S     | .013N<br>.004N<br>.003S<br>.001N          | .010N<br>.001N<br>.003S<br>.002N<br>.006S | .006N<br>.001N<br>.003S<br>.002N<br>.003S | .003N<br>.001N<br>.002S<br>.002N<br>.001S | .001N<br>0<br>.001S<br>.001N<br>0 |
| 16<br>17<br>18<br>19<br>20  | .0248<br>.004N<br>.013N<br>.020N<br>.007S | .001N<br>.007N<br>.004S<br>.016N          | .007N<br>.007N<br>.009S<br>.008N<br>.002N | .004N<br>.002N<br>.004S<br>.003N<br>.002N | .001N<br>.001N<br>.002S<br>.002N<br>.001N | 0<br>0<br>.001S<br>0              |
| 21<br>22<br>23<br>24<br>25* | .040S<br>.016S<br>.052N<br>.014S          | .0098<br>.0088<br>.019N<br>.0088          | .002N<br>.002S<br>.002N<br>.006S          | .001N<br>.001S<br>.001N<br>.003S          | 0<br>0<br>0<br>.002 <b>s</b><br>0         | 0<br>0<br>0<br>.001S<br>0         |
| 26<br>27<br>28<br>29<br>30  | .0158<br>.0688<br>.094N<br>.0018<br>.0568 | .0158<br>.0318<br>.052N<br>.004N          | .008s<br>.018s<br>.027N<br>.004N          | .0048<br>.0108<br>.015N<br>.002N          | .003S<br>.005S<br>.008N<br>.001N          | .001S<br>.001S<br>.003N<br>0      |
| 31<br>32<br>33<br>34<br>35  | .0478<br>.056N<br>.034N<br>.018N<br>.010N | .003S<br>.021N<br>.013N<br>0<br>.008N     | .004N<br>.002N<br>.003S<br>.001N<br>.003N | 0<br>.001N<br>.004S<br>.001N<br>.002N     | 0<br>.001N<br>.002S<br>.001N              | 0<br>0<br>.001S<br>0              |
| 36<br>37<br>38<br>39        | .030S<br>.006S<br>.009N<br>.013S          | .016s<br>.008s<br>0<br>.005s              | .003S<br>.009S<br>.004S<br>0              | .006s<br>.001s<br>.0                      | 0<br>.003S<br>0                           | 0<br>.001S<br>0                   |

<sup>\*</sup>Leg runs north-south

Table 22

Lake Michigan Winds on Day of Transect and Preceding Days.

# Transect of 24 July 1963

|                                  | OOOOGMT                                   |                        | <u>0600GMT</u>                                     |                            | 120   | 1200GMT                      |  | 1800GMT                       |  |
|----------------------------------|---|------------------------|--|----------------------------|---|------------------------------|--|-------------------------------|--|
| Date                             | Wind<br>from                              | Speed<br>knots         | Wind<br>from                                       | Speed<br>knots             | Wind<br>from                                    | Speed<br>knots               | Wind<br>from                                       | Speed<br>knots                |  |
| July                             | 1963                                      |                        |  |                            |   |                              |  |                               |  |
|                                  |   |                        |  | East Sec                   | ctor  |                              |  |                               |  |
| 19<br>20<br>21<br>22<br>23<br>24 | *210°<br>*330°<br>*320°<br>*040°<br>*050° | 10<br>8<br>7<br>4      | *220°<br>*240°<br>*250°<br>*270°<br>*070°<br>*090° | 942635                     | *200°<br>*330°<br>*260°<br>*260°<br>*100°       | 10<br>11<br>4<br>3<br>5<br>2 | *270°<br>*340°<br>*290°<br>*270°<br>*090°<br>*120° | 8<br>10<br>11<br>8<br>10<br>2 |  |
|                                  |   |                        |  | West Sed                   | ctor  | <br>1                        |  |                               |  |
| 19<br>20<br>21<br>22<br>23<br>24 | *010°<br>*360°<br>*050°<br>*090°<br>*030° | 3<br>6<br>10<br>5<br>8 | *216°<br>*250°<br>*220<br>*240°<br>*060°<br>*020°  | 8<br>4<br>2<br>3<br>4<br>3 | *240°<br>*310°<br>*270°<br>Ca<br>*010°<br>*100° | 7<br>11<br>6<br>1m<br>5<br>3 | *310°<br>*340°<br>*320°<br>*050°<br>*070°<br>*090° | 2<br>12<br>7<br>3<br>7<br>6   |  |

<sup>\*</sup> Weather Bureau land-station data.

24 July 1963

Muskegon - Milwaukee

Water-Volume Transports in the 2-mile x 60-meter Blocks,  $m^3/\text{sec}$ .

| Block | North Transport | South Transport | Net Transport  |
|-------|-----------------|-----------------|--|
| 1     | 3151            | 0               | 3151 North 38 North 2370 North 1110 South 1037 South |
| 2     | 332             | 294             |  |
| 3     | 2410            | 40              |  |
| 4     | 0               | 1110            |  |
| 5     | 62              | 1099            |  |
| 6     | 4               | 794             | 790 South  |
| 7     | 0               | 2355            | 2355 South   |
| 8     | 737             | 0               | 737 North  |
| 9     | 2094            | 231             | 1863 North   |
| 10    | 46              | 309             | 263 South  |
| 11    | 2212            | 0               | 2212 North 2 North 825 North 1720 South 155 South    |
| 12    | 146             | 144             |  |
| 13    | 825             | 0               |  |
| 14    | 76              | 1796            |  |
| 15    | 135             | 290             |  |
| 16    | 71              | 455             | 384 South  |
| 17    | 0               | 326             | 326 South  |
| 18    | 237             | 1890            | 1654 South   |
| 19    | 3615            | 0               | 3615 North   |
| 20    | 185             | 1985            | 1800 South   |
| 21    | 0               | 3410            | 3410 South   |
| 22    | 57              | 398             | 341 South  |
| 23    | 3542            | 0               | 3542 North   |
| 24    | 2866            | 0               | 2866 North   |
| 25    | 578             | 2               | 576 North  |
| 26    | 0               | 1565            | 1565 South   |
| 27    | 20              | 1465            | 1445 South   |
| 28    | 660             | 0               | 660 North  |
| 29    | 382             | 114             | 268 North  |
| 30    | 0               | 1508            | 1508 South   |
| 31    | 0               | 3154            | 3154 South   |
| 32    | 3043            | 0               | 3043 North   |
| 33    | 191             | 486             | 296 South  |
| 34    | 3534            | 0               | 3534 North   |
| 35    | 1184            | 0               | 1184 North   |
| 36    | 0               | 1246            | 1246 South   |
|       | 32395           | 26466           | 5927 North   |

Table 24

Muskegon - Milwaukee

24 July 1963

Mean Velocities in Each of the 2-mile x 10-meter Blocks. Mean Velocity, m/sec = Block Net Transport/Block Area.

| Block                      | <u> </u>                                  | 10-20m                                    | 20-30m                                    | <u>30-40m</u>                             | 40-50m                                    | <u>50-60m</u>                     |
|----------------------------|---|---|---|---|---|-----------------------------------|
| 1<br>2<br>3<br>4<br>5      | .088N<br>.009N<br>.065N<br>.007S<br>.025S | .010N<br>.009S<br>.010N<br>.002S<br>.009S | 0<br>.001N<br>.001S<br>.009S<br>.001S     | 0<br>0<br>.001S<br>.009S<br>.001N         | 0<br>0<br>0<br>.006S<br>.001N             | 0<br>0<br>0<br>.0028              |
| 6<br>7<br>8<br>9<br>10     | .024S<br>.043S<br>.002N<br>.051N          | 0<br>.021S<br>.006N<br>.014N<br>.001S     | .001S<br>.006S<br>.007N<br>.002S<br>.002S | 0<br>.003s<br>.004n<br>.002s<br>.003s     | 0<br>.001S<br>.003N<br>.002S<br>.002S     | 0<br>0<br>.001N<br>.001S<br>.001S |
| 11<br>12<br>13<br>14<br>15 | .034N<br>.004S<br>.020N<br>.048S<br>.009S | .015N<br>0<br>0<br>.008s<br>.004N         | .009N<br>.001N<br>.002N<br>0              | .006N<br>.001N<br>.002N<br>.001N          | .004N<br>.001N<br>.001N<br>.001N          | .001N<br>.001N<br>0<br>0          |
| 16<br>17<br>18<br>19<br>20 | .009S<br>.002S<br>.048S<br>.087N          | .0058<br>.0018<br>.0118<br>.020N          | .001N<br>.002S<br>.002N<br>.004N<br>.002N | .001N<br>.003S<br>.003N<br>.002N          | 0<br>.002S<br>.002N<br>0                  | 0<br>.001S<br>.001N<br>0          |
| 21<br>22<br>23<br>24<br>25 | .081S<br>.004S<br>.078N<br>.066N          | .0228<br>.0068<br>.024N<br>.020N          | .002S<br>.003S<br>.006N<br>.003N          | .001S<br>.001N<br>.002N<br>.001N          | 0<br>.001N<br>0<br>0                      | 0<br>0<br>0<br>0                  |
| 26<br>27<br>28<br>29<br>30 | .026S<br>.040S<br>.012N<br>.010N<br>.030S | .013S<br>.005S<br>.003N<br>.002N<br>.014S | .0058<br>0<br>.003N<br>.0028<br>.0028     | .003S<br>0<br>.002N<br>.001S              | .001S<br>0<br>.001N<br>.001S              | 0<br>0<br>0<br>0                  |
| 31<br>32<br>33<br>34<br>35 | .053S<br>.045N<br>.005N<br>.082N<br>.023N | .032S<br>.031N<br>.001N<br>.017N<br>.008N | .008s<br>.011N<br>.007S<br>.006N<br>.003N | .0038<br>.044N<br>.0058<br>.003N<br>.002N | .001S<br>.002N<br>.003S<br>.002N<br>.001N | 0<br>.001N<br>.001S<br>.001N      |
| 36                         | .0248                                     | .009S                                     | .005S                                     | .0018                                     | 0   | 0                                 |

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## APPENDIX

BATHYTHERMOGRAPH DATA



#### Muskegon to Milwaukee 10 August 1962

| Slide<br>No. | Depth,M                    | Temp.°C                     | Slide<br>No. | Depth,M               | Temp.°C              | Slide<br>No. | Corr.                 | Temp.°C<br>Corr.         |
|--------------|----------------------------|-----------------------------|--------------|-----------------------|----------------------|--------------|-----------------------|--------------------------|
| 43°<br>6     | 13.3', 86°<br>0<br>8.0     | 21.61                       | 12           | 39.0<br>57.0<br>112.5 | 5.2<br>4.3           | 16           | 33.0<br>36.0          | 5.2<br>5.4.6<br>4.6      |
|              | 11.0                       | 16.5<br>15.5<br>13.5        | 43           | 10.7', 86             | 18.6                 |              | 59.0<br>99.0<br>103.0 | 4.6<br>4.7               |
| - 100        | 13.5<br>14.0               | 10.9                        | 13           | 0<br>5.0<br>14.0      | 18.3<br>18.2         | 43<br>17     |                       |                          |
| 43°          | 13.0', 86<br>0<br>4.0      | 17.5<br>17.2                |              | 17.0<br>20.5          | 18.1<br>17.2         |              | 2.0                   | 19.0<br>18.8             |
|              | 10.5<br>13.0               | 15.1<br>13.8                |              | 24.0                  | 15.0                 |              | 3.5<br>5.5<br>16.0    | 18.7<br>18.4             |
|              | 17.5<br>30.0               | 5.9<br>5.8                  |              | 31.0<br>36.5          | 11.5<br>7.3<br>6.0   |              | 17.0<br>18.5          | 18.3<br>18.0             |
| 43°          | 12.61, 86                  | °26.8'<br>18.4              |              | 43.0<br>48.0          | 5.0<br>4.6           |              | 19.0<br>24.0          | 15.0<br>9.5<br>6.3       |
|              | 0<br>6.0<br>11.0           | 17.9<br>13.5                | 43           | 114.5<br>10.4', 86    | 4.5<br>945.1         |              | 27.0<br>28.0          | 6.0                      |
|              | 12.0                       | 10.7                        | 14           | 0                     | 19.3<br>18.8         |              | 37.0<br>49.0          | 5.3<br>5.0<br>4.7        |
|              | 22.0<br>48.0               | 5.5<br>5.4<br>5.0           |              | 9.0<br>16.0           | 18.5                 |              | 53.0<br>97.0          | 4.6                      |
| 43°<br>9     | 0                          | 18.6                        |              | 18.5<br>22.5          | 18.0                 | 18           | 0                     | 7°02.0'<br>19.9<br>19.1  |
|              | 1.0                        | 18.5<br>18.4<br>18.3<br>6.2 |              | 24.0<br>25.0<br>28.5  | 12.0<br>9.8<br>6.8   |              | 2.5<br>16.5<br>17.0   | 18.7<br>18.4             |
|              | 9.0<br>16.0<br>21.0        | 6.2                         |              | 36.0<br>42.0          | 5.4<br>5.0           |              | 19.0                  | 17.6<br>9.9              |
|              | 30.0                       | 5.0<br>4.6<br>4.3           |              | 58.5<br>112.0         | 4.7                  |              | 21.5<br>23.5          | 9.0                      |
| 43°          | '11.8°, 86                 |                             | 43<br>15     |                       | 19.8                 |              | 29.0<br>36.0          | 5.8<br>5.3               |
|              | 3.0<br>17.0                | 18.6<br>18.0                |              | 0.5<br>6.0            | 19.0<br>18.6         |              | 40.0<br>45.0          | 5.0<br>4.8               |
|              | 23.0<br>42.0               | 6.1<br>4.7                  |              | 14.0<br>19.0          | 18.5<br>18.1         |              | 65.0<br>90.0          | 4.4<br>4.3               |
| 43           | 113.0<br>11.4', 86         | 4.3<br>5°36.1'              |              | 21.0                  | 17.0<br>9.0          | 19           | 0                     | 19.7                     |
| 11           | 0<br>5.0<br>14.0           | 18.4<br>18.2                |              | 25.0<br>34.0<br>45.0  | 7.6<br>5.5<br>5.1    |              | 1.5<br>2.0<br>4.5     | 19.5-<br>18.8<br>18.4    |
|              | 17.0<br>17.0               | 18.1<br>17.8<br>16.5        |              | 45.0<br>54.0<br>59.0  | 4.9                  |              | 17.0<br>19.5          | 18.0<br>17.2             |
|              | 25.0<br>29.0               | 8.0                         |              | 102.0                 | 4.5<br>4.5<br>4.6    |              | 23.0                  | 11.7                     |
|              | 35.0                       | 4.9<br>4.4                  | 43<br>16     | °10.0°, 8             | 5°50.91              |              | 30.0<br>44.0          | 6.0                      |
| 43           | 50.0<br>112.0<br>11.0', 80 | 4.2<br>5°39.2'              | , = -        | 2.0<br>5.5            | 19.8<br>18.8<br>18.6 |              | 63.0<br>66.0          | 4.8<br>4.4<br>4.3<br>4.3 |
| 12           | 3.0                        | 18.7<br>18.4                |              | 19.0<br>21.0          | 18.3<br>17.7         |              |                       | 707.21                   |
|              | 16.0<br>26.0               | 18.0<br>12.0                |              | 25.0<br>26.5          | 10.0<br>8.8<br>6.3   | 20           | 2.0                   | 19.8<br>18.7             |
|              | 27.5<br>36.0               | 9.0<br>5.8                  | -            | 29.0<br>31.0          | 6.3<br>6.2           |              | 6.0<br>11.0           | 18.7<br>18.1<br>17.8     |

| No.  | Corr.   | Corr.   | No.      | Corr.  | Corr.                                | No.        | Corr.                                      | Corr.                                       |
|------|---|---|----------|--|--------------------------------------|------------|--|---|
| 20   | 14.0  | 17.7  | 24       | 21.0   | 11.5                                 | 43°0       | 25.21.87                                   | 25.71                                       |
|      | 18.0<br>23.0  | 17.5<br>14.7                                  |          | 23.5<br>29.0                                       | 8.0<br>6.3<br>5.9<br>5.7             | 29         | 0<br>5.0<br>8.5                            | 18.7<br>18.6                                |
|      | 24.0  | 10.0  |          | 50.0   | 5.9                                  |            | 8.5  | 18.0  |
|      | 25.0  | 8.0   |          | 30.0<br>33.0                                       | 5.7                                  |            | 16.0                                       | 17.8  |
|      | 31.0<br>41.0  | 5.7<br>4.8<br>4.6                             |          | 41.0<br>47.0                                       | 4.9<br>4.6                           |            | 20.0                                       | 9.0   |
|      | 41.0<br>47.0  | 4.6   |          | 81.0   | 4.0                                  |            | 22.0<br>26.0                               | 5.9   |
|      | 83.0  | 4.2   |          | 06.21.87   | 917 11                               |            | 37.0                                       | 4.8   |
| 43°  | 07.7', 87   | 09.31   | 25       | 0  | 19.9                                 |            | 46.0                                       | 9.0<br>2.98<br>3.98<br>3.98                 |
| 21   | 0   | 19.6  |          | 1.5  | 19.3                                 |            | 76.0<br>95.0                               | 3.9   |
|      | .50.55.55.0.5.5<br>16.66.8.2.55.0.5.5<br>22.35.80.580 | 19.6<br>18.8<br>17.9<br>17.4<br>16.56<br>75.9 |          | 1.5<br>15.5<br>20.5<br>21.0                        | 19.9<br>19.3<br>18.5<br>12.6<br>11.8 |            | 14 51 87°                                  | 20 81                                       |
|      | 16.5  | 17.4  |          | 21.0   | 11.8                                 | 30         | 3.0<br>9.0<br>13.0                         | 19.0<br>19.0<br>18.3<br>18.1<br>17.4        |
|      | 18.5<br>22.5  | 16.5  |          | 25.5<br>29.0<br>31.0                               | 7.9<br>7.56<br>5.8                   |            | 3.0  | 19.0  |
|      | 25.5  | ( • O<br>5 · O                                |          | 31.0   | 6.5                                  |            | 13.0                                       | 18.1  |
|      | 36.ó  | 4.7   |          | 37.5   | 5.6<br>4.8                           |            | 15.0                                       | 17.4  |
|      | 25.5<br>36.0<br>58.5<br>80.5                          | 4.5   |          | 46.5   | 4.8                                  |            | 16.0                                       | 16.7  |
| 43°  | 07 21 87  | °11.8'  |          | 37.5<br>46.5<br>58.5<br>81.5                       | 4.4<br>4.2                           |            | 18.0                                       | 8.7<br>7.0                                  |
| 22   | 07.21,87<br>0<br>2.0<br>6.0<br>8.0<br>13.0            | 19.9<br>19.0                                  | 43°C     | 05.91, 87  | 7010 /11                             |            | 19.5<br>25.5<br>30.0                       |   |
|      | 2.0   | 19.0  | 26<br>26 | Λ.   | 19.6                                 |            | 30.0                                       | 5.2   |
|      | 6.0   | 18.4  |          | 0<br>1.5<br>4.5                                    | 19.3                                 |            | 66.0<br>91.0                               | 5.7<br>5.2<br>4.0<br>3.8                    |
|      | 13.0  | 17.9<br>17.6                                  |          | 1.5<br>4.5<br>14.5<br>15.5<br>17.5<br>18.5<br>21.0 | 19.6<br>19.3<br>18.9<br>18.5<br>18.2 | 43°0       | 0/1 01 87                                  | ०उउ गा                                      |
|      | 16.0  | 16.9  |          | 15.5   | 18.2                                 | 31         | 3.0  | 19.4<br>19.4<br>18.9<br>18.7                |
|      | 20.0<br>21.0  | 13.0  |          | 17.5   | 14.0<br>12.7                         |            | 3.0  | 19.4  |
|      | 23.0  | 7.6   |          | 21.0   | 9.5                                  |            | 6.0  | 18.7  |
|      | 25.0  | 6.6   |          | 33.5   | 6.1                                  |            | 15.0                                       | 18.3  |
|      | 29.0  | 5.6   |          | 49.5   | 9.5<br>6.1<br>4.8<br>4.6             |            | 16.5<br>18.0                               | 13.9<br>11.9                                |
|      | 32.0<br>41.5  | 16.9<br>13.8<br>76.6<br>55.4<br>8             |          | 33.5<br>49.5<br>55.5<br>80.5                       | 4.3                                  |            | 19.5                                       | 13.9<br>11.9<br>7.0                         |
|      | 43.0  | 4.5<br>4.1                                    | 43°0     | 15 71 X7   | °21.6'                               |            | 19.5<br>27.0                               | 5.4<br>4.8                                  |
| 1120 | 79.0  | 4.1   | 27       | 0 -  | 19.1                                 |            | 33.0<br>60.0                               | 4.8   |
| 23   | 07.01, 87   | °13.31<br>20.0                                |          | 2.5<br>3.0<br>8.0                                  | 19.1                                 |            | 85.5                                       | 3.9   |
| -5   | 0<br>0.5<br>2.0                                       | 19.3<br>19.0<br>18.6                          |          | 8.0  | 18.9<br>18.4<br>18.3                 | 43°0       | 02 61 07                                   | °36.4i'                                     |
|      | 2.0<br>7.0  | 19.0  |          | 15.0<br>18.0                                       | 18.3<br>15.0                         | 32         | 03.0<br>3.0<br>6.0<br>16.5<br>17.5<br>18.0 | 19.1<br>19.1                                |
|      | Ŕ۸  | 18.2  |          | 19.0   | 14.0                                 |            | 5.0  | 19.1  |
|      | 15.5<br>20.5<br>21.5<br>23.0                          | 18.2<br>17.6                                  |          | 23.0   | 9.5<br>7.2                           |            | 16.5                                       | 18.6  |
|      | 20.5  | 10.2  |          | 29.0   | 7.2                                  |            | 17.5                                       | 17.9  |
|      | 21.5  | 7.0   |          | 35.0<br>36.0                                       | 6.0<br>5.2                           |            | 19.0                                       | 11.9  |
|      | 25.5  | 10.2<br>9.6<br>7.2<br>6.2                     |          | 39.0<br>66.5                                       | 4.9                                  |            | 20.0                                       | 17.9<br>11.9<br>8.4<br>7.7                  |
|      | 31.0  | 5.5<br>5.1<br>4.6<br>4.6                      |          |  | 4.7                                  |            | 25.5                                       |   |
|      | 38.0<br>43.0  | 5.1   | 28<br>28 | 05.3', 87  | °23.6'                               |            | 36.0<br>52.0                               | 5.4<br>4.6<br>4.2                           |
|      | 47.0  | 4.6   | 20       | 2  | 19.1<br>19.1<br>18.8                 |            | 52.0<br>55.0<br>78.0                       | 4.2   |
|      | 47.0<br>77.0  |   |          | 2.5  | 18.8                                 | 100        | 78.0                                       | /L O  |
| 43°  | 06.71, 87   | °15.31<br>20.0                                |          | 0<br>2.5<br>13.5<br>16.5<br>23.5<br>26.5           | 18.4<br>14.6                         | 43°0<br>33 | 03.2', 87                                  | 19.0<br>19.0<br>19.0<br>18.9<br>18.6<br>9.3 |
|      | 0<br>2.0<br>7.0                                       | 19.3  |          | 23.5   | 7.0                                  | 23         | 6.0  | 19.0  |
|      | 7.0   | 19.3<br>18.7<br>18.4                          |          | 26.5   | 5.1<br>4.6                           |            | 9.0<br>17.0                                | 18.9  |
|      | 14.5<br>17.0  | 17.8  |          | 50.5   | 4.0                                  |            | 17.0                                       | 9.3   |
|      | 11.0  | 41.0  |          |  |                                      |            |  |   |

| Slide<br>No. | Depth,M<br>Corr.             | Temp.°C                  | Slide<br>No. | Depth,M<br>Corr. | Temp.°C | Slide<br>_No. | Depth,M | Temp.°C |
|--------------|------------------------------|--------------------------|--------------|------------------|---------|---------------|---------|---------|
| 33           | 21.0<br>24.0<br>31.5<br>53.0 | 7.2<br>6.6<br>5.9<br>4.7 |              |                  |         |               |         |         |
|              | 60.0<br>63.0                 | 4.6<br>4.3<br>4.1        |              |                  |         |               |         |         |
| 43°          | 02.91, 87                    |                          |              |                  |         |               |         |         |
| 34           | 1.0<br>6.0<br>10.0<br>13.0   | 18.9<br>18.5<br>18.4     |              |                  |         |               |         |         |
|              | 19.0                         | 18.3                     |              |                  |         |               |         |         |
|              | 21.0<br>22.0                 | 17.9<br>16.6             |              |                  |         |               |         |         |
|              | 23.0<br>24.0                 | 10.6<br>8.2<br>6.6       |              |                  |         |               |         |         |
|              | 29.0<br>37.0                 | 6.6<br>5.7<br>5.1<br>4.7 |              |                  |         |               |         |         |
|              | 39.0<br>43.0                 | 5.1                      |              |                  |         |               |         |         |
| 43°          | 43.0<br>57.0<br>02.4', 87    | °44.8'                   |              |                  |         |               |         |         |
| 35           | 7.5<br>9.5<br>24.0           | 20.1<br>20.0             |              |                  |         |               |         |         |
|              | 9.5                          | 19.7                     |              |                  |         |               |         |         |
|              | 24.0<br>25.0                 | 18.9<br>18.5<br>10.5     |              |                  |         |               |         |         |
|              | 25.0<br>26.5<br>28.0         | 10.5                     |              |                  |         |               |         |         |
|              | 29.5                         | 8.0<br>7.5<br>6.8        |              |                  |         |               |         |         |
|              | 30.5                         | 6.8                      |              |                  |         |               |         |         |
|              | 32.5<br>45.0                 | 6.0<br>5.7<br>°47.6      |              |                  |         |               |         |         |
| 43°<br>36    | 02.11, 87                    | 20.5                     |              |                  |         |               |         |         |
|              | 9.0<br>11.0                  | 20.5<br>20.5<br>20.4     |              |                  |         |               |         |         |
|              | 11.5                         | 19.9<br>19.8             |              |                  |         |               |         |         |
|              | 12.5<br>17.0                 | 19.8<br>19.6             |              |                  |         |               |         |         |
|              | 21.0                         | 19.4                     |              |                  |         |               |         |         |
|              | 22.5<br>23.0                 | 19.2<br>18.9             |              |                  |         |               |         |         |
| 43°          | 27.0                         | 18.6                     |              |                  |         |               |         |         |
| 37           | 01.8', 87                    | 20.6                     |              |                  |         |               |         |         |
|              | 0<br>5.5<br>6.5              | 20.6<br>20.4             |              |                  |         |               |         |         |
|              | 18.0                         | 20.3                     |              |                  |         |               |         |         |

# Grand Haven to Milwaukee

| Slide | Depth,M                              | Temp.°C                                      | Slide      | Depth,M                         | Temp.°C   | Slide      | Depth,M              | Temp,°C   |
|-------|--------------------------------------|--|------------|---------------------------------|---|------------|----------------------|---|
| No.   | Corr.                                | Corr.  | No.<br>144 | Corr.                           | Corr.   | No.<br>149 | Corr.<br>21          | Corr.   |
| 43°   | 03.41, 86                            | 18.01  | 144        | 40                              | 4.7   | 149        | 51                   | 16.3  |
| 141   | 0                                    | 19.3   |            | 44                              | 4.4   |            | 22                   | 11.3  |
|       | 10<br>14                             | 19.3   |            | 55                              | 4.1   |            | 23                   | 7.8   |
|       | 14                                   | 19.3<br>19.3<br>19.1                         | 43°        | 02.71, 86                       | 26.81   |            | 27                   | 5.8   |
|       | 15<br>18                             | 18.5<br>18.4                                 | 145        | 0                               | 18.8  |            | 29                   | 5.3   |
|       | 18                                   | 18.4   |            | 7                               | 18.7  |            | 31                   | 4.8   |
|       | 19<br>20                             | 18.1<br>18.1                                 |            | 10                              | 18.4  |            | 36                   | 16.3<br>11.3<br>7.8<br>5.8<br>5.3<br>4.5<br>4.4 |
|       | 20                                   | 18.1   |            | 16                              | 15.4  |            | 45                   | 4.4   |
|       | 22                                   | 17.5<br>16.6<br>16.3<br>16.2                 |            | 18<br>19<br>22                  | 13.0  | 43         | 86 , 10، 20°         | 38.21   |
|       | 23<br>25                             | 16.6   |            | 19                              | 12.2  | 150        | 0<br>16              | 19.3<br>19.2                                    |
|       | 25                                   | 16.3   |            | 22                              | 11.9  |            | 16                   | 19.2  |
| 100   | 27                                   | 16.2   |            | 27<br>32                        | 6.2   |            | 17                   | 19.0  |
| 142   | 03.21, 86                            | °19.8'                                       |            | 32                              | 11.9<br>6.2<br>5.1<br>4.8<br>4.4                  |            | 20                   | 18.4  |
| 142   | 10                                   | 18.7   |            | 37<br>40                        | 4.8   |            | 22                   | 18.0  |
|       | 0<br>15<br>16                        | 10.7   |            | 58                              | 4.4   |            | 23<br>25             | 12.4  |
|       | 17                                   | 10.5   | 1120       | 02.61, 86                       |   |            | 27                   | 1.2   |
|       | 21                                   | 18.3<br>17.1<br>16.8                         | 146        | 0 0                             | 18 0  |            | 30                   | 7.2<br>6.2<br>5.8<br>4.7<br>4.4                 |
|       | 24                                   | 15.1   | 170        | 11                              | 18.9<br>18.7<br>18.4                              |            | 37                   | J. 7  |
|       |                                      | 14.0   |            | 12                              | 18.4  |            | 37<br>60             | $\frac{1}{1} \cdot \int_{\Gamma}$               |
|       | 29                                   | 77 0   |            | 12<br>16                        | 12.2  |            | 85                   | 4.4   |
|       | 30                                   | 10.3   |            | 21                              | 6.9   | 43°        | 01.91.86             |   |
|       | 25<br>29<br>30<br>33<br>37<br>41     | 10.3<br>9.1<br>8.9<br>8.0<br>6.3             |            | 24                              | 12.2<br>6.9<br>5.4<br>4.7                         | 151        | 0<br>10<br>14        | 19.2  |
|       | 37                                   | 8.9  |            | 34<br>44                        | 4.7   |            | 10                   | 10 1  |
|       | 4i                                   | 8.0  |            | 44                              | 4.2   |            | 14                   | 19.0<br>18.4                                    |
|       | 43<br>. 45                           | 6.3  |            | 59                              | 4.2   |            | 18                   | 18.4  |
|       | . 45                                 | 7.1  | 43°        | 02.51, 86                       | 31.3  |            | 21                   | 18.2  |
|       | 02.91, 86                            | °22.31<br>18.1<br>18.0<br>17.8               | 147        | 0<br>13<br>15<br>16<br>18<br>21 | 19.0  |            | 22                   | 18.38649555<br>146554444<br>44.4                |
| 143   | 0<br>14<br>16.2                      | 18.1   |            | 13                              | 18.8  |            | 24                   | 6.8   |
|       | 14                                   | 18.0   |            | 15                              | 18.5  |            | 27                   | 5.6   |
|       | 16.2                                 | 17.8   |            | 16                              | 15.3  |            | 30<br>33<br>46       | 5.4   |
|       | 17                                   | 15.7   |            | 18                              | 8.8   |            | 33                   | 4.9   |
|       | 20                                   | 14.4   |            | 51                              | 6.9   |            | 46                   | 4.5   |
|       | 21                                   | 13.7   |            | 27                              | 5.7   |            | 60                   | 4.5   |
|       | 22.5                                 | 13.0   |            | 36                              | 19.0<br>18.5<br>18.5<br>15.3<br>6.9<br>7.3<br>6.9 | 1130       | 69<br>01.81,86       |   |
|       | 22.5<br>23<br>28                     | 11.0<br>7.9                                  |            | 32<br>36<br>40<br>60            | 4.0   | 43°<br>152 | 01.81, 86            | 42.71   |
|       | 32                                   | 7.9<br>6.2<br>4.7                            |            | 60                              | λ З   | عزد        | 10                   | 19.2<br>19.1                                    |
|       | 32<br>39                             | 4.7  | 43°        | 02,4', 86                       | °33.5'  |            | 14                   | 19.1  |
|       | 54                                   |  | 148        | 0 00                            | 19.0  |            | 17                   | 18.6  |
|       | 54<br>60                             | 4.5<br>4.5<br>4.3                            | _ 10       | 13                              | 18.8  |            | 19                   | 18.3  |
|       | 65                                   | 4.3  |            | 0<br>13<br>16                   | 18.2  |            | 22                   | 17.8  |
| 43°   |                                      |  |            | 17                              | 19.0<br>18.8<br>18.2<br>17.2                      |            | 19<br>22<br>23<br>26 | 19.6.3.8<br>18.7.9.6.5.5.6.4<br>4.4.4<br>4.4.4  |
| 144   |                                      | 18.6<br>18.6<br>17.9<br>17.8<br>16.8<br>13.6 |            | 17<br>20                        | 7.7   |            | 26                   | 6.5   |
|       | 0<br>7<br>13<br>15<br>18<br>20<br>21 | 18.6   |            | 21                              | 6.7   |            | 57                   | 6.3   |
|       | 13                                   | 17.9   |            | 27                              | 6.7<br>5.1<br>4.2<br>4.2                          |            | 30                   | 5.6   |
|       | 15                                   | 17.8   |            | 29                              | 5.1   |            | 30<br>32<br>39<br>60 | 5.5   |
|       | 18                                   | 16.8   |            | 39<br>44                        | 4.3   |            | 39                   | 4.6   |
|       | 20                                   | 13.6   |            |                                 | 4.2   |            | 60                   | 4.4   |
|       | 22                                   | 15.0   |            | 60<br>67                        | 4.2<br>4.2  |            | 76<br>86             | 4.3   |
|       | 55                                   | 10.6   | 43°        | 02.21, 86                       |   | 43°        |                      | 4.4   |
|       | 23<br>25<br>28                       | 10.0<br>7.8<br>6.2<br>5.3<br>4.8             | 149        | UE, 2', 00                      | 35.81   | 153        | 01.7', 86            | 19.2<br>19.2                                    |
|       | 28                                   | 6.3  | エサフ        | 0                               | 19.1  | エンン        | ŏ                    | 19.2  |
|       | 31                                   | 5 3  |            | 15                              | 19.1<br>19.1<br>18.8<br>17.8                      |            | 0<br>9<br>12         | 10 1  |
|       | 31<br>36                             | 4°8  |            | 15<br>_19                       | 17.8  |            | 15                   | 19.1  |
|       |                                      | 1.0  |            |                                 | 2100  |            |                      | 40.7  |

| Slide      | Depth,M<br>Corr.         | Temp.°C<br>Corr.   | Slide<br>No. | Depth,M<br>Corr.                                    | Temp.°C<br>Corr.   | Slide<br>No. | Depth,M<br>Corr.                 | Temp.°C<br>Corr.   |
|------------|--------------------------|--|--------------|---|--|--------------|----------------------------------|--|
| No.<br>153 | 18                       | 18.4   | 43           | °01.3', 86  |  | 160          | 82                               | 4.5  |
| 1)3        | 22                       | 17.7   | 157          | 0   | 19.3   | 43           | 00.61.87                         | 03.01  |
|            | 23<br>27<br>28           | 12 4   |              | 0<br>7<br>16  | 19.3<br>19.3<br>19.4<br>17.5<br>13.3<br>65.4<br>4.6<br>3.4<br>4.3<br>4.3 | 43°<br>161   | 0 7                              | 19998819853966<br>11985375444  |
|            | 27                       | 9.4<br>7.4<br>6.4  |              | 16  | 19.2   |              | 7                                | 19.5   |
|            | 28                       | 7.4  |              | 19  | 18.4   |              | 13                               | 19.3   |
|            | 30                       | 6.4  |              | 23  | 17.5   |              | 15                               | 18.6   |
|            | 36                       | 5.3<br>4.7   |              | 19<br>23<br>25<br>28                                | 13.3   |              | 19                               | 18.1   |
|            | 30<br>36<br>42           | 4.7  |              | 28  | 8.3  |              | 23                               | 16.9   |
|            | 45                       | 5.3<br>4.7<br>4.6<br>4.4   |              | 30<br>33<br>34                                      | 6.3  |              | 15<br>19<br>23<br>25<br>27       | 13.8   |
|            | 60                       |  |              | 33  | 5.4  |              | 27                               | 7.5  |
|            | 96                       | 4.3  |              | 34  | 4.9  |              | 3i                               | 5.3  |
| 43         | °01.6', 86               | 47.4   |              | 37  | 4.6  |              | 33                               | 4.9  |
| 154        | 0<br>13<br>16<br>18      | 19.3   |              | 60<br>86  | 4.3  |              | 33<br>60<br>78                   | 4.5  |
|            | 13                       | 19.3   |              |   | 4.2  |              | 78                               | 4.6  |
|            | 16                       | 19.2   | 43           | °01.1', 86  | 19.3<br>19.2<br>19.1<br>18.7   | 43           | 00.41, 87                        | 7°05,51  |
|            | 18                       | 19.0   | 158          | 0<br>12<br>15<br>17                                 | 19.3   | 162          | 0<br>4<br>9<br>15<br>16          | 19.8   |
|            | 20                       | 10.0   |              | 75  | 19.2   |              | 4                                | 19.0   |
|            | 23                       | 10.1   |              | 12  | 19.1   |              | 39                               | 19.0   |
|            | 25<br>26                 | 12.4   |              | 7.1   | 15.9   |              | 15                               | 19.0   |
|            | 28                       | 9.4  |              | 23<br>26  | 10.4   |              | 21                               | 18.0   |
|            | 29                       | 6.9  |              | 20  | 6.6  |              | 24                               | 16.6   |
|            | 35                       | 5.6  |              | 30  | 6.2  |              | 27                               | 12.3   |
|            | 35<br>36                 | 5.3  |              | 33  | 5.4  |              | 28                               | 7.1  |
|            | 43                       | 1.6  |              | 35  | 4.6  |              | 31                               | 6.1  |
|            | 60                       | 4.5  |              | 29<br>30<br>33<br>35<br>42                          | 4.5  |              | 33                               | 5.4  |
|            | 60<br>88                 | 1993.206.144.926.365.4<br>1999.888.4.4.926.365.4.4.                |              | 60  | 15.9462465555<br>10665445555   |              | 27<br>28<br>31<br>33<br>35<br>44 | 4.7  |
| 43         | 01.51.86                 | 49.51  |              | 60<br>67  | 4.5  |              | 44                               | 705.51.86<br>19.86<br>19.66<br>19.66<br>18.66.3<br>16.6.3<br>17.6.1.4<br>4.55.4<br>4.4 |
| 155        | 0                        | 19.51<br>19.3<br>19.6<br>18.3<br>17.4<br>17.2<br>5.6<br>5.5<br>5.7 | 43           | 01.01, 86   | 19.3<br>19.3<br>19.2<br>18.5<br>17.8<br>13.4                             |              | 60                               | 4.5  |
|            | 16                       | 19.1   | 159          | 0   | 19.3   |              | 76                               | 4.4  |
|            | 17                       | 18.6   |              | 10  | 19.3   | 43           | °00.31, 8                        | 7°07.6'  |
|            | 20                       | 18.3   |              | 14  | 19.2   | 163          | 0                                | 20.0   |
|            | 22                       | 17.4   |              | 18  | 18.5   |              | 10<br>13<br>17                   | 19.9   |
|            | 24                       | 11.4   |              | 21<br>25<br>27                                      | 17.8   |              | 13                               | 19.6   |
|            | 27                       | 7.2  |              | 25  | 13.4   |              | 17                               | 19.2   |
|            | 34                       | 5.6  |              | 27  | 9.4<br>7.2<br>6.4  |              | 19                               | 18.7   |
|            | 37                       | 2.5  |              | 29  | 7.2  |              | 25                               | 16.3   |
|            | 38                       | 5.0  |              | 30<br>32  | 6.4  |              | 30                               | 6.6  |
|            | 39                       | 4.7  |              |   | 5.7<br>5.0   |              | 32                               | 5.4  |
|            | 49<br>60                 | 4.6<br>4.4   |              | 33<br>36  | 2.0  |              | 19<br>25<br>30<br>33<br>35<br>43 | 5.2  |
|            | 78                       | 4.4  |              | 60  | 7.6  |              | 60                               | 5.0  |
| 43         | °01.4°, 86               |  |              | 84  | 4.7<br>4.6<br>4.6  |              | 78                               | 7°07.6!<br>20.0<br>19.6<br>19.6<br>19.2<br>18.7<br>16.8<br>5.0<br>5.0<br>4.6           |
| 156        |                          | 19.3   | 43           |   | 7°00.8   | 43           | 000 01 0                         | 7°09.81  |
|            | 0<br>9<br>15<br>17<br>20 | 19.3<br>19.2   | 160          | 0,  | 19.4   | 164          | 00.21, 6                         | 20.0   |
|            | 15                       | 19.0   |              | 0<br>5<br>8<br>14                                   | ול מר  | 201          | 0<br>3<br>7<br>13                | 19.8   |
|            | īź                       | ī8.5   |              | 8   | 19.2<br>18.9<br>18.6   |              | 7                                | 19.8   |
|            | 20                       | 18.1   |              | 14  | 18.9   |              | 13                               | 19.4   |
|            | 22                       | 17.3   |              | 15  | 18.6   |              | 19                               | 18.9   |
|            | 24                       | 13.3   |              | 17  | 18.4   |              | 19<br>22<br>25<br>27             | 16.5   |
|            | 25<br>26<br>28           | 11.8   |              | 18  | 18.0   |              | 25                               | 14.5   |
|            | 26                       | 8.8  |              | 23  | 16.8   |              | 27                               | 9.6  |
|            | 28                       | 7.3  |              | 25  | 14.3   |              | 29<br>32                         | 7.8  |
|            | 31                       | 6.2  |              | 26  | 10.3   |              | 32                               | 5.4  |
|            | 32                       | 19.0<br>18.5<br>18.1<br>17.3<br>13.8<br>8.3<br>6.8<br>7.6<br>4.4   |              | 27  | 8.8  |              | 35<br>40                         | 5.1  |
|            | 39                       | 4.4  |              | 28  | 8.0  |              | 40                               | 4.9  |
|            | ŞΤ                       | 4.4  |              | 30<br>16  | 5.1  |              | 60                               | 7°09.84.4.95.568.4.1.96.5  |
|            | 60<br>78                 | 4.3<br>4.3   |              | 15<br>17<br>18<br>23<br>25<br>27<br>28<br>346<br>60 | 14.3<br>10.3<br>8.8<br>8.0<br>5.1<br>4.5                                 |              | 79                               | 4.5  |
|            | 10                       | 4.3  |              | 00  | 4.5  |              |                                  |  |

| Slide<br>No.   | Depth,M  | Temp.°C<br>Corr.   | Slide<br>No.                            | Depth,M<br>Corr.                                    | Temp.°C<br>Corr.   | Slide<br>No. | Depth,M  | Temp.°C<br>Corr.   |
|----------------|--|--|---|---|--|--------------|--|--|
|                | 00.0°, 87<br>0<br>2<br>3<br>12<br>17<br>20<br>25<br>27                 | 20.1<br>20.0<br>19.9<br>19.7<br>18.9<br>15.7   | No.<br>169<br>42°<br>170                | 17<br>19.5<br>22.5<br>29<br>48<br>60<br>84          | 18.3<br>14.0<br>9.6<br>5.3<br>4.3<br>4.2   | 173          | 758.7°, 87<br>0<br>1<br>7<br>13<br>19<br>21<br>23<br>26.5        | Corr.<br>30.31<br>20.4<br>20.0<br>19.8<br>19.5<br>19.0<br>17.3<br>10.1<br>6.1                      |
| 42°            | 34<br>60<br>80<br>59.9°, 87<br>0<br>3<br>15<br>16                      | 6.3<br>5.1<br>4.5<br>4.5<br>19.5<br>19.2<br>19.0<br>18.6   |   | 0<br>2<br>6<br>12<br>18<br>18,5                     | 19.3<br>19.0<br>18.2   |              | 34<br>40<br>46<br>60<br>86<br>58.61, 87                          | 6.1<br>5.0<br>4.7<br>4.6<br>4.1<br>32.7  |
|                | 17.5<br>19<br>22<br>24<br>26<br>28                                     | 19.6<br>18.7<br>11.8<br>11.8<br>17.0<br>11.9<br>17.0<br>19.5<br>19.5   |   | 20<br>23<br>26<br>27<br>28<br>31<br>33<br>39        | 5,845,0941854<br>173,988655444   | al.g t       | 0 3 9 14 18 19 5 21 24   | 20.3<br>19.8<br>19.8<br>18.4<br>18.2<br>14<br>8.5<br>7.0<br>65.1<br>4.3<br>4.1                     |
| 42°            | 29<br>32<br>60<br>84<br>59 • 7 • 87 °                                  | 4.1<br>4.0   | 42°<br>171                              | 79<br>59.0°, 87<br>0<br>6<br>10<br>13<br>16         | 25.81  |              | 36<br>44<br>46<br>60<br>75                                       |  |
| <del>42°</del> | 59.7; 87<br>0 3<br>11<br>18<br>22.5<br>24.5<br>24.5<br>31<br>60<br>78  | 19.7<br>19.3<br>19.1<br>17.7<br>97.8<br>55.5<br>4.6<br>4.3   |   | 16<br>19<br>21<br>22<br>25<br>31<br>37<br>43<br>460 | 20°04<br>1994<br>1987<br>1885<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778<br>11778 | 175          | 758.51, 87<br>0.5<br>2<br>10<br>13<br>16<br>20<br>23<br>25<br>28 | 735.1;<br>20.6<br>20.6<br>19.5<br>19.4<br>18.7<br>18.8<br>7.7<br>5.2<br>4.6<br>4.5                 |
| 168            | 0<br>5<br>12<br>16.5   | 19.7<br>19.4<br>19.2<br>18.6<br>18.1<br>9.9  | 172                                     | 85<br>58.91, 87<br>0<br>2<br>4                      | 3.9  | 42.          | 37<br>43<br>46<br>60<br>62<br>38,31,87                           | 6.7<br>5.8<br>4.6<br>4.5<br>4.5  |
| <del></del>    | 17<br>21<br>23<br>25<br>27.5<br>30<br>33<br>36<br>60<br>72<br>59.3, 87 | 4.9<br>4.4<br>4.4  |   | 701056934471435083                                  | 20,38,65,38,65,38,65,38,65,38,65,38,65,44,44,44,44,44,44,44,44,44,44,44,44,44  | 176          | 0<br>136<br>8<br>108<br>120<br>225<br>236                        | 37.21<br>20.6<br>19.8<br>19.5<br>19.5<br>19.3<br>19.3<br>18.8<br>18.1<br>14.6<br>7.0<br>6.4<br>5.3 |
| -              |  | ann ann an Aire ann an Air | *************************************** | 83<br>6A  | 4.0<br>3.9   |              |  |  |

| Slide      | Depth, M                     |                |
|------------|------------------------------|----------------|
| No.        | Corr.                        | Corr.          |
| 176        | 39<br>48                     | 4.7            |
| 42         |                              | 4.5            |
| 177        | '58.2¹, 87                   | °39.5'<br>20.7 |
| 711        | 1                            | 20.1           |
|            | 7                            | 20.1           |
|            | ٥                            | 19.9           |
|            | 21                           | 18.7           |
|            | 22.5                         | 13.6           |
|            | 24                           | 8.6            |
|            | 26                           | 7.1            |
|            | 31                           | 5.8            |
|            | 34                           | 5.1            |
|            | 42                           | 4.8            |
| 42°<br>178 | 758.1, 87                    | 41.71          |
| 110        | 2                            | 20.7<br>20.1   |
|            |                              | 19.6           |
|            | 19.5                         | 18.4           |
|            | 22                           | 9.6            |
|            | 15<br>19.5<br>22<br>23<br>24 | 6.4            |
|            |                              | 5.8            |
| 100        | 33<br>57.91,87               | 5.4            |
| 179        | 57.9', 87<br>0               | 20.8           |
| 119        | 1                            | 20.6           |
|            | 2                            | 20.3           |
|            | 15                           | 19.7           |
|            | 19<br>20                     | 14.7           |
|            | 20                           | 10.2           |
|            | 21.5                         | 7.2            |
|            | 23<br>26                     | 6.7            |
| 42°        | 26<br>57.71.87               | 6.7            |
| 180        | 57.71, 87                    | 20.9           |
| 100        | 2                            | 20.4           |
|            | 4                            | 20.1           |
|            | 12                           | 19.7           |
|            | 15                           | 18.7           |
|            | 16                           | 16.7           |
|            | 18                           | 13.5           |
|            | 20                           | 7.9            |
|            | 22<br>23                     | 7.5            |
|            | 4.5                          | 7.4            |

Slide Depth,M Temp.°C No. Corr. Corr.

Slide Depth, M Temp. Corr.

Temp.°C

### Grand Haven to Milwaukee 3 November 1962

|                | pth,M<br>orr.  | Temp.°C              | Slide<br>No. | Depth,M  | Temp, °C  | Slide<br>No. | Depth,M<br>Corr.                 | Temp.°C  |
|----------------|--|----------------------|--------------|--|---|--------------|----------------------------------|--|
| 43°03.         | 51, 86°  | 18.01                | 310          | '03.3°, 86   | 29.81   | No.<br>314   | 16                               | 10.2   |
| 309            | 0<br>2<br>16   | 12.8<br>12.8<br>12.8 | 510          | 0<br>4   | 12.5<br>12.5<br>12.4  |              | 25<br>31<br>38                   | 10.06<br>5.24<br>4.27  |
| 43.03          | 41.86  | 12.8                 |              | 19<br>33<br>35<br>38<br>39<br>41                   | 12.0  |              | 38<br>40                         | 9.5  |
| 306            | 0<br>2<br>25<br>26   | 13.0                 |              | 35   | 11.3  |              | 41<br>44                         | 6.4  |
| 4              | 25   | 13.0<br>13.0         |              | 39   | 6.4   |              | 47                               | 5.4<br>5.2<br>4.7  |
| á              | 26<br>25   | 12.7                 |              | 41<br>44   | 6.9<br>6.4<br>5.1<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4<br>9.4 |              | 52<br>89                         | 4.7  |
| :              | 35<br>37   | 12.5<br>12.1         |              | 79   |   | 43°          | '03.01. 86                       | 71 71  |
| 43°03.         | 41<br>31,86°   | 12.1                 | 43°          | 03.2°, 86  | 12.5  | 315          | 0                                | 10.8<br>10.8<br>10.7   |
| 307            | 0<br>2<br>26   | 12.8<br>12.8<br>12.8 | J            | 0<br>1<br>11                                       | 12.5<br>12.5<br>12.5<br>12.2  |              | 21<br>26                         | 10.7   |
| :              | 26   | 12.8                 |              | 16   | 12.2  |              | 32<br>41                         | 10.5   |
|                | 32<br>40   | 12.7<br>11.7         |              | 21   | 12.2<br>12.0  |              | 41<br>44                         | 9.5  |
| į              | 43   | 11.4                 |              | 27   | 11.7  |              | 47<br>81                         | 5.2  |
|                | 43<br>45<br>45<br>45<br>45<br>45<br>45<br>55<br>55<br>55<br>55<br>55<br>55 | 10.9<br>10.6         |              | 16<br>21<br>23<br>27<br>31<br>38<br>41<br>42<br>46 | 11.7<br>9.0<br>8.0  |              | 81<br>99                         | 10.452255<br>10.9654.55                                      |
| !              | 50   | 10.1                 |              | 41   | 7.2<br>6.0  | 43°          | 03.01, 86                        | · · · · · · · · · · · · · · · · · · ·                        |
|                | 56<br>56   | 9.6<br>8.1<br>6.3    |              | 46   | 5.5   | 316          | 0 4                              | 10.6<br>10.6   |
| į              | 58.5   | 8.1<br>6.3<br>6.0    |              | 53<br>57<br>80                                     | 5.5<br>5.0<br>4.3   |              | 41<br>42                         | 10.5   |
|                | 69   | 4.3                  |              | 86   | 4.0   |              | 46                               | 5.1  |
| 43°03.4<br>308 | 41, 86°<br>0<br>4  | 25.1'<br>12.3        | 43°<br>312   | '03.21, 86<br>0                                    | 12.2<br>12.2  |              | 48<br>105                        | 10.5<br>8.1<br>5.1<br>4.2                                    |
|                | 4  | 12.3<br>12.3<br>12.2 |              | 0<br>4<br>22                                       | 12.2<br>12.2  | 43°<br>317   |                                  | 10.6   |
|                | 19<br>25<br>26   | 12.1                 |              | 27   | 12.0  | 211          | 4<br>22                          | 10.6   |
| 2              | 26<br>37   | 12.0<br>11.7         |              | 27<br>32<br>37<br>44                               | 9.3<br>9.1<br>8.4   |              | 22<br>37                         | 10.6   |
| Ž              | 37<br>42<br>44 . 5   | 11.7<br>9.8          |              | 44<br>49   | 8.4   |              | 37<br>46                         | 10.4<br>10.4<br>10.4<br>10.4<br>10.4<br>10.4<br>10.4<br>10.4 |
|                | 44.5<br>45<br>48   | 9.1                  | 43           | 03.1', 86  | 937 11  |              | 54<br>57<br>61                   | 7.4<br>5.6   |
|                | 48<br>55   | 7.6                  | 313          | 0<br>4   | 11.8<br>11.8<br>11.8  |              | 61                               | 5.2  |
| 100000         | 55<br>72   | 4.3                  |              | 11   | 11.8  | -            | 77<br>101                        | 4.5  |
| 43°03.3<br>309 | 31, 86°<br>0   | 27.5°<br>12.4        |              | 17<br>22<br>26                                     | 11.5<br>11.0  | 318          | 02.91, 86                        | 10.3   |
|                | 3  | 12.4<br>12.3         |              | 26   | 10.5  | •            | 0<br>4<br>22                     | 10.3   |
|                | 0<br>3<br>18<br>23<br>30<br>33<br>35                                       | 12.1                 |              | 30<br>38<br>42                                     | 10.5<br>9.7<br>9.5<br>9.5<br>9.7<br>4.7   |              | 34                               | 10.3   |
|                | 30<br>33   | 12.0<br>11.4         |              | 47   | 8.5<br>4.9  |              | 39<br>45<br>52<br>61<br>66<br>68 | 9.9<br>8.1   |
|                | 35   | 10.3<br>7.3<br>5.2   |              | 51<br>55<br>67                                     | 4.7<br>4.2  |              | 52                               | 7.5  |
| 7              | 37<br>40   | 5.2                  |              | 67<br>67   | 3.9<br>3.8  |              | 66<br>61                         | 6.2  |
|                | 46<br>49   | 4.7                  | 43           | 84<br>'03.1', 86                                   | 39.41   |              | 68<br>69                         | 10.33<br>10.33<br>10.29<br>10.29<br>15.02<br>55.7            |
|                | 49<br>74   | 4.7<br>4.6           | 314          | 0<br>4<br>8  | 10.7<br>10.7  |              | 69<br>84                         | 4.7  |
|                |  |                      |              | . 8  | 10.7  | -            | 99                               | 4.7  |

| Slide<br>No. | Depth,M<br>Corr.                       | Temp.°C                                       | Slide<br>No. | Depth, M<br>Corr.                    | Temp.°C<br>Corr.  | Slide<br>No. | Depth,M<br>Corr.                       | Temp.°C  |
|--------------|--|---|--------------|--------------------------------------|---|--------------|--|--|
| 43           | 02.91,86                               | Corr. 51.3' 10.5 10.5 10.5 2 9.8 8.9 7.6 7.4  | 7130         | 02.71.87                             | 03.21   | 329          | 46                                     | 7.9  |
| 319          | 0,                                     | 10.5  | 324          | 0                                    | 10.0  |              | 50                                     | 5.9  |
| 545          | 0<br>4                                 | 10.5  |              | 4                                    | 10.0  |              | 54                                     | 5.9<br>5.0   |
|              | 22                                     | 10.5  |              | 26                                   | 9.9   |              | 50<br>54<br>78                         | 5.9<br>5.0<br>4.6                                      |
|              | 30                                     | 10.2  |              | 30                                   | 9.9<br>9.6<br>9.4   | 439          | 02.41, 87                              | °17.31   |
|              | 30<br>33<br>37<br>47<br>50<br>52<br>63 | 9.8   |              | 30<br>31                             | 9.4   | 330          | 0                                      | 9.7  |
|              | 37                                     | 8.0   |              | 36                                   | 7 0   | 334          | 4                                      | 9.7  |
|              | 17                                     | 8.3   |              | 36<br>41                             | 7.9<br>4.8  |              | 30                                     | 9.6  |
|              | 50                                     | 7.6   |              | 79                                   | 4 4   |              | 32                                     | 9.2  |
|              | 50                                     | 7 4   | 43           | 200 01 00                            | 05.5  |              | 34                                     | 8.6  |
|              | 63                                     | 5.2   | 325          | 02.71, 07                            | 05.5'<br>10.1   |              | 35                                     | 8.5  |
|              | 96                                     | 5.2<br>5.0                                    | رےر          | ŭ                                    | 10.1  |              | รัล                                    | 6.8  |
| 43           | 200 01 07                              | °53.6†  |              | 31                                   | 10.1<br>10.0<br>8.6   |              | 30<br>32<br>34<br>35<br>38<br>40       | 6.2  |
| 320          | 02.97, 86                              | °53.6'<br>10.2                                |              | 33                                   | 8.6   |              | 42                                     | 5.2  |
| 320          | 0 4                                    | 10.2  |              | 35                                   | 6.0   |              | 42<br>48                               | 4 8  |
|              | 12                                     | 10.2  |              | 0<br>4<br>31<br>33<br>35<br>38<br>40 | 4.9   |              | 79                                     | 77.626582288665448                                     |
|              | īL                                     | 9.8   |              | 40                                   | 4.8   | 43           | 79<br>'02.4', 87                       | 7019.71  |
|              | 12<br>14<br>23<br>29<br>35<br>38<br>45 | 9.6   |              | 75                                   | 4.9<br>4.8<br>4.6   | 331          | 0                                      | 9.8  |
|              | 20                                     | 8.8   | 113          | 02 61 87                             | 007 71  | 554          | 0<br>5<br>25<br>36<br>40<br>43         | 9.8  |
|              | 35                                     | 8.3   | 326          | 16                                   | 99996   |              | 25                                     | 9.8  |
|              | 38                                     | 7 11  | 240          | й                                    | 6.6   |              | 36                                     | 9.7  |
|              | 115                                    | 6.3   |              | 16                                   | á.á   |              | 10                                     | a° å   |
|              | 4)<br>E/I                              | 6.5   |              | 117                                  | 3.3   |              | 713                                    | 8.3  |
|              | 56                                     | 5.5   |              | 41<br>45<br>48                       | 7.1   |              | 50                                     | 5.8  |
|              | 50                                     | 5.0   |              | 718                                  | 6.1   |              | 57                                     | 5.3  |
|              | 54<br>56<br>59<br>79                   | 10.28683430506<br>99887665554                 |              | 51                                   | 5.2   |              | 57<br>73                               | 8888733831<br>999998555                                |
|              | 94                                     |   |              | 76                                   | 5.1   | 43           | 02.47, 87                              |  |
| 43°          | 200 01 00                              |   | 43           | °02.6°, 87                           |   | 332          | 02.7,0                                 | 10 1   |
| 321          | 02.81,86                               | 10.3  | 327          | 02.0, 0,                             | 9 9   | 55-          | 0<br>5<br>14                           | 10.1   |
| . 041        | 0 4                                    | 10.3  | 2-1          | 0<br>4<br>19<br>28<br>34             | 3.0   |              | ıĹ                                     | 10.1   |
|              | 13                                     | 10.3  |              | 10                                   | 3.3   |              | П5                                     | 9.7  |
|              | 13<br>16<br>38<br>42                   | 10.0  |              | 2 <u>ี</u> 8                         | á.k   |              | 50<br>53<br>54                         | 8.0  |
|              | 38                                     | 10.0  |              | 3/1                                  | 9.5   |              | 53                                     | 7.6  |
|              | 710                                    | 3.5   |              | 38                                   | 3.3   |              | 57                                     | 6.8  |
|              | 43                                     | 7.6   |              | 41                                   | 2.2   |              | 52                                     | 5.8  |
|              | 47                                     | 7.0   |              | 72 5                                 | 6.7   |              | 58<br>60                               | 10.1<br>9.7<br>8.0<br>7.6<br>6.8<br>5.8<br>5.3         |
|              | 56                                     | 1.5   |              | 42.5<br>43.5                         | 5.5   | 113,         |  | 7°24.51  |
|              | 56<br>92                               | 4.4   |              | 46                                   | 10.21<br>9.99<br>9.99<br>9.99<br>9.99<br>9.99<br>7.65<br>5.50   | 333          | 702.31, 87                             | 10.1<br>10.1<br>10.1                                   |
| /13          |  | *58.21  |              | 78                                   | 4.8   | 333          | 0.555555555555555555555555555555555555 | 10.1   |
| 322          | 102.81, 86                             | 9.8<br>9.8<br>9.8<br>9.6<br>8.1<br>7.0<br>6.1 | 43           | 78<br>°02.5', 87                     | °12.7'  |              | 75.5                                   | 10.1<br>10.0<br>9.6<br>8.0                             |
|              | 0<br>4                                 | a a   | 328          | 02.51, 87                            | 10.0  |              | 73.5                                   | 10.1   |
|              | 22                                     | a a   | 520          | ĭ                                    | 10.0  |              | 72.2                                   | 10.6   |
|              | 33                                     | á.6   |              | 15                                   | 10 1  |              | 16.5                                   | ă.0  |
|              | 22<br>33<br>43                         | 8.1   |              | 0<br>1<br>15<br>22<br>26             | 10.0  |              | 48.5                                   | 7 4  |
|              | 47                                     | 7.0   |              | 26                                   | 9 8   |              | 50.5                                   | 6.7  |
|              |  | 6.1   |              | 32                                   | á 6   |              | 58.5                                   | 6.7<br>6.3   |
|              | 51<br>53<br>85                         | 5.1   |              | 37                                   | 9.5   | 43           | 02.31, 87                              |  |
|              | ล์ร์                                   | 5.4<br>5.1                                    |              | 40                                   | ă.  | 334          | , 02.                                  | 10.0   |
| 43           | 02.71.87                               | °00.81  |              | 41                                   | 6.8   | 55.          | ŭ                                      | 10.0   |
| 323          | 0, 0,                                  | 10.1  |              | 116                                  | 4.9   |              | 22                                     | 10.0   |
| 5-5          | 0<br>4<br>31<br>35<br>39<br>41         | 10.1  |              | 78<br>'02.5', 87                     | 10.08<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.99<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90<br>10.90 |              | 0<br>4<br>22<br>40<br>43               | 9.8  |
|              | 31                                     | 10.1  | 43           | 02.51, 87                            | °15.11  |              | 43                                     | 9.7  |
|              | 35                                     | 9.8   | 329          | 0                                    | 9.9   |              | 47                                     | 9.j  |
|              | 39                                     | 9.3   | 0-7          | 4                                    | 9.9   |              | 50                                     | 8.7  |
|              | 41                                     | 8.ĭ   |              | 13                                   | °15.1'<br>9.9<br>9.9<br>9.8   |              | 51                                     | 8.1  |
|              | 43                                     | 5.6   |              | 23                                   | 9.6   |              | 56                                     | 7.3  |
|              | 43<br>46                               | 10.1<br>10.18<br>998.16<br>554.               |              | 29                                   | 9.ž   |              | 58                                     | 6.2  |
|              | 81                                     | 4.6   |              | 0<br>4<br>13<br>23<br>29<br>41       | 9998625   |              | 51<br>56<br>58<br>60                   | 10.0<br>10.0<br>9.7<br>9.7<br>9.7<br>8.1<br>7.6<br>5.8 |
|              |  |   |              | 42                                   | 8.1   |              | 95                                     | 4.8  |
|              |  |   |              | 04                                   |   |              |  |  |

9A

| Slide Depth, M Temp.°C No. Corr. Corr. 43°02.3', 87°29.3'                      | Slide Depth,M Temp.°C No. Corr. Corr. 43°01.9', 87°41.1' | Slide<br>No. | Depth,M<br>Corr. | Temp.°C |
|--|--|--------------|------------------|---------|
| 335 0 10.0<br>4 10.0<br>16 10.0  | 340 0 11.0<br>1 11.0<br>52 11.0                          |              |                  |         |
| 30 9.7<br>44 9.5<br>47 9.4   | 43°01.8', 87°43.4'                                       |              |                  |         |
| 30<br>44<br>9.7<br>9.9<br>9.9<br>9.9<br>9.9<br>9.9<br>9.9<br>9.9               | 341 0 11.1<br>1 11.1<br>43 11.0<br>49 11.0               |              |                  |         |
| 43°02.21. 87°31.61   | 43°01.7', 87°45.8'<br>342 0 11.2<br>1 11.2               |              |                  |         |
| 336 0 10.5<br>4 10.5<br>16 10.6<br>28 10.5                                     | 33 11.2<br>43°01.7', 87°48.1'<br>343 0 11.0<br>1 11.0    |              |                  |         |
| 43 10.2<br>58 9.6<br>60 7.7  | 21.5 11.0<br>43°01.6', 87°50.5'                          |              |                  |         |
| 28 10.5<br>43 10.2<br>58 9.6<br>60 7.7<br>63 6.8<br>66 6.1<br>82 5.7<br>82 5.7 | 344 0 10.7<br>1 10.7<br>15.5 10.7                        |              |                  |         |
| 337 0 11.0   |  |              |                  |         |
| 20 11.0<br>26 10.8<br>36 10.7  |  |              |                  |         |
| 52 8.7   |  |              |                  |         |
| 57 6.7<br>70 5.4<br>81 5.4<br>43°02.1', 87°36.5'<br>338 0 10.9                 |  |              |                  |         |
| 24 10.7  |  |              |                  |         |
| 47 10.3<br>53 10.0<br>59 8.0   |  |              |                  |         |
| 113°02.01. 87°39.01  |  |              |                  |         |
| 1 10.8<br>19 10.8  |  |              |                  |         |
| 43 10.4<br>64 10.4   |  |              |                  |         |
| 70 10.1  |  |              |                  |         |

|             |                                       |  |                                |  |  |         |   | 1  |
|-------------|---------------------------------------|--|--------------------------------|--|--|---------|---|--|
| Slide       | Depth,M                               | Temp.°C  | Slide                          | Depth,M  | Temp.°C                                | Slide   | Denth I   | M Temp.°C  |
| No.         | Corr.                                 | Corr.  | No.                            | Corr.  |  |         |   | and the second s |
|             | יים ווי סיים                          | 0/12/21  | 110.                           |  | Corr.                                  | No.     |   | Corr.  |
| 206         | 44.1, 87                              | . 43,31  | 42                             |  | 7°23.01                                | 42      |   | 87°12.3'   |
| 396         | 0                                     | 8. <u>7</u>  | 405                            | Q  | 8.8                                    | 410     | 0   | 8.6  |
|             | 12.5                                  | 8.7  |                                | 24   | 8.9                                    |         | 39  | 8.5  |
| *****       |                                       |  |                                | 39   | 8.9                                    |         | 44  | 8.4  |
| 42°         | 44.61, 87                             | 41.0'  |                                | 48   | 8.7                                    | ž.      | 45<br>48  | 8.2  |
| 397         | Q                                     | 10.1   |                                | 50   | 8.1                                    |         | 48  | 8.2<br>5.8   |
|             | 18.5                                  | 10.1   |                                | 55   | 7.2                                    |         | 52  | 4.5  |
| 42°         | 45.11,87                              | °38.61   |                                | 56   | 6.6                                    |         | 60  | 4.2  |
| 398         | - O                                   | 10.0   |                                | 58   | 6.4                                    |         | 72  | 4.0  |
|             | 23                                    | 10.0   |                                | 59   | 6.1                                    |         | 133   | 4.0  |
|             | 45.6' <b>,</b> 87                     | °36.01   |                                | 60   | 6.0                                    | 42      |   | 87°10.21   |
| 399         | 0                                     | 9.9  |                                | 63   | 5.7                                    | 411     | 0   | 87°10.2'<br>8.7  |
|             | 31                                    | 9.9  |                                | 63<br>72<br>78                                     | 5.5                                    |         | 36  | 8.7  |
| 42°         | 46.1', 87                             | °33.81   |                                | 78   | 5.2                                    |         | 48  | 8.6  |
| 400         | 0 .                                   | 9.5  |                                | 90   | 4,9.                                   |         | 51  | 6.4  |
|             | 49                                    | 9.5<br>9.5   |                                | 101  | 4.7                                    |         | 53  | 5.3  |
| 42°         | 46.61, 87                             | °31.6'   | 42                             |  | 7°20.9'                                |         | 60  | 4.6  |
| 401         | 0                                     | 9.2  | 406                            | .,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,            | 8.4                                    |         | 66  | 」。<br>」。   |
|             | 57.5                                  | 9.2  |                                | 45   | 8.4                                    |         | 135   | 4.5<br>4.4   |
| • •         | 58.5                                  | 9.1  |                                | 49   | 8.3                                    | 429     |   | 87°08.0'   |
| . 1         | 60                                    | 9.0  | 4                              | 51   | 8.0                                    | 412     | 0   | 8 8  |
|             | 68.5                                  | 8.7  |                                | 54   | 7.4                                    | 1 -4-4- | 21  | 8 8  |
| 42°         | 47.11,87                              |  |                                | 60   | 5 5                                    |         | 49  | 8.8<br>8.8<br>8.6  |
| 402         | 0                                     | 9.1  |                                | 63   | 4.9                                    |         | 51  | 7.5  |
|             | 48                                    | 9.0  |                                | 81   | 4.4                                    |         | 60  | 5.4  |
|             | 50                                    | 8.9  |                                | .96  | 4 4                                    |         | 64  | フ・ <del>イ</del><br>ル・7   |
|             | 52                                    | 8.6  | 42°                            |  | 7°18.7'                                |         | 81  | 4.5  |
|             | 54                                    | 7.9  | 407                            | 0  | 8.3                                    |         | 135   | 4.5  |
| * *         | 59                                    | 7.0  | 7.                             | 47   | 8.2                                    | 42°     |   | 37°06.01   |
|             | 60                                    | 6.6  |                                | 50   | 7.1                                    | 413     |   | 9.0  |
|             | 62                                    | 6.1  |                                | 55   | 6.4                                    |         | 21  | 9.0  |
|             | 64                                    | 5.9  |                                | 55<br>56   | 6.0                                    |         | 36  | 8.8  |
|             | 66                                    | 5.2  |                                | 60   | 5.3                                    |         | 42  |  |
|             | 80                                    | 4.8  |                                | 67   | 4.4                                    |         | 44  | 8 6  |
| 42°,<br>403 | 87 ( 16.74                            | 27.21  |                                | 8i<br>109  | 4.2<br>4.1                             |         | li O  | 8.7  |
| 403         | 0                                     | 8.9  |                                | 109  | 4.1                                    |         | 51  | 8.3  |
|             | 36                                    | 8.9  | 42°                            | 49.91,87   | 7°16.7'                                |         | 52  | 8.2  |
| -           | 45                                    | 8.8  | 42°<br>408                     | 0  | 8.4                                    |         | 58  | 6.4  |
|             | 55                                    | 8.5  |                                | 45   | 8.4                                    |         | 60  | 6.3  |
| i           | 60:                                   | 5.2  |                                | 46   | 8.1                                    |         | 61  | 6.2  |
|             | 61                                    | 4.8  |                                | 48   | 7.0                                    |         | 63  | 5.6  |
|             | 63                                    | 4.6  | • • •                          | 52   | 6.3                                    |         | 68  | 11.8   |
|             | 0<br>36<br>55<br>50<br>61<br>63<br>89 | 5.2<br>4.9<br>9.98<br>8.52<br>8.6<br>4.4<br>24.9   |                                | 60   | 5.3                                    | •       | 72  | л.<br>6  |
| 42°2<br>404 |                                       | 24.91  |                                | 67   | 4.4                                    |         | 75  | Д. И   |
| 404         | 0                                     | 24.9!<br>8.8<br>8.7<br>8.4<br>8.0<br>7.1<br>6.1  | •                              | 0<br>45<br>46<br>48<br>52<br>60<br>67<br>116       | 8.4<br>8.1<br>7.0<br>6.3<br>5.4<br>4.3 |         | 51<br>52<br>58<br>60<br>61<br>63<br>68<br>72<br>75<br>81<br>130 | 888886666544444444444444444444444444444  |
|             | 0<br>491<br>535<br>552<br>639<br>99   | 8.7  | 42°<br>409                     | 50.51, 87  |  |         | 130   | Д 1  |
|             | 51                                    | 8.4  | 409                            | 0  |  | 42      | <u>°52.81                                    </u>               | 87°04.0'   |
|             | 53                                    | 8.0  | -                              | 46   | 8.1                                    | 414     | 0   | 9.0  |
|             | 55                                    | 7.1  |                                | 48   | 7.8                                    |         | 5Ĩ  | 9.0  |
|             | 62                                    | 6.1  |                                | 50   | 7.1                                    |         | 56  | á.š  |
|             | 63                                    | 5.7  | -                              | 53   | 5.4                                    |         | 60  | 6.6  |
| •           | 69                                    | 5.7<br>5.0<br>4.4  |                                | 54   | 5.3                                    |         | 61  | 6.3  |
|             | 99                                    | 4.4  |                                | 60   | 4.6                                    |         | 62  | 5.9  |
|             | į.                                    | **************************************   | 1.                             | 0<br>46<br>48<br>50<br>53<br>54<br>60<br>67<br>121 | 8.18<br>7.14<br>5.43<br>4.1            |         | 0<br>556<br>60<br>62<br>66<br>66                                | 87°04.01<br>9.0<br>9.8<br>6.3<br>5.0<br>4.7  |
|             |                                       | e a compara de la compara de l | ****************************** | <u> </u>   | 4.1                                    |         | 66  | 4.7  |
|             |                                       |  |                                |  |  |         |   |  |

| Slide<br>No. | Depth,M<br>Corr.  | Temp.°C<br>Corr.                         | Slide<br>No. | Depth,M<br>Corr.                                       | Temp.°C   | Slide<br>No.                             | Depth,M<br>Corr.                                       | Temp.°C  |
|--------------|---|--|--------------|--|---|--|--|--|
| 414          | 81<br>123   | 4.5<br>4.3                               | 419          | 81<br>101  | 4.6<br>4.6  | 423                                      | 65<br>71   | 4.7  |
| 42°          |   | °01.8'                                   | 42           | °55.41,86  | 5°50.5'   | en e | 80   | 4.4  |
| 415          | 0<br>18   | 9.1                                      | 420          | 0<br>48  | 9.5<br>9.5  | 1120                                     | 96<br>57.31,86   | 4.4<br>41.5  |
|              | 30  | 9.1<br>8.8<br>8.5<br>8.3                 |              | 54   | 9.3   | 424                                      | 0  | 10.9   |
|              | 42<br>54  | 8.5<br>8.3                               |              | 55<br>56   | 8.7<br>7.9  |  | 17<br>21.5   | 10.8<br>10.5   |
|              | 57  | 6.2                                      |              | 57   | 7.5<br>5.7  |  | 23   | 10.0   |
|              | 59  | 5.2<br>5.1                               |              | 57<br>59<br>60   | 5.7<br>5.6  |  | · 26<br>29   | 9.4<br>9.2   |
|              | 60<br>64  | 5.1<br>4.5                               |              | 63<br>78   | 5.5<br>5.5  |  | 50   | 9.1  |
|              | 81<br>119   | 4.4<br>4.2                               |              | 78<br>84   | 5.4<br>5.3  |  | 50<br>54<br>55<br>57                                   | 9.1<br>8.2<br>8.0  |
| 42°          |   | °59.6'                                   | •            | 87   | 5.2   |  | 57 ·   | 8.0  |
| 416          | 0<br>35   | 9.2<br>9.2<br>9.0<br>8.7                 |              | 93<br>96   | 4.9<br>4.8  | , .                                      | 59<br>60<br>63<br>65                                   | 6.1<br>6.0   |
|              | 39  | 9.0                                      |              | 99   | 4.8   |  | 63   | 5.5<br>5.2   |
|              | 40<br>44  | 8.7<br>6.1                               | 42°<br>421   | °55.9', 86   | 9.3   |  | 65<br>71   | 5.2<br>4.7   |
|              | 47  | 4.9<br>4.6                               | 1 444 25     | 45   | 9.2   |  | 77   | 4.6  |
|              | 53<br>60  | 4.6<br>4.5                               |              | 51<br>54   | 9.0<br>7.9  | 42°                                      | 95<br>57.8', 86  | 4.5°39.2°  |
|              | 115   | 4.1                                      |              | 56<br>60   | 7.0   | 425                                      | 0  | 11.4   |
| 42°<br>417   | 54.0', 86<br>0  | 9.3                                      |              | 65   | 6.6<br>6.1  |  | 20<br>22   | 11.4<br>11.3   |
| ,_,          | 38  | 9.2                                      |              | 67<br>81   | 5.2   |  | 24   | 10.5<br>10.3   |
|              | 40<br>41  | 9.1<br>8.9                               |              | 96   | 4.9   |  | 25<br>27   | 9.6<br>9.4   |
|              | 43  | $6.7 \\ 4.7$                             | 42°<br>422   | °56.31, 86<br>0  | 9.3   |  | 29<br>32   | 9.4<br>9.3   |
|              | 47<br>50<br>60  | 4.5                                      |              | 18   | 9.2   |  | 50   | 9.2  |
|              | 60<br>95  | 4.4<br>4.2                               |              | 27<br>45   | 9.0<br>9.0  |  | 52<br>55.5   | 9.1<br>7.4   |
| ·            | 110   | .4.2                                     |              | 48   | 8.9   |  | 57   | 6.2  |
| 42°<br>418   |   | °55.0'                                   |              | 45<br>48<br>538<br>636<br>67<br>81<br>96               | 98875554444<br>44.  |  | 57<br>60<br>63<br>65<br>77<br>91                       | 6.9.1.0.9.9<br>5.5.4.9   |
| 410          | 42.5  | 9.6                                      |              | 58   | 5.9   |  | 6 <u>5</u>   | 5.0  |
|              | 43.5<br>45  | 9.0<br>8.4                               |              | 60<br>63   | 5.4   |  | 91   | 4.9<br>4.9   |
|              | 49  | 5.5                                      | •            | 66   | 4.7   | 42°<br>426                               | 58.21, 86  | °37.0'   |
|              | 51<br>54  | 4.9<br>4.7                               |              | 81   | 4.9<br>4.4  | 420                                      | 27.5   | 11.1   |
|              | 57  | 4.6                                      | - JO         | 96<br>°56.8', 86                                       | 4.4   |  | 29.5   | 11.1   |
|              | 60<br>66  | 4.6<br>4.5                               | 423<br>423   | 50.0.  | 10.4  |  | 37.5   | 10.7   |
|              | 54.6', 86<br>42.5<br>43.45<br>45<br>45<br>54<br>57<br>66<br>81<br>106 | 0999854444444444444444444444444444444444 |              | 5<br>11  | 10.4  |  | 40.5   | 8.2  |
| 42°          |   |  |              | 14   | 10.2  |  | 44.5   | °37.0'<br>11.2<br>11.7<br>10.4<br>10.4<br>10.5<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7 |
| 419          | 715<br>0  | 9.5                                      |              | 16<br>20   | 10.1<br>9.5   |  | 46.5<br>50.5   | 5.7<br>5.5   |
|              | 48  | 9.4                                      |              | 23   | 9.3   |  | 56.5   | 5.4  |
|              | 49.5<br>51  | 8.2<br>7.5                               |              | 47<br>51.5   | 9.2<br>9.1  |  | 60<br>74.5   | 5.4<br>5.3   |
|              | 55  | 5.5                                      |              | 53   | 7.9   |  | 83.5   | 5.0  |
|              | 48<br>49<br>49<br>55<br>57<br>66                                      | 52.99987548.7<br>99987544.7              |              | 0<br>5<br>14<br>16<br>20<br>23<br>47<br>55<br>55<br>62 | 10.4<br>10.4<br>10.3<br>10.1<br>10.5<br>10.9<br>99.9<br>76.5<br>5.5 | 42°                                      | 58.2, 0<br>2796.55.55.55.55.55.55.55.55.55.55.55.55.55 | °34.1'   |
| •            | 66  | 4.7                                      |              | 62   | 5.3   | 427                                      | 0  | °34.1'<br>11.0   |

| Slide<br>No. | Depth,M<br>Corr.  | Temp.°C  |
|--------------|---|--|
| 427          | 92868<br>133442<br>45106<br>86  | 11.0<br>10.965617552098  |
| 42°<br>428   | 59.6', 86<br>27<br>336<br>41<br>44<br>48<br>54<br>48<br>54<br>60<br>82                  | 31.1<br>11.0<br>10.8<br>10.7<br>10.5<br>10.4<br>7.5<br>5.2<br>5.1<br>5.9   |
| 43°<br>429   | 00.3'0124344578490190080  | 11.0<br>11.0<br>10.9<br>10.7<br>10.4<br>9.9  |
| 43°<br>430   | 45<br>478<br>490<br>490<br>555600<br>80<br>100<br>100<br>100<br>100<br>100<br>100<br>10 | 6.6<br>5.3<br>5.4<br>12.0<br>11.7<br>11.3<br>76.0<br>12.7<br>11.3<br>76.0<br>12.7<br>12.7<br>11.3<br>12.7<br>12.7<br>11.3<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12.7<br>12. |
| 43°<br>431   | 01.3', 86<br>0<br>42<br>50  | 12.8<br>12.7<br>12.2   |

| Slide<br>No. | Depth,M<br>Corr.   | Temp.°C<br>Corr. | Slide<br>No. | Depth,M<br>Corr. |
|--------------|--------------------|------------------|--------------|------------------|
| 431          | 56                 | 11.6             |              |                  |
|              | 58                 | 10.9             |              |                  |
|              | 60                 | 10.9             | •            |                  |
|              | 62                 | 10.9             |              |                  |
| 43°          | <u>'01.8', 86</u>  | °19.7'           |              |                  |
| 432          | Ō                  | 11.5             |              |                  |
|              | 38.5               | 11.5             |              |                  |
| 43°          | '02.5' <b>,</b> 86 | °16.81           |              |                  |
| 433          | 0                  | 11.3             |              |                  |
|              | 28.5               | 11.3             |              |                  |
|              |                    |                  |              |                  |

Temp.°C Corr.

## Grand Haven to Milwaukee 17 April 1963

| Slide<br>No. | Depth,M<br>Corr.                              | Temp.°C                             |
|--------------|---|-------------------------------------|
| 43°<br>434   | 03.1', 86<br>0<br>16<br>25                    | 1.0<br>1.1<br>1.4                   |
| 435          | 0<br>46<br>51                                 | 1.0<br>1.2<br>1.6                   |
| 436          | 0<br>60<br>75                                 | 1.0<br>1.0<br>1.0                   |
| 43°<br>437   | 0<br>60<br>67                                 | 1.0<br>1.0<br>1.0                   |
| 438          | 03.0', 86<br>0<br>60<br>82                    | 0.8<br>0.8<br>0.8                   |
| 43°<br>439   | 03.01, 86<br>0<br>60<br>94                    | 1.0<br>1.0<br>1.0                   |
| 43°<br>440   | 03.0', 86<br>0<br>60<br>100                   | 1.0<br>0.9<br>0.9                   |
| 43°<br>441   | 03.0', 86<br>0<br>60<br>103                   | 1.3<br>1.3<br>1.2                   |
| 442<br>442   | 02.91, 86<br>0<br>60<br>99                    | 1.3<br>1.2<br>1.2                   |
| 443          | 02.9', 86<br>0<br>60<br>107                   | 1.3<br>1.3<br>1.3                   |
| 444          | 02.9', 86<br>0<br>60<br>108                   | 1.3<br>1.2<br>1.2                   |
| 43°<br>445   | 02.9', 86<br>0<br>60<br>65<br>101             | 1.3<br>1.2<br>1.2<br>1.1            |
| 43°<br>446   | 02.8 <sup>†</sup> , 86<br>0<br>35<br>60<br>92 | 0°46.0°<br>1.2<br>1.2<br>1.1<br>1.0 |

|  |                                       |           | -               |                    |
|--|---------------------------------------|-----------|-----------------|--------------------|
| Slide  | Depth,                                | M         | Ten             | D°.an              |
| No.  | Corr                                  |           |                 | ri.                |
| 430  | 02.81                                 | 86        | 48              |                    |
| 447  |                                       | •         | . •             | i 2                |
| 441  | 50                                    |           |                 | 1.2                |
|  | 60<br>60                              |           |                 |                    |
| (1) A  | . 60                                  |           |                 | 1.2                |
| - 100  | 97                                    | (77-)     |                 | 1.0                |
| 43   | 02.81                                 | 86        | '50 .           | .9'                |
| 448  | O                                     |           |                 | 1.3                |
| 11 × 4 × 1   | 59                                    |           |                 | 1.3                |
|  | 60                                    |           |                 | 1.3                |
|  | 93                                    |           |                 | 1.1                |
| 43°  | 02.81.                                | 86        | <sup>2</sup> 53 | . סי               |
| 449  | O                                     |           |                 | 1.3                |
|  | 40                                    |           |                 | 1.3                |
|  | 60                                    |           |                 | 1 2                |
|  | 94                                    |           |                 | 1 1                |
| 1130   | 02.71                                 | QZ I      | °55             | <del>. 6 i -</del> |
| 43°  | ٠,١٠٥٠                                | 86        | つつ              | .o.                |
| 450  | 0                                     |           |                 | 7.3                |
|  | 60                                    |           |                 | 1.3                |
|  | 89                                    |           |                 | 1.3                |
| 43°  | 02.61,                                | 86        | <b>°</b> 57     | . <del>8</del> i   |
| 451  | 0                                     |           |                 | 1.2                |
| <del>.</del>   | 60                                    |           |                 | 1.1                |
|  | 89                                    |           |                 | 1.1                |
| 43°  | 02.61.                                | 87        | °00             | 71                 |
| 452  | 0                                     | ٠,        | •               | ī 2                |
|  | 60                                    |           |                 | 1.1                |
|  | 72                                    |           |                 | 7 7                |
| פכוו   | 00 6                                  | 87        | °02             | <del></del>        |
| 43°  | 02.00                                 | Οį        | UZ              | • ( `              |
| 453  | -0                                    |           |                 | 1.1                |
|  | 78                                    | 71        | n = 1:-         | 1.0                |
| 43°  | 02.51                                 | 87        | °04             | .8'                |
| 454  | 0                                     |           |                 | 1.1                |
|  | 77                                    |           |                 | 1.0                |
| 43°  | 02.51,                                | 87        | °07             | .1'                |
| 455  | 0                                     |           |                 | 1.1                |
|  | 75                                    |           |                 | 1.1                |
| 43°  | 02.41                                 | 87        | °09             | 31                 |
| 456  | 0                                     | ٠,        | -               | 1.1                |
| 1,70   | 70                                    |           |                 | 0.0                |
| 43°  | 11 co                                 | 87        | ० न न           | <del>612</del>     |
| りにつ  | 02.4                                  | 01        | 11              | • O ·              |
| 457  |                                       | grand on  | g in company    | ተ•ች                |
| - 1.50   | ( 1                                   | - C) == 1 | 0 - 8           | 4.0                |
| 43   | 02.41                                 | 8.L       | 13              | .8'                |
| 458  | 0                                     |           | 7. 1.           | 1.1                |
| A STATE OF S | 85                                    |           |                 | 0.8                |
| 43°  | 02.31,                                | 87        | 16              | .01                |
| 459  | 0                                     |           |                 | 1.1                |
|  | 87                                    |           |                 | 0.9                |
| 439  | 02.21.                                | 87        | °18             | .21                |
| 460  | 0                                     | •         |                 | 1.1                |
|  | 87                                    |           |                 | 0.9                |
|  | ~                                     | 077       | °20             | ĒŤ                 |
| ग्रद   | 02.21                                 | OI        | -c              | - ") "             |
| 43°  | · · · · · · · · · · · · · · · · · · · | 01        | 20              | •5°                |
| 43°<br>461   | 02.2',<br>0<br>57                     | 01        | 20              | 1.1                |

| Slide    | Depth,M               | Temp.°C        |
|----------|-----------------------|----------------|
| No.      | Corr.                 | Corr.          |
| <u> </u> | 02.21.87              | °22.71         |
| 462      | 0                     | 1.1            |
| -1 () Gu | ດາ                    | 0.0            |
| 43       | <sup>ウ</sup> ヘク 11 日7 | °25.0i         |
|          | 02.17, 01             | 25.0           |
| 463      | 0                     | 7.5            |
|          | 89                    | 1.3            |
| 43       | °02.1', 87            | (,54.5)        |
| 464      | 0                     | 1.6            |
|          | 9 <b>2</b>            | 1.3            |
| 43       | °02.1', 87            | 7°29.81        |
| 465      | 0                     | 1.6            |
|          | 88                    | 1.3            |
| 43       | 02.11.87              | 7°32.11        |
| 466      | 0.                    | 1 6            |
| 400      | 7/1                   | ī. Ŭ           |
| 43       | 000 AT B7             | 7934.61        |
| 1167     | 02.00                 | J              |
| 467      | - C                   | 1.6            |
|          | 70                    | 1.5            |
| 43       | °02.0°, 87            | (37.41)        |
| 468      | 0                     | 1.6            |
|          | 68                    | 1.4            |
| 43       | 87 <b>, '0</b> 1.9°   | 7°40.71        |
| 469      | 0                     | 1.8            |
| _        | 56                    | 1.7            |
| 43       | °01.81.87             | 7°42.91        |
| 470      | 0                     | 2.0            |
| ., •     | 44                    | 2.0            |
| 43       | <u>ਅਨਰ ਲੰਗੇ ਲਾ</u>    | 7°46.0'        |
| 471      | 01.0 , 0              | 2.4            |
| 4 ( T    | 2/1                   |                |
| 43       | 901 71 OF             | 2.4<br>7°48.91 |
|          | OT. (1) 87            |                |
| 472      | 0                     | 2.4            |
| -        | 20                    | 2.4            |
|          |                       |                |
|          |                       |                |
|          |                       |                |

| Slide Depth, M Temp.°C   | Slide Depth, M Temp.°C No. Corr. Corr.                                    | Slide Depth, M Temp.°C  |
|--|---|---|
| 43°03.4', 86°16.6'<br>575 0 9.0<br>13 9.0<br>17 8.7  | 43°03.1', 86°42.0'<br>584 0 3.0<br>32 3.0<br>60 2.9                       | 43°02.6', 87°09.9'<br>595 0 3.5<br>60 3.2<br>81 3.1                                 |
| 43°03.4', 86°19.1'<br>576 0 9.0<br>19 8.3<br>26 6.0<br>30 6.0                                  | 102 2.8<br>43°03.0', 86°44.5'<br>585 0 3.0<br>35 3.0<br>60 2.9            | 43°02.6',87°12.5'<br>596 0 3.7<br>30 3.7<br>60 3.6<br>79 3.5                        |
| 43°03.4', 86°21.7' 577 0 6.5 28 6.1 31 5.6 38 5.6  | 102 2.7<br>43°03.0', 86°47.2'<br>586 0 3.0<br>45 3.0<br>60 2.9<br>99 2.8  | 43°02.5', 87°15.2' 597  |
| 51 4.9<br>43°03.4', 86°24.0'<br>578 0 5.1<br>30 4.7<br>60 4.3                                  | 43°03.0', 86°49.8'<br>587 0 3.0<br>60 3.0<br>95 2.9<br>42°02.9', 86°52.3' | 598 0 3.7<br>30 3.7<br>60 3.5<br>80 3.4<br>43°02.4', 87°20.2'                       |
| 75 4.3 One cast missed. 43°03.3', 86°29.4'   | 588 0 3.1<br>60 3.1<br>97 3.0<br>43°02.9', 86°54.8'                       | 599 0 3.5<br>30 3.5<br>60 3.4<br>70 3.4   |
| 579 0 3.8<br>40 4.0<br>60 3.9<br>74 3.7  | 589 0 3.1<br>50 3.1<br>60 3.0<br>90 3.0                                   | 43°02.4', 87°22.6'<br>600 0 3.5<br>30 3.5<br>53 3.4                                 |
| 9 3.9<br>43°03.2', 86°31.8'<br>580 0 3.5<br>25 3.5<br>60 3.2<br>80 3.0                         | 43°02.8', 86°57.4' 590 0 3.4 50 3.4 60 3.3 84 3.2                         | 43°02.4', 87°25.1'<br>601 0 3.5<br>25 3.5<br>60 3.2<br>74 3.2                       |
| 95 3.2   | 43°02.8', 86°59.9' 591 0 3.6 50 3.6 60 3.4 85 3.3                         | 43°02.3', 87°27.7'<br>602 0 3.8<br>30 3.7<br>60 3.3<br>85 3.2<br>43°02.3', 87°30.2' |
| 581 0 3.5<br>30 3.5<br>60 3.3<br>75 3.1<br>97 3.0<br>43°03.2', 86°37.0'<br>582 0 3.5<br>30 3.5 | 592 0 3.8<br>23 3.8<br>60 3.6   | 45 3.8<br>60 3.7  |
| 582 0 3.5<br>30 3.5<br>60 3.4<br>72 3.1<br>85 3.5<br>100 4.0                                   | 43°02.7', 87°04.9'<br>593 0 3.7<br>30 3.7<br>60 3.6<br>68 3.6             | 43°02.2', 87°32.8'<br>604 0 3.8<br>30 3.8<br>60 3.7                                 |
| 43°03.2', 86°37.0' 582   | 68 3.6<br>43°02.7', 87°07.5'<br>594 0 3.7<br>30 3.7<br>60 3.5<br>69 3.5   | 43°02.2', 87°35.4'<br>605 0 3.9<br>30 3.9<br>60 3.8<br>78 3.7                       |

| Slide<br>No. | Depth,M<br>Corr.               | Temp.°C<br>Corr.            | Slide<br>No. | Depth, M Temp. Corr. Corr |  |
|--------------|--------------------------------|-----------------------------|--------------|---------------------------|--|
| 606          | 02.1', 87<br>0<br>60<br>63     | 38.0'<br>4.0<br>3.7<br>3.7  |              | i i                       |  |
| 607          | 02.1', 87<br>0<br>50<br>60     | *40.6'<br>4.0<br>3.8<br>3.7 |              |                           |  |
| 43°<br>608   | 02.0', 87<br>0<br>25<br>52     | 43.0°<br>4.1<br>4.1<br>4.0  |              |                           |  |
| 43°<br>609   | 01.9, 87<br>0<br>35            | 45.6'<br>4.7<br>4.6         |              |                           |  |
| 610          | 01.8', 87<br>0<br>19           | 6.0<br>6.0                  |              |                           |  |
| 611          | 01.7', 87<br>0<br>7<br>9<br>11 | 8.3<br>8.0<br>7.2<br>7.1    |              | . •                       |  |

Slide Depth,M Temp.°C No. Corr. Corr.

# Grand Haven to Port Washington 24 June 1963

|  | Corr.      | Temp.°C<br>Corr.  |
|--|------------|---|
| 633  | 6          | 8.6<br>7.6<br>7.0   |
|  | 13         | 6.7<br>6.4  |
|  | 26         | 6.2<br>5.8  |
| 43°  |            | 5.1<br>5°42.0'  |
| 634  | 0 2        | 9.4   |
|  | 5<br>7     | 8.5<br>7.8  |
| ,  | 16         | 6.9<br>6.6<br>6.1   |
|  | 33<br>37   | 5.8<br>5.7  |
|  | 46<br>56   | 5.3<br>4.8  |
|  | 65         | 4.6<br>4.5<br>4.3   |
|  | 74<br>104  | 4.3   |
| .635   | 0          | 6°44.6'<br>9.4  |
|  | 3          | 9.1<br>8.8<br>7.9   |
|  | 760        | 7.7<br>7.5  |
|  | 14<br>21   | 6.7<br>6.4  |
|  | 27         | 5.7<br>5.6  |
|  | 32<br>41   | 5.2764.4<br>4.3   |
|  | 44<br>60   | 4.6   |
| 43°  | °03.1', 8  | 6°47.3'   |
|  | 1<br>3     | 9.2<br>7.4  |
|  | 14<br>17   | 6.3<br>6.2  |
|  | 25<br>34   | 6.0<br>5.4  |
| -  | 38<br>56   | 4.7<br>4.2  |
|  | 71<br>85   | 6°47.32.4.32.04.72.22.1   |
| NACES CONTRACTOR OF THE SECOND CONTRACTOR OF T |            | · .   |
|  | 43°<br>635 | 633<br>6<br>10<br>13<br>15<br>26<br>35<br>42<br>43°03.1', 86<br>634<br>0<br>2<br>5<br>7<br>14<br>16<br>30<br>33<br>37<br>46<br>60<br>65<br>74<br>104<br>43°03.1', 86<br>635<br>0<br>2<br>3<br>5<br>6<br>9<br>14<br>21<br>27<br>29<br>32<br>44<br>44<br>60<br>95<br>43°03.1', 86<br>60<br>61<br>61<br>61<br>62<br>63<br>63<br>63<br>63<br>63<br>63<br>63<br>63<br>63<br>63 |

| 43*03.1*, 86*49.8*   | Slide<br>No.     | Depth,M<br>Corr.     | Temp.°C<br>Corr. | Slide<br>No. | Depth,M<br>Corr.                       | Temp.°C<br>Corr.                        | Slide<br>No. | Depth,M<br>Corr. | Temp.°C<br>Corr.               |
|--|------------------|----------------------|------------------|--------------|--|---|--------------|------------------|--------------------------------|
| 2 9.7  |                  | - 1                  | 9.8              | 640          | 71                                     | 4.1                                     | 645          | 5<br>7           |                                |
| 5 7, 4 (winch failure)  10 6.7 7, 2 43°03.0¹, 87°07.6¹  11 6.0 3.8  121 6.0 1 1 11.3  211 6.0 1 1 11.3  211 6.0 1 1 11.3  31 5.5 4 9.6  41 9.6 2 11.9  41 1.0 9  60 4.5 15 8.5 10 10.9  60 4.5 15 8.5 10 10.3  71 4.3 16 7.3 21 5.4  43°03.0¹, 86°52.3¹  638 4 9.0 60 4.2  7 7 7.5 43°02.9¹, 87°10.4¹  10 7.2 642 0 11.4  11 7.4 14 3 9.9  10 7.2 642 0 11.4  11 7.4 14 6.4  14 4.6 19 6.4 18 4.7  52 4.4 4 29 5.7  60 4.3 32 12 8.4  14 4.6 19 6.4 18 4.7  52 4.4 4 29 5.7  60 4.3 32 5.4  60 4.3 32 5.5 4  60 4.3 32 5.5 4  60 4.3 32 5.5 4  60 4.3 32 5.5 4  60 4.3 32 5.5 5  60 4.3 38 7°10.4¹  10 7.2 642 0 11.4  11 7.4 14 6.4  14 6.4 18 4.7  52 4.4 4 29 5.7  60 4.3 32 5.4  60 4.3 32 5.5 4  60 4.3 33 4.1  60 6.3 8  1 10.4 18 4.7  22 4.3 33 4.1  60 6.4 1.1 6.4  43°03.0¹, 86°54.9¹  643 0 10.6  643 0 11.9  643 0 10.6  648 0 4.1  60 4.3 38 4.4  60 4.3 38 4.4  60 4.3 38 5.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 4.3 38 6.5  60 60 4.3 4.3  60 4.1 16 6.4  60 4.3 4.4  60 4.4 18 8 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 4.4  60 4.3 6.4  60 4.3 8.8  60 4.1  60 4.3 8.8  60 4.1  60 60 4.3 8.9  60 60 4.0 8.9  60 60 4.3 8.9  60 60 4.0 8.9  60 60 4.0 8.9  60 60 4.0 8.9  60 60 4.0 8.9  60 60 4.0 8. |                  | 2<br>4               | 9.7              | FD           | ······································ | *************************************** |              |                  |                                |
| 10 6.7 641 0 11.3 77 3.6 19 67 11.9 6.3 641 0 11.3 743°02.8', 87°21.0' 12.4 11.3 646 0 12.4 11.3 646 0 12.4 11.3 646 0 12.4 11.3 646 0 12.4 11.3 646 0 12.4 11.3 11.3 646 0 12.4 11.3 11.3 646 0 12.4 11.3 11.3 646 0 12.4 11.9 660 4.5 15 8.5 10 10.3 71 4.3 166 7.3 21 5.4 14 10.9 660 4.5 12.4 12.2 11.5 14.3 12.2 11.5 14.3 12.2 11.5 14.3 12.2 11.5 14.3 12.2 11.5 14.3 12.2 11.5 14.3 12.3 12.3 12.3 12.3 12.3 12.3 12.3 12  |                  | 5<br>7               | 7.4              |              |  |   |              |                  |                                |
| 21 6.0 1 11.9 6.0 2 11.9 6.0 12.4 1.0.9 6.0 12.4 1.0.9 6.0 12.4 1.0.9 6.0 12.5 1.0 10.3 1.0.9 6.0 12.5 1.0 10.3 10.9 6.7 2.0 1.0 10.3 1.0 10.0 10  |                  |                      | 6.7              |              | 03.01, 87                              |   | . 1120       | 77               | 3.6                            |
| ## 1 5.0   |                  | 21                   | 6.0              | 641          | į                                      | 11.3                                    | 646          | 0                | 12.4                           |
| 60 4.5 71 4.3 15 8.5 10 10.3 21 5.4 60 4.0 638 0 9.5 29 4.4 60 4.0 638 0 9.5 7.9 73 4.1 10 7.2 12.2 7.7 7.5 642 0 11.4 3 9.9 17 6.2 23 6.1 11 7.4 14 4 4.6 19 6.4 18 4.7 52 4.4 29 5.7 22 4.3 60 4.0 60 4.0 60 4.0 60 4.0 60 60 4.2 60 60 60 60 60 60 60 60 60 60 60 60 60   |                  | 31<br>41             |                  |              | 7                                      |   |              |                  |                                |
| ## ## ## ## ## ## ## ## ## ## ## ## ##   |                  | 60                   | 4.5              |              | 15<br>16                               |   |              |                  | 10.3                           |
| 638  | <del>- nao</del> | 84                   | 4.3              |              | 19                                     | 6.7                                     |              | 28               | 4.4                            |
| 7 7 7 5 43°02.9¹, 87°10.4¹ 647 0 12.2 11.8 10 7.2 642 0 11.4 3 9.9 12 6.5 1 11.3 6 8.9 17 6.2 3 9.2 12 8.4 4 44 4.6 19 6.4 18 4.7 56 4.0 4.1 71 4.2 38 5.0 60 4.1 71 4.2 38 5.0 60 4.1 77 4.3 60 4.1 77 4.3 60 4.1 77 6.1 6.1 6.3 6 7.8 4 9.5 643 0 10.6 6 7.8 4 9.5 643 0 10.6 6 7.8 4 9.5 6 7.8 6 7.8 4 9.5 6 7.8 6 7. | 638              | _                    | 9.5              |              | 29                                     | 4.4                                     |              | 83               | 4.0                            |
| 7 7.5  |                  | 4<br>5               | 7.9              |              |  |   | 647          | _                | 12.2                           |
| 12 6.5 17 6.2 23 6.1 11 77.4 14 4.6 44 4.6 19 6.4 18 4.7 52 4.4 29 5.7 22 4.3 60 4.3 80 4.1 71 4.2 80 4.1 90 4.1 77 4.3 639 0 9.5 643 0 10.6 5 8.4 1 10.4 22 5.6 5 8.4 2 9.7 6 7.8 6 7.8 4 9.5 6 7.8 4 9.5 6 7.8 6 7.8 4 9.5 6 7.8 6 9.1 6 10.9 6 11.4 6 11.4 6 |                  | 7                    | 7.5<br>7.2       | 43°<br>642   |  |   |              | 2<br>3           |                                |
| 23 6.1 11 7.4 14 6.4 4.6 4 4.4 4.6 19 6.4 18 4.7 52 4.4 4.6 6.4 19 6.4 18 4.7 52 4.4 4.6 6.4 19 6.4 18 4.7 52 4.3 32 5.4 33 4.1 60 4.1 60 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.   |                  | 12                   | 6.5              |              | j                                      | 11.3                                    |              |                  | 8.9<br>8.4                     |
| 60 4.3 32 5.4 60 4.0 80 4.1 60 4.4 648 0 11.9 639 0 4.1 648 0 11.9 639 0 4.8 8 1 10.4 22 5.6 5 8.4 2 9.7 23 5.1 66 7.8 4 9.5 277 4.9 10 6.8 12 7.1 48 4.4 25 6.3 15 5.7 60 4.3 38 5.5 29 4.6 60 4.3 38 5.5 29 4.6 60 4.3 88 5.5 29 4.6 60 4.3 88 5.5 29 4.6 60 4.3 89 4.2 60 4.3 60 4.1 60 60 4.3 60 4.1 60 60 4.3 60 60 4.1 60 60 4.3 60 60 4.1 60 60 60 60 60 60 60 60 60 60 60 60 60  |                  |                      | 6.1              |              |  | 7.4                                     |              | 14               | 6.4                            |
| 71   |                  | 44<br>52             | 4.4              |              | 19<br>29                               | 5.7                                     |              | 22               |                                |
| 90 4.1 77 4.3 648 0 11.9  43°03.0', 86°54.9' 43°02.9', 87°13.3' 11 7.8 639 0 9.5 643 0 10.6 17 6.1 94 8.8 1 10.4 22 5.6 5 8.4 2 9.7 23 5.1 6 7.8 4 9.5 27 4.9 10 6.8 12 7.1 48 4.4 25 6.3 15 5.7 60 4.3 34 5.7 21 5.0 69 4.1 38 5.5 29 4.6 45 5.1 53 4.4 56 4.2 60 4.3 89 4.2 83 4.0  One cast missed. (winch failure)  00e cast missed. (winch failure)  43°03.0', 86°59.9' 4 9.2  01 11.0 9 8.3 10.6 23 4.8 4 10.4 34 4.5 6 6 4.2 6 10.9 1 11.0 17 5.8 1 10.4 34 4.5 6 6 4.2 1 10.4 34 4.5 6 6 4.2 1 10.4 34 4.5 1 10.4 34 4.5 1 10.8 4.9 1 10 |                  | 60<br>71             |                  |              | 32<br>38                               | 5.4<br>5.0                              |              | 60               |                                |
| ## 43°03.0°, 86°54.9°   #43°02.9°, 87°13.3°   11   |                  | 80                   | _                |              |  | 4.4<br>4.3                              | 648          |                  |                                |
| ## 8.8   | 43°              | <del>03.01, 86</del> | °54.9'           | 43           | °02.91,87                              | °13.3'                                  | •            | 11               |                                |
| 10   6.8   12   7.1   48   4.4   4.5   4   | 639              | 4                    | 9.0              | 043          | 1                                      |   |              | 22               | 5.6                            |
| 10 6.8 12 7.1 48 4.4 4.4 25 6.3 15 5.7 60 4.3 34 5.7 21 5.0 69 4.1 38 5.5 29 4.6 89 4.1 45 5.1 53 4.4 56 4.2 60 4.3 60 4.1 89 4.2 83 4.0 649 0 14.2 60 649 0 14.2 60 649 0 14.2 60 649 0 14.2 60 649 0 14.2 60 649 0 14.2 60 11.4 6 10.9 61 640 0 11.4 10 10.3 12.0 640 0 11.4 10 10.3 12.0 640 0 11.0 10.3 12.0 640 0 11.0 10.3 12.0 640 0 11.0 10.3 12.0 640 0 11.0 10.3 12.0 640 0 11.0 17 5.8 22 4.9 3 10.6 23 4.8 4.8 4.4 4.5 60 4.0 7 8.9 42 4.1 92 4.2 10 8.4 10.4 34 4.5 60 4.0 TRANSECT TURNS NORTHWARD 65 4.0 TRANSECT TURNS NORTHWARD 65 4.0 TRANSECT TURNS NORTHWESTWARD   |                  | 5<br>6               | 8.4<br>7.8       |              | 2<br>4                                 | 9.7<br>9.5                              |              | 27               |                                |
| 60 4.3 60 4.1 43°05.7', 87°26.7'  89 4.2 83 4.0 649 0 14.2  One cast missed. (winch failure) 1 11.4 6 10.9  43°03.0', 86°59.9' 4 9.2 12 8.6  640 0 11.0 9 8.3 18 5.6  1 11.0 17 5.8 22 4.9  3 10.6 23 4.8 48 4.4  4 10.4 34 4.5 60 4.1  7 8.9 42 4.1 92 4.1  10 8.4 60 4.0 TRANSECT TURNS  10 8.4 60 4.0 TRANSECT TURNS  NORTHWESTWARD   |                  | 10                   | 6.8<br>6.3       |              |  | $7.1 \\ 5.7$                            |              | 60               | ~~ ·~                          |
| 60 4.3 60 4.1 43°05.7', 87°26.7'  89 4.2 83 4.0 649 0 14.2  One cast missed. (winch failure) 1 11.4 6 10.9  43°03.0', 86°59.9' 4 9.2 12 8.6  640 0 11.0 9 8.3 18 5.6  1 11.0 17 5.8 22 4.9  3 10.6 23 4.8 48 4.4  4 10.4 34 4.5 60 4.1  7 8.9 42 4.1 92 4.1  10 8.4 60 4.0 TRANSECT TURNS  10 8.4 60 4.0 TRANSECT TURNS  NORTHWESTWARD   |                  | 34                   | 5.7              |              | 21<br>20                               | 5.0                                     |              | 69<br>80         | 4.1                            |
| 60 4.3 60 4.1 43°05.7', 87°26.7'  89 4.2 83 4.0 649 0 14.2  One cast missed. (winch failure) 1 11.4 6 10.9  43°03.0', 86°59.9' 4 9.2 12 8.6  640 0 11.0 9 8.3 18 5.6  1 11.0 17 5.8 22 4.9  3 10.6 23 4.8 48 4.4  4 10.4 34 4.5 60 4.1  7 8.9 42 4.1 92 4.1  10 8.4 60 4.0 TRANSECT TURNS  10 8.4 60 4.0 TRANSECT TURNS  NORTHWESTWARD   |                  | 45<br>45             | 5.1<br>5.1       |              | 53                                     | 4.4                                     | TRANSI       |                  |                                |
| One cast missed. (winch failure)  43°02.8', 87°15.8'  644  |                  | 53<br>60             | 4.4              |              | 50<br>60                               | 4.1                                     | 43°          |                  | 7°26.7'                        |
| 1       11.4       10       10.3         43°03.0', 86°59.9'       4       9.2       12       8.6         640       0       11.0       9       8.3       18       5.6         1       11.0       17       5.8       22       4.9         3       10.6       23       4.8       48       4.4         4       10.4       34       4.5       60       4.4         7       8.9       42       4.1       92       4.2         10       8.4       60       4.0       TRANSECT TURNS         12       7.8       65       4.0       NORTHWESTWARD   |                  |                      |                  | 43           | 83<br>02.81,87                         | 4.0<br>'°15.8'                          | 649          |                  | 12.0                           |
| 43°03.0', 86°59.9'       4       9.2       12       8.6         640       0       11.0       9       8.3       18       5.6         1       11.0       17       5.8       22       4.9         3       10.6       23       4.8       48       4.4         4       10.4       34       4.5       60       4.4         7       8.9       42       4.1       92       4.2         10       8.4       60       4.0       TRANSECT TURNS         12       7.8       65       4.0       NORTHWESTWARD  |                  |                      |                  | 644          | 0<br>1                                 | 77 4                                    |              |                  | 10.3                           |
| 10 8.4 60 4.0 TRANSECT TURNS<br>12 7.8 65 4.0 NORTHWESTWARD  | 43°              | 03.01, 86            | °59.9'           |              | 4                                      | 9.2                                     |              | 12               | 8.6<br>5.6                     |
| 10 8.4 60 4.0 TRANSECT TURNS<br>12 7.8 65 4.0 NORTHWESTWARD  | 040              | 1                    | 11.0             |              | 17<br>22                               | 5.8<br>5.8                              |              | 22               | 4.9                            |
| 10 8.4 60 4.0 TRANSECT TURNS<br>12 7.8 65 4.0 NORTHWESTWARD  |                  | <b>3</b><br>4        | 10.4             |              | 23<br>34                               | 4.5                                     |              | 60               | 4.4                            |
| 12 7.8 65 4.0 NORTHWESTWARD 17 7.4 80 3.8 28 5.4 43°02.8', 87°18.4' 43°07.6', 87°29.3' 35 4.8 645 0 12.2 650 0 14.4 38 4.7 1 12.2 1 13.0   |                  | 7<br>10              | 8.9<br>8.4       |              | 42<br>60                               | 4.0                                     | ŋ            |                  | ****************************** |
| 28 5.4 43°02.8', 87°18.4' 43°07.6', 87°29.3'<br>35 4.8 645 0 12.2 650 0 14.4<br>38 4.7 1 12.2 1 13.0   |                  | 12<br>17             | 7.8<br>7.4       |              | 65<br>80                               | 4.0<br>3.8                              | 1            | NORTHWESTW       | VARD                           |
| 38 4.7 1 12.2 1 13.0   |                  | 28<br>35             | 5.4<br>4.8       | 43°          | °02.81, 87                             | 7°18.4'                                 | 43°<br>650   | °07.61, 87<br>0  | 14.4                           |
| $\mu \gamma = \mu \gamma = \mu \gamma = \gamma = \gamma = \gamma = \gamma = \gamma = \gamma $  |                  | 38<br>117            | 4.7<br>4.5       | J , J        | 1 2                                    | 12.2<br>11.7                            | · <b>/</b> · | 1                | 13.0<br>12.8                   |

| Slide<br>No. | Depth,M<br>Corr.                                 | Temp.°C<br>Corr.  | Slide No.        | Depth,M<br>Corr.  | Temp.°C<br>Corr.   | Slide No.    | Depth, M                                | Temp.°C  |
|--------------|--|---|------------------|---|--|--------------|---|--|
| No.<br>650   | 4<br>9<br>15<br>18                               | 11.0<br>10.1<br>7.7<br>7.1  | 654              | 28<br>35<br>60<br>74  | 4.8<br>4.4<br>4.1<br>4.1   | No.<br>659   | 5<br>9<br>14<br>15<br>22                | 9.7  |
|              | 21<br>27<br>36<br>60<br>86                       | 6.3<br>5.1<br>5.4.6   | 655              | 0   | 737.1'<br>15.2<br>14.1<br>12.5<br>10.7   |              | 33<br>42<br>60<br>90                    | 7.52<br>6.52<br>4.2<br>3.7   |
| 43°<br>651   | '08.2', 87<br>0<br>4<br>7                        | 14.4<br>13.7<br>12.5  |                  | 5<br>15<br>25<br>25<br>34<br>60   | 5.6<br>5.4.5<br>4.2  | 660          | '19.1', 87<br>0<br>2                    | 15.4<br>12.0<br>11.6   |
|              | 9<br>11<br>13<br>15<br>18                        | 10.9<br>10.0<br>9.5<br>9.1<br>7.5   | 43°<br>656       | 60<br>714.3', 87<br>0<br>1<br>4   | 4.2<br>738.91<br>14.9<br>14.9<br>12.4  |              | 4<br>6<br>16<br>22<br>30<br>39          | 9.710932<br>4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.   |
| 1130         | 21<br>36<br>60<br>88                             | 7.0<br>5.4<br>5.1   |                  | 5<br>6<br>8<br>14   | 12.0<br>11.0<br>10.4<br>9.6<br>8.0   | 43°          |   | 4.1<br>4.0<br>7°47.51  |
| 43°<br>652   | 0<br>1<br>9<br>11                                | 15.0<br>13.2<br>9.6<br>8.8<br>7.8<br>6.1  |                  | 17<br>20<br>22<br>26<br>30<br>36<br>60  | 7.0<br>6.9<br>4.2<br>4.0   | 661          | 0<br>1<br>2<br>3<br>7<br>11<br>15       | 15.4<br>12.5<br>11.7<br>9.4<br>7.5   |
|              | 13<br>15<br>16<br>23<br>30<br>60<br>63           | 5.7<br>4.6<br>4.2<br>4.2  | 657              | 114<br>15.9', 87<br>0<br>1<br>3   | 15.0<br>15.0<br>13.0   | 43°          | 15<br>23<br>26<br>39<br>52<br>21.5', 87 | 6.5<br>5.7<br>5.1<br>5.0   |
| 43°<br>653   | 10.6', 87<br>0                                   | °33.6'<br>14.7  |                  | 1<br>3<br>6<br>7<br>9<br>12<br>13<br>18<br>23<br>27<br>60<br>102<br>16.7', 87 | 10.3<br>10.9<br>10.9<br>9.3<br>9.8<br>5.0<br>4.0<br>12.6<br>12.6<br>10.5<br>10.1<br>13.9<br>14.6<br>14.5 | 662          | 0<br>2<br>5<br>8<br>11<br>22<br>30      | 15.5<br>12.9<br>15.0<br>99.8<br>12.9<br>76.4<br>15.4<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8<br>11 |
|              | 3<br>8<br>15<br>19<br>21<br>27<br>36<br>60<br>67 | 12.4<br>11.3<br>10.5<br>4.7<br>4.1<br>4.1<br>4.1<br>4.1<br>15.2<br>10.2<br>10.8<br>10.8<br>10.8<br>10.9<br>9.4<br>7.2 | 43°              | 23<br>27<br>60<br>102<br>16.7', 87  | 5.0<br>4.9<br>4.4<br>4.0   | — 43°<br>663 | 30<br>22.7', 87<br>0<br>2<br>3          | 6.2<br>250.8<br>15.5<br>12.4<br>11.8   |
| 43°<br>654   | 11.8', 87<br>0 2<br>3 4<br>6 8<br>14<br>18 21    | 35.21<br>15.0<br>12.2<br>12.2   | 050              | 1<br>3<br>4<br>5<br>23<br>60<br>104<br>17.8', 87<br>0<br>1                    | 15.2<br>12.6<br>12.0<br>10.5<br>10.0   |              | 0<br>2<br>3<br>4<br>6<br>8<br>10<br>15  | 9.8<br>8.7<br>8.4<br>8.2   |
|              | 6 8  | 10.2  | <del>- nso</del> | 60<br>104   | 4.1<br>3.9   |              | Trace lo                                | ost.   |
|              | 18<br>21<br>23                                   | 9.6<br>9.4<br>7.2   | 659              | 1,.0°, 67<br>0<br>1<br>3  | 14.6<br>14.5<br>12.0   |              |   |  |

# South of Muskegon to North of Milwaukee 24 July 1963

| Slide<br>No. | Depth,M<br>Corr.                                     | Temp.°C<br>Corr.  | Slide<br>No.     | Depth,M<br>Corr.                                       | Temp.°C Corr.                               | Slide<br>No. | Depth,M<br>Corr.                            | Temp.°C<br>Corr.  |
|--------------|--|---|------------------|--|---|--------------|---|---|
| 43°          | 06.51, 86  | °18.0'  | 43°              | 07.01, 86  | °30.81                                      | 43°          | 707.4, 86°                                  | 40.4  |
| 669          | Ō  | 20.2  | 674              | ō  | 19.9  | 678          | 0   | 18.9  |
|              | )<br>7   | 19.4<br>18.6  |                  | 1<br>1   | 18.2<br>13.5                                |              | ð   | 17.4  |
|              | 8  | 17.0  |                  | 13   | 8.2   |              | . 9   | 9.9<br>9.2  |
|              | 9  | 16.7  |                  | 17   | 7.2   |              | 11  | 8.5   |
| 43°          |  | °20.7'  |                  | 23<br>29<br>60   | 6.7   |              | 17  | 7.1   |
| 670          | 0<br>3   | 20.4<br>17.8  |                  | 29<br>60   | 6.4<br>5.0                                  |              | 37<br>63                                    | 6.3<br>5.8  |
|              | 5  | 16.7  |                  | 102  | 5.9<br>5.6                                  |              | 37<br>63<br>106                             | 7.1<br>6.3<br>5.6   |
|              | 58   | 13.1  | <sup>3</sup> 43° |  | *32.9                                       | 43°          | 07.51, 86                                   | 42.61   |
|              | 13   | 7.5<br>6.8  | 675              | 0  | 18.3  | 679          | 0   | 19.0  |
|              | 20<br>24   | 6.8<br>6.7  |                  | 2  | 18.2<br>14.8                                |              | 5<br>10                                     | 14.4  |
|              | 28   | 6.6   |                  | 7  | 13.2  |              | 13  | 8.9<br>8.2  |
| 43°          |  | °22.91  |                  | ıi   | 8.8   |              | 13<br>14                                    | 7.6   |
| 671          | 0  | 20.8  |                  | 12   | 8.2   |              | 17  | 7.1   |
|              | 2  | 19.5<br>16.6  |                  | 20   | $\substack{7.1\\6.7}$                       |              | 79<br>29                                    | 6.5<br>6.3  |
|              | 4  | 15.2  |                  | 23<br>29   | 6.5   |              | 66  | 6.0   |
|              | 7  | 11.6  |                  | 35   | 6.3   |              | 17<br>29<br>42<br>66<br>78<br>106           | 5.8   |
|              | 10   | 9.9<br>8.8  |                  | 54<br>84   | 6.0   | 1100         | 106   | 5.6   |
|              | 16<br>25   | 6.8<br>6.3  |                  | 106  | 5.6<br>5.6                                  | 680          | 07.61, 86                                   | 18.0  |
|              | 25<br>33   | 6.0   | 43°              |  |   | 000          | ì   | 18.9<br>18.7  |
|              | 40   | 5.9   | 676              | , o  | 18.7  |              | 2   | 18.3  |
| 43°6<br>672  | 06.81, 86  | °25.91  |                  | 4  | 18.0  |              | 4   | 15.0  |
| 0/2          | i<br>i   | 20.4<br>18.2  |                  | 8  | 13.2<br>11.6                                |              | 6<br>8<br>9<br>12                           | 10.6<br>8.9   |
|              | . 2  | 14.9  |                  | 14   | 9.6   |              | 9   | 8.3   |
|              | 3  | 13.8  |                  | 15<br>18   | 8.6   |              | 12  | 8.9<br>8.3<br>7.2   |
|              | 3<br>5<br>9  | 11.6  |                  | 18   | 8.0   |              | 14  | 7.2   |
| •            | 13   | 9.6<br>8.0  |                  | 23<br>25   | 6.8   | • •          | 17<br>30                                    | 6.7<br>6.3  |
|              | 13<br>16   | 78  |                  | 30   | 6.8<br>6.6                                  |              | 30<br>61                                    | 5.8   |
|              | 20   | 6.9   |                  | 55   | 6.0   |              | 79  | 5.7   |
|              | 31   | 6.2   |                  | 55<br>79<br>106  | 6.0<br>5.8<br>5.6                           |              | 79<br>85<br>99                              | 6.3<br>5.7<br>5.7<br>5.6  |
|              | 48<br>48   | 5.7   | 43°              | 07.31, 86  | <b>'27 71</b>                               | 43°          | <del>99</del><br>07.7', 86                  | °47.81  |
|              | 31<br>40<br>48<br>60                                 | 6.9<br>6.2<br>5.7<br>5.6  | 677              | 0,   | 19.2<br>16.6<br>15.9<br>13.2<br>10.7<br>8.6 | 43°<br>681   | 0   | 19.5  |
| 43°          | 06.91,86   | °28.01  |                  | 4  | 16.6  |              | 1   | 18.6  |
| 673          | . 2  | 20.6  | • .              | 5<br>7   | 15.9  |              | 3<br>4                                      | 17.2  |
|              | 3  | 13.2  |                  | 12   | 10.7  |              | 7   | 10.0  |
|              | 5  | 11.0  |                  | 15   | 8.6   |              | 9   | 8.3   |
|              | 11   | 7.6   |                  | 18   | 7.7   |              | 11  | 8.0   |
|              | 5.3 *<br>∓ (   | 7.0<br>6.5  | 1 4              | 0<br>4<br>57<br>12<br>18<br>18<br>24<br>30<br>53<br>61 | 6.8   |              | 12<br>15                                    | (・5<br>7 . 1  |
|              | 29   | 6.3   |                  | 30   | 6.5   |              | ī́8   | 6.8   |
|              | 38   | 6.2   |                  | 53   | 5.9   |              | 24  | 6.6   |
|              | 65<br>71   | 5.9   | •                | 61<br>01   | 766.59766                                   |              | 30<br>61                                    | 6.3   |
|              | 0<br>2<br>3<br>11<br>23<br>23<br>8<br>51<br>77<br>90 | 2.1<br>5.7  |                  | 91<br>101  | 5.6<br>5.6                                  |              | 9<br>11<br>12<br>15<br>18<br>24<br>30<br>96 | 8, 19.6<br>19.6<br>17.0<br>15.0<br>15.0<br>15.0<br>88.7<br>76.6<br>55.6 |
|              | 90   | 28.0'<br>28.0'<br>20.6<br>19.2<br>11.0<br>7.53<br>6.3<br>5.7<br>5.6 |                  |  |   |              |   | Secretary control   |

| No. Cor   | r. Corr.  | No.                                     | Corr.   | Corr.  | No.         | Corr.  | Corr.   |
|---|---|---|---|--|-------------|--|---|
| 43°07.8,  | 86°50.4'  | 43°                                     | 708.3 کی  | 37°02.91   | 692         | ,10  | 11.6  |
| 682 o   | 19.2<br>14.7  | 687                                     | 0   | 20.3<br>18.8   | 4.4.1.2     | 14   | 8.6   |
| 6   |   | e war and a second                      | 5   | 15.7   |             | 23   | 6.0   |
| 6   | 8.3<br>7.8  | - •                                     | 7.1   | 11.6   |             | 42   | 5.6   |
| 17  | 7.2   |   | 13  | 9.9  |             | 54<br>77                                     | 5.6<br>5.6<br>5.6   |
| 24  | 6.7   |   | 19  | 9.9<br>7.7   |             | 08.91, 8                                     |   |
|   |   |   | 19<br>23  | 6.7  | 693         | 00.5, 0                                      | 20.9  |
| 3C<br>41  | 5.9   |   | 30  | 6.2  | <b>U</b>    | š  | 18.2  |
| 61  | 5.7   |   | 30<br>39<br>48  | 5.9<br>5.7   |             | 5  | 14.6  |
| 93  | 5.6   | ,                                       | 48  |  |             | 8  | 10.5  |
| 43°07.9'<br>683 0                                 | , 86°53.0'  |   | 60<br>86  | 5.7  |             | 12   | 7.7   |
| 683 C   | 19.8  | 1130                                    | 86  | 5.6  |             | 17   | 6.7   |
| L<br>Ji   | . 10.0  | 688                                     |   | 20.5   |             | 25<br>29                                     | 5.7   |
| 7   | 14.3  | 000                                     | 0   | 18.8   |             | 29   | 5.6<br>5.6<br>5.6   |
| 10  |   |   | 7   | 11.8   |             | 41<br>75                                     | 5.6<br>5.6  |
| 14  |   | *                                       | 15  | 8.1  | <u> ДЗо</u> | <del>09.01, 8</del>                          |   |
| 18  | 7.3   |   | 19  | 7.1  | 43°<br>694  | 0  | 21.0  |
| 26  | 6.6   |   | 28  | 6.1  | ٠, د        | ž  | 21.0<br>18.9  |
| 41  | . 5 <b>.</b> 9  | **                                      | 41  | 5.7  |             | 4  | 16.5  |
| 47<br>87  | 5.7   | 1100                                    | 81  | 5.6  |             | 6  | 11.7  |
| 43°08.0'<br>684 0                                 | 5.6   | 690                                     |   | 37°08.91<br>20.9   |             | 8  | 10.0<br>8.3   |
| 68/I 00.0°  | , 86°55.8'<br>20.1                                      | 689                                     | 0   | 20.9   |             | 11   | 8.3   |
| 004 0   | 15.6  |   | 12  | 9.4  |             | 12   |   |
| 8   | 12.6  |   | 13  | 8.3  |             | 17   | 6.3   |
| 10  |   |   | 21  | 6.5  |             | 23<br>35                                     | 55.6<br>55.6  |
| 12  | 8.3   |   | 24  | 6.1  | •           | 35<br>41                                     | 5.6   |
| 15  | 7.4   |   | 30<br>42  | 5.9  |             | 70   | 7.2<br>76.3<br>55.6<br>5.6<br>5.6   |
| 15<br>23<br>37<br>46                              | 6.8   |   | 42  | 5.7  | 43°         |  | 7°23.3'   |
| 37  | 6.0   | ە دىر                                   | 81  | 5.6  | 695         | O  | 21.0  |
| 40<br>52  | 5.8<br>5.7  | 690                                     | 08.6', 8<br>0   | 7°10.6'<br>20.9  |             | 4  | 15.6  |
| 52<br>89  | 5.6   | 090                                     | 2   | 19.9   |             | 10   | 9.2<br>7.4  |
| 43°08.1'  |   |   | 7   | 17.2   |             | 15<br>18                                     | 6.6   |
| /O= -   |   |   | ıi  | 12.8   |             | 30   | 5.8   |
| 3   | 15.5  |   | 14  | 10.0   |             | 30<br>74                                     | 5.8<br>5.6  |
| 7   | 14.1  |   | 11<br>14<br>18<br>21<br>27<br>49<br>76                  | 10.0<br>7.4<br>6.7<br>5.9                                      | 43°<br>696  | 09.21, 8                                     | 7°25.4i   |
| 12  | 8.9   |   | 21  | 6.7  | 696         | 0  | 20.8  |
| 15  | 8.2   |   | 27  | 5.9  |             | 3  | 18.3  |
| 28  | (·1   |   | 49<br>76  | 5.7<br>5.6   |             | 0<br>3<br>12<br>16                           | 8.9   |
| 685<br>3<br>7<br>12<br>15<br>21<br>28<br>43<br>52 | 20.2<br>15.1<br>14.1<br>8.2<br>7.3<br>5.7<br>6.5<br>5.6 | 43°                                     | 08.71, 8  | 7°13.3'  |             | 16   | 20.8<br>18.3<br>8.9<br>7.4<br>5.9<br>5.7<br>5.6                                   |
| 52<br>52  | 5.7   | 69i                                     | 0,  | 20.9   |             | 21   | 5.0   |
| 90  | 5.6   |   | 1   | 20.5   |             | 30<br>49<br>61                               | 5·9   |
| 43°08.21  | ,87°00.6'   |   | 2<br>6  | 19.3   |             | 61   | 5.6   |
| 686 0   | 5.6<br>, 87°00.6'<br>20.5<br>15.5<br>13.2<br>8.2<br>7.1 |   | 6   | 18.2   | 43°         | 09.37, 87                                    | 7°29.0'   |
| 3<br>8<br>14<br>17<br>22                          | 15.5  |   | 11  | 12.7   | 697         | 0  | 21.0  |
| ال ا  | 13.2  |   | 16  | 8.2  |             | ļ  | 20.0  |
| 14  | 7.1   |   | 28  | 7.8  |             | 4  | 16.1  |
| 55  | 6.6   |   | 20<br>36  | 0.2<br>5.0   |             | -8   | 13.9  |
| 29  | 6.2   |   | 48  | 5.6  |             | 12   | 8.9   |
| 29<br>60<br>88                                    | 7.1<br>6.6<br>6.2<br>5.7<br>5.6                         |   | 70  | 7°13.3'<br>20.5<br>20.5<br>19.2<br>12.7<br>8.2.9<br>6.9<br>5.6 | ,           | 57   | 6.4<br>6.1  |
| 88  | 5.6   | 43°                                     | 0 <del>8.81,8</del>                                     | 7°15.9'  | 144         | 37   | 5.7   |
|   |   | 692                                     | 0   | 20.8   |             | 8<br>12<br>18<br>24<br>37<br>72<br>09.41, 87 | 5.7<br>5.6<br>7°29.0'<br>21.0<br>20.0<br>16.1<br>13.9<br>6.4<br>6.1<br>5.7<br>5.6 |
|   |   |   | 6<br>11<br>16<br>17<br>28<br>36<br>48<br>70<br>08.8', 8 | 7°15.9'<br>20.8<br>19.6<br>16.7                                | <u> 43°</u> | 09.41, 87                                    | 21.0  |
|   |   | *************************************** | 7   | 10./   | 698         | 0  | 21.0  |
|   |   |   | 21A   | )  |             |  | •   |

|              |  |   |              |   |               |              |                  | ,       |
|--------------|--|---|--------------|---|---------------|--------------|------------------|---------|
| Slide<br>No. | Depth,M<br>Corr.   | Temp.°C   | Slide<br>No. | Depth,M<br>Corr.  | Temp.°C Corr. | Slide<br>No. | Depth,M<br>Corr. | Temp.°C |
| 698          | 5<br>12  | 15.6<br>7.8   | 701          | '09.8', 87<br>0   | 20.9          |              |                  | •       |
|              | 16   | 7.5<br>6.8  |              | 3<br>5  | 15,0<br>11.4  |              |                  | •       |
|              | 20<br>26<br>32<br>35   | 6.0<br>5.8<br>5.7   |              | 9<br>13   | 8.9<br>7.2    |              |                  |         |
| 43           | '09.4', 87   | 5.7<br>34.5'<br>20.5  |              | 16<br>23  | 6.5<br>6.0    |              |                  |         |
| 699          | O<br>4   | 16.9  | 110          | 3<br>5<br>9<br>13<br>16<br>23<br>33<br>59<br>'09.8', 87 | 5.7<br>5.6    |              |                  | ,       |
|              | 11<br>16   | 10.0  | 705          | 0   | 21.5<br>19.4  |              |                  |         |
|              | 20<br>25   | 7.2<br>6.4  |              | 1<br>5<br>7   | 13.9<br>8.9   |              |                  |         |
|              | 25<br>31<br>37<br>50<br>77                                     | 5.7<br>5.7<br>5.6   |              | 5<br>7<br>9<br><b>23</b><br><b>2</b> 9                  | 7.1           |              |                  |         |
| ग्रद         | 77<br>'09.5', 87   | 5.6   |              | 29  | 6.7<br>6.7    |              |                  |         |
| 700          | 0  | 37.1'<br>20.3<br>15.6   |              |   |               |              |                  |         |
|              | 5<br>14<br>17  | 10.4<br>9.4   |              |   |               |              |                  |         |
|              | 23<br>26   | 7.2<br>6.7  |              |   |               |              |                  |         |
|              | 29<br>37   | 6.3   |              |   |               |              |                  |         |
|              | 17<br>23<br>26<br>29<br>37<br>43<br>61<br>87                   | 6.8<br>5.7  |              | •   |               |              |                  |         |
|              | '09.6', 87   | 7°40.01   |              |   |               |              |                  |         |
| 701          | 0<br>2<br>6  | 20.7<br>19.4  |              |   |               |              |                  |         |
|              |  | 8.3   |              |   |               |              |                  |         |
|              | 25<br>32   | 6.2<br>5.8  |              |   |               |              |                  |         |
|              | 16<br>19<br><b>2</b> 5<br><b>32</b><br>35<br>84                | 14.2<br>14.3<br>86.2<br>55.5<br>55.5                                      |              |   |               |              |                  |         |
| 702          |  | 5.7<br>5.6<br>7°42.9'<br>20.7<br>19.6<br>12.6<br>7.8<br>6.7<br>6.8<br>5.6 |              |   |               |              |                  |         |
| ,            | 2  | 19.6<br>12.6  |              |   |               |              |                  |         |
|              | 14<br>23   | 7.8<br>6.7  |              |   |               |              |                  |         |
|              | 29<br>54   | 6.0<br>5.8  |              |   |               |              |                  |         |
| 43           | 709.71, 87<br>0 2<br>8 14<br>23<br>29<br>54<br>83<br>09.81, 87 | 5.6<br>7°45.41  |              |   |               |              |                  |         |
| 703          | 0<br>2   | 20.7<br>16.3  |              |   |               |              |                  |         |
|              | 9  | 10.2  |              |   |               |              |                  |         |
|              | 0<br>2<br>4<br>9<br>13<br>17<br>28                             | 20.7<br>16.3<br>14.1<br>10.2<br>7.5<br>6.6<br>6.0                         |              |   |               |              |                  |         |

# STUDIES ON WATER MOVEMENTS AND SEDIMENTS IN SOUTHERN LAKE MICHIGAN

Part II. The Surficial Bottom Sediments in 1962-1963

John C. Ayers Jack L. Hough

ORA Project 05466

Part II of the Final Report of H.E.W. Contract PH-86-63-60

GREAT LAKES RESEARCH DIVISION Special Report No. 19

INSTITUTE OF SCIENCE AND TECHNOLOGY
THE UNIVERSITY OF MICHIGAN
ANN ARBOR, MICHIGAN

January 31, 1964

## PREFACE TO THE ENTIRE REPORT

Several factors have dictated that this final report should be in separate parts.

The contract covered studies of different sorts. By the nature of the studies, the times required for work-up and analysis of data have varied widely, some parts being completed long before others could be finished. The different studies have required greatly varying amounts of ship-time and some, which required unexpectedly large amounts of ship-time, are being augmented by data obtained during cruises for other projects when vessels are in suitable regions. Finally, it is believed that assimilation by the reader is aided by brevity and unit reporting.

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#### INTRODUCTION

This study of present-day surficial bottom sediments of the southern basin of Lake Michigan was carried out for two reasons: to expand and complete the coverage obtained by Hough (1935), and to ascertain whether there have taken place any recognizable changes in the composition of the bottom sediments in the thirty years that have lapsed since his studies.

Hough, operating from a small sailboat with little gear and insufficient help, was able to cover a significant portion of the southern basin. His coverage was sufficient that if sediment changes have taken place as a result of eutrophication, they should be detectable.

If the eutrophication process has not yet progressed to the point where there has been recognizable change of sediment type, Hough's map of bottom sediments should be filled in and made as complete as possible in order that there may be a map against which to determine the onset of eutrophication-caused sediment-type changes if they occur in the future.

#### METHODS

The 524 samples upon which this report is based are indicated in Figure 1.

The samples were for the most part in lines roughly perpendicular to shore, the lines being from five to 15 miles apart. In each line the sampling intervals usually were: at one-mile intervals from the 1st through the 10th mile from the beach, at 2-mile intervals from the 10th through the 20th mile, and at 5-mile intervals thereafter. In the center of the basin 23 samples were taken in four lines down the slope toward the deepest portion. A single sample was taken off, and between, the lakeward ends of lines IV and V. Figure 1 shows that coverage of the basin is not complete, and that an additional line is needed between lines XXVIII and XXIX.

The sample numbers, distances from shore, depths of water, and field descriptions of the sediments are given in the Appendix. Sample numbers are consecutive by time of taking. Some lines were taken on courses toward shore, others on courses away from shore.

With the exception of about eighteen samples, all samples were taken with the dwarf orange-peel sampler. Fifteen of the samples were cores and two or three were obtained with the Smith-McIntyre sampler (a spring-loaded modification of the Petersen dredge).

Navigation was by radar range and bearing out to about the 20th mile, beyond which navigation was by dead-reckoning.

The bathymetry shown in Figure 1 was provided by Prof. Hough

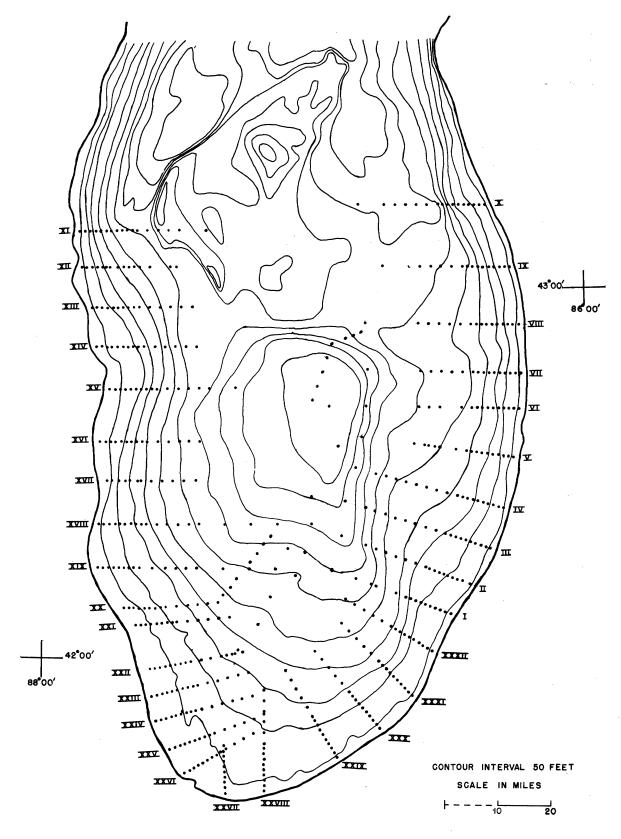


Fig. 1. Present bathymetry and sampling locations, survey of 1962-1963.

and was derived from the detailed field sheets (boat sheets) of the U. S. Lake Survey. This bathymetry represents the bestpossible synthesis of all the sounding data of the Lake Survey up to the present. The depth-contour interval is 50 feet.

Figure 2 presents Hough's 1935 sediment map, reproduced without latitude-longitude lines or state lines. It is also without three 90-fathom depth contours in the deepest portion, these depths having proven to be false.

The bathymetry of Figure 2 was constructed by Prof. Hough in the early 1930's and represents the then best-possible synthesis of the Lake Survey data of that time. The depth-contour interval of this figure is 10 fathoms.

Figure 3 presents the results of our bottom sediment survey.

It is necessary to explain here certain aspects of the preparation of this map.

The edges of the several sediment types in Figure 3 have been placed halfway between the pairs of differing samples that require a boundary somewhere between them. Probably a certain amount of error in the positioning of boundaries has resulted from this practice.

In the north-central portion of the basin, where boundaries appear to cross the basin but where additional samples are needed, question marks along the boundaries indicate our uncertainty as to their locations.

This map was prepared from the field descriptions of sediment type(s). By "field description" is meant a phenotypic description based upon combined visual inspection, testing for odor, and feeling of the sediment with the fingers. Field description

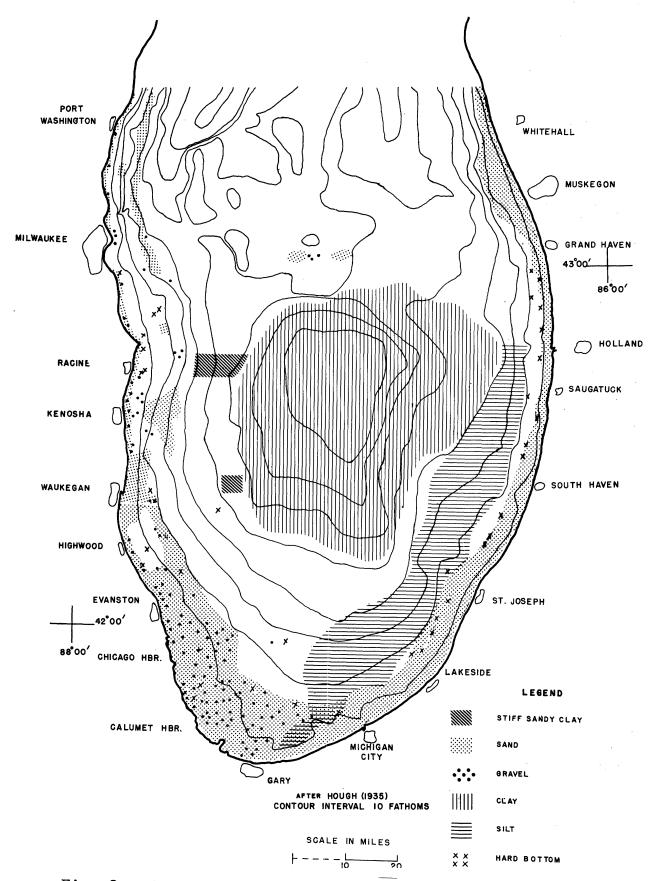


Fig. 2. Hough's 1935 sediment map and bathymetry.

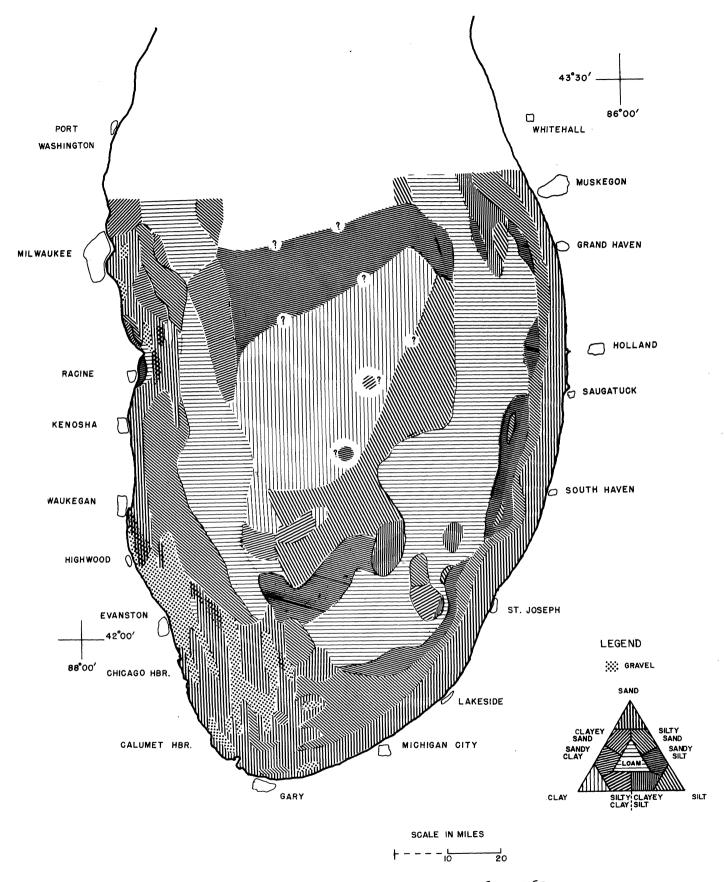


Fig. 3. The surficial sediments of 1962-1963.

is a combination of the observations carried out on board ship, when the sample was fresh, and re-examination of the material in the laboratory under a binocular microscope with a metric scale in the field of view. The term is used as an opposite to any of the several means of designating sediment type by the measured proportions of sand, silt, and clay determined in particle-size analyses.

Each sample has been placed subjectively in a sediment-type category on the basis of the field description of the uppermost sediment layer, even if it was only a thin surface layer.

The sediment-type categories used follow the triangular-graph categorization of Shepard (1954) except that a subjective basis rather than a percentage-composition basis is used. "Loam" in the center of the triangle represents the several 3-way combinations of sand, silt and clay (sandy silty clay, clayey sandy silt, silty clayey sand, etc.).

The use of only the uppermost sediment layer was dictated by the fact that sediment-type changes resulting from eutrophication will first be evident in the thin surficial layers.

The use of the field description of sediment type was necessary for three reasons: 1) eutrophication-caused changes will probably be first visible as significant color changes in the surface layer as it modifies toward the organic sediments (if not between Hough's survey and this, then between this and some future survey), 2) the presence of unnatural odors is detected most surely in the field observation of the fresh sediment, and 3) sufficient funds for the scraping-off and analysis of samples of the uppermost sediment layer were not available.

#### RESULTS AND DISCUSSION

The basic purpose of this report is to present the tabulated data of the Appendix, but in order that these data may be visualized Figure 3 has been prepared.

Comparisons between Figures 2 and 3 are the present best available means of determining whether the intervening period of 30 years has produced differences in the composition of the surficial sediments.

In one sense these figures are only partially comparable: Figure 2 is based upon the results of particle-size analyses augmented by field descriptions obtained from U. S. Lake Survey charts; Figure 3 is based only upon field descriptions. Incomparability becomes greatest in cases where a thin layer of a sediment of one type overlies a thick layer of a sediment of a different type. Partical-size analysis of a split "representative sample" gives most statistical weight to the thicker second layer and is not apt to detect the environmental change represented by the thin surficial layer. Plots of field descriptions of the uppermost layer, however thin it may be, take no account of the underlying layer(s) and are not based upon the concept of the "representative sample" or aliquot thereof.

Fortunately, the numbers of cases where greatly different sediment types occur in layered configurations are not numerous. For this reason there is a degree of justification for cross-comparisons between Figures 2 and 3.

## Comparisons of Figures 2 and 3

The primary result of comparison of these figures is that

over most of the lower lake, there is no conclusive demonstration of change in the surficial sediments since the early 1930's.

In the central portion of the basin apparent differences in sediment types involve, in large part, those distinctions between proportions of sand and silt or silt and clay that are least accurately made by the field descriptions. The apparent differences are believed not to be real, but rather effects of masking (in Fig. 2) due to the weight given to a second thicker layer by partical-size analysis of representative samples.

Along the shores there are but minor differences between the two figures. The differences for the most part, again, involve the judgment of proportions of sand and silt or silt and clay.

In the area off Chicago and its environs there are some differences in position of gravel and sand in the two figures.

These sediments are quite accurately assessed by the field description; they also are sediments more apt to be non-layered through the depths reached by a grab sampler. The positional differences are taken to indicate that sand bars move or migrate in the region off Chicago.

The more complete spatial coverage upon which Figure 3 is based allows the elimination of open spaces (<u>terrae incognitae</u>) that were necessary in Figure 2. It is to be noted, however, that our coverage is not complete, and that some sediment-type boundaries will move if more-closely spaced samples are obtained.

# Samples of Special Note

In only eight of the samples were there evidences that man's activities have resulted in modification of the native lake-bottom

sediments. These samples, their locations, and their field descriptions are given in Table 1.

Table 1. Samples of Special Note

| Sample<br>No. | Location  | Description  |
|---------------|---|--|
| I-11          | ca 12 miles, 290°<br>true, off Benton<br>Harbor | Black sandy clayey silt over brown sandy silt over gray silt.                  |
| XXV-1         | l mile, 70° true,<br>off Calumet Harbor         | Gravel over gray stiff sandy clay. Foul odor.                                  |
| XXVI-6        | 8 miles, 60° true, off Indiana Harbor           | Mottled gray and brown silty fine sand. Odor of oil.                           |
| XXVI-7        | 7 miles, 60° true, off Indiana Harbor           | Mottled gray and brown silty fine sand. Odor of oil.                           |
| 8-IVXX        | 6 miles, 60° true, off Indiana Harbor           | Fine sand with some organic matter, cinders, wood. Odor of oil.                |
| XXVII-6       | 6 miles, 0° true, off Gary, Indiana             | Coarse sand. Odor of oil.  |
| XXVII-7       | 7 miles, 0° true, off Gary, Indiana             | Dark gray silty very fine sand with some vegetable matter. Strong odor of oil. |
| XVIII-5       | 5 miles, 0° true, off Burns Ditch               | Coarse sand-fine gravel over gray silty very fine sand.  Odor of oil.          |

In Table 1 there have not been included a few samples in which cinders were present. Nor does the table include samples XXIII-5 or XXIII-6 (5 and 6 miles off Chicago Harbor) which contained, respectively, pieces of ceramic tile and rusty nails. These are mentioned here as evidences of dumping activity past or present, but are omitted from the table as being of little significance to the eutrophication process.

The black surface sediment of sample I-ll is of interest because it was the only sample of the survey whose color was sufficient to be called <u>black</u>. There are numerous instances of gray sediments which cannot be shown to be related to eutrophication (though it is suspected that some are).

Sample I-11 appears to be too distant and too far west to be a reflection of organic contributions from the St. Joseph River.

At present nothing is known of the origin of its black color.

# The Area of Possibly Modifying Sediments

The remaining seven samples of Table 1 may represent: 1) incipient modification of lake-bottom sediments as a result of man's activities, or 2) temporary effects of dumping of petroleum products, or 3) temporary results of shipwreck of tankers or oil barges in the region.

From the data presently at hand it cannot be ascertained which of the three possibilities above is(are) responsible for the oil odor in the sediments.

Despite our inability to assign a cause or causes it is significant that the sediments of an area ranging from one to three miles wide and more than 15 miles long, situated in the heavily-populated heavily-industrialized end of the lake, have been found to exhibit deteriorative effects attributable to man. Even if the present effects prove to be temporary, the area in which they occur should be well-noted as an area where definitive eutrophic deterioration should be watched for.

#### SUMMARY AND CONCLUSIONS

- 1. Five hundred and twenty-four samples of the surficial sediments taken in 1962-63 are the basis of this report. The coverage represented is good, though not complete.
- 2. Comparison of this survey to that of Hough (1935) does not demonstrate changes in sediment type as such over the 30-year intervening period.
- 3. Seven samples in the southern extremity of the lake (off Calumet Harbor, Indiana Harbor, Gary, and Burns Ditch) give olfactory evidence that organic materials are being incorporated into the sediments, though the process appears to have not yet gone to the point of causing changed sediment-type or changed sediment color.
- 4. Six of these seven samples indicate the incorporation of oil into the sediment.
- 5. It is suggested that the region where oil odor is now present is one that should be watched for evidences of future definitive eutrophic deterioration.

## REFERENCES

- Hough, J. L. 1935. The bottom deposits of southern Lake Michigan. Jour. Sed. Petrol., 5(2) 57-80.
- Shepard, F. P. 1954. Nomenclature based on sand-silt-clay ratios. Jour. Sed. Petrol., 24(3) 151-158.

# APPENDIX

Sample numbers, sample positions, and field descriptions of sediment types. Bottom samples taken between 7 August 1962 and 18 November 1963. All compass directions indicated are in degrees true.

Line I; bearing 290° from Benton Harbor pierhead

| Sample<br>No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description   |
|---------------|---------------------------|-----------------|---|
| 1             | 1                         | 53              | Medium sand   |
| 2             | 2                         | 67              | Fine sand   |
| 3             | 3                         | 76              | Fine sand   |
| 4             | 4                         | 84              | Very fine sand  |
| 5             | 5                         | 93              | Silty very fine sand  |
| 6             | 6                         | 106             | Silty very fine sand  |
| 7             | 6.9                       | 115             | Silty very fine sand  |
| 8             | 8                         | 128             | Very-fine-sandy silt  |
| 9             | 9                         | 147             | Very-fine-sandy silt  |
| 10            | 10                        | 175             | Dark gray silt  |
| 11            | 12 ?                      | 250             | Black sandy clayey silt over brown sandy silt over gray silt            |
| 12            | 16                        | 282             | Brown silty sand  |
| 13            | 17                        | 304             | Brown sandy clayey silt   |
| 14            | 20                        | 334             | Grayish-brown clayey silt   |
| 15            | 25                        | 365             | $\frac{1}{4}$ " gray sandy silt over red-brown slightly-sandy soft clay |

<sup>&</sup>quot; = inch

Line II; bearing 110° from E. shore, 6.7 miles N.E. of Benton Harbor pierhead

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|------------|------------------------|-----------------|---|
| 16         | 1                      | 52              | Fine sand   |
| 15         | 2.5                    | 66              | Very fine sand  |
| 14         | 3.4                    | 73              | Medium-coarse sand  |
| 13         | 4.4                    | 83              | Medium-fine sand  |
| 12         | 5.4                    | 91              | Fine-to-very-fine sand  |
| 11         | 6.3                    | 99              | Grayish-buff silty very fine sand   |
| 10         | 7.2                    | 108             | Grayish-buff silty very fine sand   |
| 9          | 8.2                    | 119             | Gray sandy clayey silt  |
| 8          | 9.2                    | 126             | Gray sandy clayey silt  |
| 7          | 10.1                   | 134             | Gray sandy clayey silt  |
| 6          | 12                     | 156             | Gray clayey silt  |
| 5          | 14                     | 199             | Gray clayey silt  |
| 4          | 16                     | 233             | Gray slightly-sandy clayey silt   |
| 3          | 18                     | 255             | Grayish-buff sandy clayey silt  |
| 2          | 20                     | 285             | Grayish-buff sandy clayey silt  |
| 1          | 22                     | 358             | Grayish-buff sandy clayey silt  |
| 17         | 27                     | 427             | <pre>1/16" gray silt over gray slightly-<br/>sandy silty clay</pre>   |
| 18         | 33                     | 425             | 1/2" gray silt over 1" of layered clay structure in 1/8" layers. First four layers of gray clay then alternating layers of gray and orange slightly-sandy clay; below last layer of orange clay a fine line of black. Clay below black line shades from gray to red-brown and is soft sandy clay. |

Line III; bearing 287° from E. shore 7.2 miles S. of South Haven light

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description                                   |
|------------|------------------------|-----------------|---|
| 1          | 1                      | 49              | Fine sand 5 trials: small sample              |
| 2          | 2                      | 62              | Medium sand                                   |
| 3          | 3                      | 88              | Silty very fine sand                          |
| 4          | 4                      | 100             | Silty fine-to-medium sand                     |
| 5          | 5                      | 110             | Grayish-brown sandy coarse silt               |
| 6          | 6                      | 119             | Brownish-gray sandy silt                      |
| 7          | 7                      | 131             | Gray silt                                     |
| 8          | 8                      | 139             | Gray sandy very fine silt                     |
| 9          | 9                      | 149             | Gray sandy clayey silt                        |
| 10         | 10                     | 158             | Gray slightly-sandy clayey silt               |
| 11         | 12                     | 174             | Dark-gray slightly-sandy clayey silt          |
| 12         | 14                     | 187             | Dark-gray slightly-sandy clayey silt          |
| 13         | 16                     | 210             | Dark-gray slightly-sandy clayey silt          |
| 14         | 18                     | 232             | Dark-gray slightly-sandy clayey silt          |
| 15         | 20                     | 247             | Dark-gray slightly-sandy clayey silt          |
| 16         | 22?                    | 263             | Dark-gray slightly-sandy clayey silt          |
| 17         | 24?                    | 298             | Dark-gray slightly-sandy clayey silt          |
| 18         | 26?                    | 340             | Dark-gray slightly-sandy clayey silt          |
| 19         | 30                     | 490             | Brownish-gray very-slightly-sandy clayey silt |

Line IV; bearing 105° from South Haven pierhead

| Sample<br>No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description                                |
|---------------|---------------------------|-----------------|--|
| 6             | 1                         | 50              | No sample, 3 trials                        |
| 7             | 2                         | 65              | Medium sand                                |
| 8             | 3                         | 90              | Fine sand                                  |
| 9             | 4                         | 105             | Grayish-brown fine sand and very fine sand |
| 10            | 5                         | 118             | Grayish-brown very fine sand               |
| 11            | 6                         | 132             | Brownish-gray silty very fine sand         |
| 12            | 7                         | 151             | Gray very-fine-sandy silt                  |
| 13            | 8                         | 168             | Gray very-fine-sandy silt                  |
| 14            | 9                         | 178             | Brownish-gray very-fine-sandy silt         |
| 15            | 10                        | 188             | Dark gray slightly-sandy clayey silt       |
| 16            | 12                        | 210             | Dark gray slightly-sandy clayey silt       |
| 17            | 14                        | 222             | Dark gray slightly-sandy clayey silt       |
| 18            | 16                        | 238             | Dark gray slightly-sandy clayey silt       |
| 5             | 18                        | 240             | Dark gray slightly-sandy clayey silt       |
| 4             | 20                        | <b>2</b> 55 .   | Gray slightly-sandy clayey silt            |
| 3             | 22?                       | 273             | Gray slightly-sandy clayey silt            |
| 2             | 24?                       | 318             | Dark gray slightly-sandy clayey silt       |
| 1             | 26?                       | 348             | Dark gray slightly-sandy clayey silt       |
| 19            | 30                        | ş'              | Gray slightly-sandy slightly-clayey silt   |

Line V; bearing 277° from point on E. shore 10 miles N. of South Haven

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|---------------|------------------------|-----------------|---|
| ı             | 1                      | 50              | Fine sand   |
| 2             | 2                      | 75              | Fine sand   |
| 3             | 3                      | 100             | Very fine sand to fine sand   |
| 4             | 4                      | 120             | Silty very fine sand  |
| 5             | 5                      | 140             | Silty very fine sand  |
| 6             | 6                      | 160             | Very-fine-sandy silt  |
| 7             | 7                      | 178             | Very_fine_sandy silt  |
| 8             | 8                      | 192             | Gray very-fine-sandy fine silt  |
| 9             | 9                      | 202             | Buff silty very fine sand   |
| 10            | 10                     | 215             | Grayish buff very-fine-sandy silt   |
| 11            | 12                     | 238             | Grayish buff very-fine-sandy clayey silt  |
| 12            | 15                     | 245             | Grayish buff very-fine-sandy clayey silt  |
| 13            | 16                     | 248             | Grayish buff very-fine-sandy clayey silt  |
| 14            | 17.2                   | 260             | Grayish buff very-fine-sandy clayey silt  |
| 15            | 18                     | 268             | Grayish buff very-fine-sandy clayey silt  |
| 16            | 20                     | 277             | Grayish buff very-fine-sandy clayey silt  |
| 17            | 30                     | 455             | <pre>1/16" gray silt over brownish-gray   very-slightly-sandy clayey silt</pre> |

Line VI; bearing 90° through Saugatuck pierhead light

| Sample<br>No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description   |
|---------------|---------------------------|-----------------|---|
| 15            | 1                         | 50              | Medium-fine sand  |
| 14            | 2                         | 78              | Very fine sand  |
| 13            | 3                         | 90              | Very fine sand  |
| 12            | 4                         | 120             | Very fine sand (with a few coarser sand grains)                                   |
| 11            | 5                         | 143             | Silty very fine sand  |
| 10            | 6                         | 170             | Silty very fine sand  |
| 9             | 7                         | 193             | Grayish-buff clayey very-fine-sandy silt  |
| 8             | 8                         | 217             | Grayish-buff very-fine-sandy clayey silt  |
| 7             | 9                         | 230             | Buff-gray very-fine-sandy clayey silt   |
| 6             | 10                        | 243             | Buff-gray very-fine-sandy clayey silt   |
| 5             | 12                        | 266             | Gray-buff clayey sandy silt   |
| 4             | 14                        | 272             | Gray-buff clayey sandy silt   |
| 3             | 16                        | 285             | Buff-gray sandy clayey silt   |
| 2             | 18                        | 290             | Buff-gray sandy clayey silt   |
| 1             | 20                        | 310             | Buff-gray sandy clayey silt   |
| 17            | 30                        | 475             | <pre>1/16" gray silt over brownish-gray<br/>very-slightly-sandy clayey silt</pre> |
| 16            | 37                        |                 | Gelatinous gritless gray silty clay   |

Line VII; bearing 270° from Holland pierhead light

| Sample<br>No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description  |
|---------------|---------------------------|-----------------|--|
| ı             | 1                         | 52              | Medium-fine sand   |
| 2             | 2                         | 78              | Medium sand  |
| 3             | . 3                       | 109             | Grayish-buff very fine sand  |
| 4             | 4 .                       | 136             | Grayish-buff silty very fine sand  |
| 5             | 5                         | 167             | Buff-gray very-fine-sandy silt   |
| 6             | 6                         | 184             | Buff-gray very-fine-sandy silt   |
| 7             | 7                         | 208             | Gray slightly-very-fine-sandy silt   |
| 8             | 8                         | 223             | Gray slightly-sandy clayey silt  |
| 9             | 9                         | 242             | Gray slightly-sandy clayey silt  |
| 10            | 10                        | 253             | Gray slightly-sandy clayey silt  |
| 11            | 12                        | 263             | Gray slightly-sandy clayey silt  |
| 12            | 14                        | 269             | Gray slightly-sandy clayey silt  |
| 13            | 16                        | 278             | Dark gray slightly-sandy clayey silt with layers of gray-buff clayey silty sand            |
| 14            | 18                        | 282             | Gray-buff clayey silty sand  |
| 15            | 20                        | 298             | Gray-buff clayey silty sand  |
| 16            | , 30                      | 360             | 1/4" brown-gray silt over 1/2" brown-<br>gray sandy silt over red-brown soft<br>sandy clay |

Line VIII; bearing 270° from pierhead, Port Sheldon

| Sample No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description  |
|------------|---------------------------|-----------------|--|
| 1          | 1                         | 48              | Fine sand  |
| 2          | 2                         | 80              | Medium sand  |
| 3          | 3                         | 117             | Sightly-silty very fine sand   |
| 4          | 4                         | 138             | Grayish-buff silty very fine sand  |
| 5          | 5                         | 163             | Gray clayey very_fine_sandy silt   |
| 6          | 6                         | 180             | Gray clayey very-fine-sandy silt   |
| 7          | 7                         | 197             | Gray clayey very-fine-sandy silt   |
| 8          | 8                         | 213             | Gray clayey very-fine-sandy silt   |
| 9          | 9                         | 225             | Gray very-fine-sandy clayey silt   |
| 10         | 10                        | 232             | Gray very-fine-sandy clayey silt   |
| 11         | 12                        | 243             | Buff-gray clayey silty sand  |
| 12         | 14                        | 260             | Buff-gray clayey silty sand  |
| 13         | 16                        | 270?            | Buff-gray clayey silty sand  |
| 14         | 18                        | 283?            | Buff-gray clayey silty sand  |
| 15         | 20                        | 292             | Gray very-fine-sandy clayey silt   |
| 16         | 30                        | 334             | <pre>1/4" brown-gray silt over 3/4"  brown-gray sandy silt over red-  brown soft sandy clay with small  shells</pre> |

Line IX; bearing 90° to E. shore at Grand Haven

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|------------|------------------------|-----------------|---|
| 15         | 1.                     | 54              | Medium sand (clean)   |
| 14         | 2                      | 77              | Fine sand (clean)   |
| 13         | 3                      | 104             | Slightly-silty fine sand, some coarse sand  |
| 12         | 4                      | 136             | Grayish-buff silty very fine sand   |
| 11         | 5                      | 164             | Grayish-buff very-fine-sandy silt, some medium sand   |
| 10         | 6                      | 204             | <pre>Grayish-buff very-fine-sandy silt,   some medium sand</pre>  |
| 9          | 7                      | 240             | Gray-buff clayey silt, very few sand grains   |
| 8          | 8                      | 266             | Dark gray clayey sandy silt over<br>light gray very-sandy silt over<br>rusty-tan very-sandy silty clay  |
| 7          | 9                      | 272             | <pre>1/4" grayish-brown silt over dark   gray sandy silt with black zones,   over light grayish-buff silty sand</pre>   |
| 6          | 10                     | 277             | 1/4" grayish-brown silt over dark gray sandy silt with black zones, over light grayish-buff silty sand  |
| 5          | 12                     | 287             | Brownish-gray clayey silt over brownish-gray very-sandy silt  |
| 4          | 14                     | 312             | Sandy silt; in layers of lighter and darker grays   |
| 3          | 16                     | 330             | Gray clayey very-sandy silt over clayey very-sandy silt with reddish-brown color  |
| 2          | 18                     | 328             | Gray clayey very-sandy silt over red-brown (almost Valders red) very-sandy silty clay   |
| 1          | 20                     | 335             | Gray sandy silt over reddish-brown very-sandy silt over "clay" (dark brown 1/16" thick) over "clay" (rusty brown 1/8" thick) over reddish-brown slightly-sandy silty clay |
| 16         | 25                     | 345             | 1/2" brown-gray sandy silt over red-<br>brown soft sandy clay   |

Line X; bearing 270° from Muskegon pierhead

| Sample<br>No. | Miles<br>from<br>Pierhead | Depth<br>(feet) | Description   |
|---------------|---------------------------|-----------------|---|
| 1             | 1                         | 55              | Medium-fine sand (clean)  |
| 2             | 2                         | 80              | Medium sand   |
| 3             | 3                         | 98              | Medium-coarse sand, very slightly silty   |
| 4             | 4                         | 118             | Sandy buff silty very-fine-to-fine sand   |
| 5             | 5                         | 127             | Buff silty very-fine-to-fine sand   |
| 6             | 6                         | 150             | <pre>1/2" brownish gray silty fine sand   over buff very-silty very-fine-to-   fine sand</pre>                    |
| 7             | 7                         | 180             | <pre>1/2" brownish gray silty fine sand   over buff very-silty very-fine-to-   fine sand</pre>                    |
| 8             | 8                         | 282             | <pre>1/2" brownish gray silty fine sand   over buff very-silty very-fine-to-   fine sand</pre>                    |
| 9             | 9                         | 342             | 1/2" buff silty fine sand over 1-1/2" light gray silty fine sand over dark gray slightly-sandy clayey silt        |
| 10            | 10                        | 352             | 1/8" buff clayey silt over dark gray clayey silt  |
| 11            | 12                        | 355             | <pre>l/l6" buff clayey silt over 2" light   gray slightly-sandy clayey silt   over dark gray clayey silt</pre>    |
| 12            | 14                        | 362             | Clayey very-slightly-sandy silt, in thin zones: gray, rusty, brownish-black, rusty, gray, dark gray-from top down |
| 13            | 16                        | 375             | Clayey very-slightly-sandy silt, in thin zones: gray-brown, red-brown, brownish-black, rusty, gray, from top down |
| 14            | 18                        | 390             | <pre>1/4" buff clayey very-slightly-sandy   silt over dark gray clayey very-   slightly-sandy silt</pre>          |
| 15            | 20                        | 387             | Clayey very-slightly-sandy silt:<br>gray (1/2") over rusty (1/4") over<br>medium gray                             |
| 16            | 25                        |                 | Gray gritless silt over red-brown gritless silt   |

Line XI; bearing  $90^{\circ}$  from point on W. shore about 9.5 miles N. of Milwaukee light

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 1          | 1                      | 63              | Slightly-clayey medium-to-coarse sand  |
| 2          | 2                      | 128             | Slightly-clayey medium-to-fine sand  |
| 3          | 3                      | 168             | Slightly-clayey medium-to-fine sand  |
| 4          | 4                      | 194             | Slightly-clayey fine-to-very-fine sand   |
| 5          | 5                      | 232             | Slightly-clayey fine-to-very-fine sand   |
| 6          | 6                      | 248             | Buff-gray clayey sandy silt  |
| 7          | 7                      | 262             | Buff-gray clayey sandy silt  |
| 8          | 8                      | 274             | Buff-gray clayey sandy silt  |
| 9          | 9                      | 278             | Buff-gray clayey sandy silt  |
| 10         | 10                     | 286             | 2" buff-gray clayey sandy silt over rusty-brown clayey silty sand  |
| 11         | 12                     | 294             | <pre>1-1/2" red-brown clayey sandy silt   over red-brown stiff clayey sandy   silt over clayey silt</pre>                            |
| 12         | 14                     | 307             | <pre>1/2" gray clayey sandy silt over<br/>1-1/2" brown-buff silty fine sand<br/>over gray silty clay</pre>                           |
| 13         | 16                     | 268             | 3/4" gray silty fine sand over reddish-buff clayey silty fine sand   |
| 14         | 18                     | 265             | <pre>1/2" gray silty fine sand over<br/>reddish-buff clayey silty fine-<br/>medium-coarse sand</pre>                                 |
| 15         | 20                     | 233             | <pre>1/2" gray silty fine sand over clayey   silty fine-medium-coarse sand with   pebble 8 cm long (Lower layer till?)</pre>         |
| 16         | 25                     |                 | Limestone cobble, 13 cm x 8 cm; chert layer 1 cm thick on one face; black (powdery when dry) discoloration on surface of three faces |

Line XII; bearing 90° from N. Point Light (about 2.8 miles N. of Milwaukee)

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 1          | 1.1                    | 55              | Coarse sand over stiff red clay  |
| 2          | 2.0                    | 75              | Gravel, up to 3 cm, over stiff sandy red clay  |
| 3          | 3.1                    | 105             | Medium sand, with $1/2$ " layer cinders at $1-1/2$ " depth   |
| 4          | 4.0                    | 120             | Medium sand, both buff and buff-gray; small pebbles (sample slumped; which material was on top is not known)   |
| 5          | 5.0                    | 145             | <pre>l" grayish buff silty medium-fine sand<br/>over brownish-buff silty fine sand</pre>   |
| 6          | 5.6                    | 163             | <pre>l" grayish-buff silty medium-fine sand<br/>over brownish-buff silty fine sand</pre>   |
| 7          | 6.4                    | 180             | <pre>l" grayish-buff silty medium-fine sand<br/>over brownish-buff silty fine sand</pre>   |
| 8          | "8"                    | 214             | Brownish-buff clayey fine sand   |
| 9          | 9                      | 230             | Brownish-buff clayey fine sand with one pebble 1 cm in diameter  |
| 10         | 10                     | 242             | <pre>1/2" rusty-brown clayey silty medium-<br/>fine sand over brownish-buff clayey<br/>fine sand</pre>   |
| 10A        | "11"                   | 254             | <pre>1/2" rusty-brown clayey silty medium-<br/>fine sand over brownish-buff clayey<br/>fine sand</pre>   |
| 11         | 12                     | 264             | Brownish-buff sandy silty clay   |
| 12         | 14                     | 284             | Reddish-buff sandy clayey silt with shell fragments  |
| 13         | 16                     | 297             | Reddish-buff sandy clayey silt with shell fragments  |
| 14         | 18                     | 308             | Slightly-sandy silty clay, gray with rusty brown layer   |
| 15         | (19)                   | 308             | Gray slightly-sandy silty clay   |
| 16         | 25                     |                 | Sand (fine, medium, coarse), chert cobble 6 cm x 6 cm x 1cm; limestone cobble 11 x 9 x 6 cm; both cobbles with black (powdery when dry) surface discoloration on 3 faces |

Line XIII; bearing 90° from W. shore, 4.8 miles S. of Milwaukee

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|---------------|------------------------|-----------------|--|
| 15            | 1                      | 52              | Gravel: including cobbles up to 10 cm diameter. Rocks mainly carbonates                          |
| 14            | 2                      | 67              | Medium-to-coarse sand; gravel  |
| 13            | 3                      | 73              | Reddish-buff stiff sandy clay  |
| 12            | 4                      | 78              | Reddish-buff stiff sandy clay  |
| 11            | 5                      | 92              | Reddish-buff stiff sandy clay  |
| 10            | 6                      | 107             | Reddish-buff stiff sandy clay  |
| 9             | 7                      | 120             | Hard bottom. No sample, 4 trials   |
| 8             | 8                      | 142             | Slightly-silty medium sand, with few pebbles   |
| 7             | 9                      | 163             | Slightly-silty fine sand, with few granules  |
| 6             | 10                     | 182             | <pre>Grayish-buff slightly-silty medium   sand</pre>   |
| 5             | 12                     | 198             | Grayish-buff slightly-silty medium sand  |
| 4             | 14                     | 256             | Thin cover of medium sand over reddish-<br>grayish-buff sandy clay                               |
| 3             | 16                     | 292             | Thin cover of medium sand over reddish-<br>grayish-buff sandy clay                               |
| 2             | 18                     | 308             | Thin cover of medium sand over reddish-<br>grayish-buff sandy clay                               |
| 1             | 20                     | 313             | Thin cover of layered medium sand over reddish-grayish-buff sandy clay. A few shells in the clay |
| 16            | 25                     |                 | <pre>1/2" gray slightly sandy silt over<br/>gritless reddish-grayish-buff clay</pre>             |

Line XIV; bearing 90° from W. shore stack, 12.2 miles S. of Milwaukee

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|---------------|------------------------|-----------------|--|
| 1             | 1                      | 47              | Gray-buff clayey poorly-sorted coarse sand   |
| 2             | 2                      | 58              | Silty fine sand  |
| 3             | 3                      | 57              | Coarse sand over stiff gray clay   |
| 4             | 4                      | 62              | Gravel (3 pebbles, 5 to 7 cm long)   |
| 5             | 5                      | 77              | Medium-coarse sand   |
| 6             | 6                      | 78              | Medium-coarse sand over stiff grayish-red clay   |
| 7             | 7                      | 88              | Gravel, mainly 1 to 2 cm and 1 pebble 9 cm, over stiff grayish-red clay  |
| 8             | 8                      | 102             | Gray watery clay ca. 1 mm thick, over stiff grayish-red clay with a few small pebbles                          |
| 9             | 9                      | 122             | Medium sand  |
| 10            | 10                     | 143             | Silty medium sand, few small pebbles   |
| 11            | 12 (11) <sup>2</sup>   | 173             | Clayey silty fine sand over stiff grayish-red clay   |
| 12            | 14 (13) <sup>2</sup>   | 247             | Clayey silty fine sand over stiff grayish-red clay   |
| 13            | 16 (15) <sup>2</sup>   | 293             | Grayish-brown sandy clay with zones of clayey medium sand with black coatings                                  |
| 14            | 18 (17) <sup>2</sup>   | 332             | Grayish-brown sandy clay with zones of clayey medium sand with black coatings plus shells in zones and in clay |
| 15            | 20 (19) <sup>2</sup>   | 334             | Grayish-brown sandy clay with zones of clayey medium sand with black coatings (with few shells)                |
| 15            | 25                     |                 | 1/2" gray slightly-sandy silt over brownish-gray gritless clay   |

<sup>2 =</sup> by fathometer time marks

Line XV; bearing 90° from W. shore, Racine

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|---------------|------------------------|-----------------|---|
| 15            | 1                      | 40              | Gray fine-sandy silt  |
| 14            | 2                      | 50              | Gray clayey silty poorly-sorted coarse sand                                   |
| 13            | 3                      | 58              | 1/8" of clean coarse sand and fine gravel over stiff grayish-red clay         |
| 12            | 4                      | 72              | Gravel (pieces up to 3.5 cm)  |
| 11            | 5                      | 75              | Clean medium sand, with few pebbles up to 2.8 cm                              |
| 10            | 6                      | 87              | Clean medium sand, with few pebbles up to 2.2 cm                              |
| 9             | 7                      | 100             | Clean medium sand, with very few pebbles up to 1.2 cm                         |
| 8             | 8                      | 146             | Gray-buff clayey silty fine sand with a few granules                          |
| 7             | 9                      | 167             | Gray-buff clayey silty fine sand  |
| 6             | 10                     | 192             | Gray-buff clayey silty fine sand  |
| 5             | 12                     | 235             | Gray-buff clayey silty fine sand  |
| 4             | 14                     | 265             | Gray-brown very-clayey silty fine sand  |
| 3             | 16                     | 292             | Grayish-brown sandy clay with zones of clayey medium sand with black coatings |
| 2             | 18                     | 323             | Grayish-brown sandy clay with zones of clayey medium sand with black coatings |
| . 1           | 20                     | 352             | Gray soft clay  |
| 16            | 25                     |                 | Gray gritless clay  |

Line XVI; bearing 90° from shore at Kenosha, Wisconsin

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 1          | 1                      | 38              | Medium-fine sand (clean)   |
| 2          | 2                      | 55              | Medium-fine sand, few pebbles to 1 cm (clean)  |
| 3          | 3                      | 55              | Pebble (1) 2 cm diameter   |
| 4          | 4                      | 60              | Medium-coarse sand (clean)   |
| 5          | 5                      | 100             | Grayish-buff silty very fine sand, small shells  |
| 6          | 6.1                    | 133             | Grayish-buff silty medium-fine sand  |
| 7          | 7                      | 150             | Grayish-buff silty fine sand   |
| 8          | 8                      | 165             | Grayish-buff silty fine sand, few granules   |
| 9          | 9.1                    | 185             | Medium-fine sand, few small pebbles and cinders (fairly clean)   |
| 10         | 10                     | 210             | Slightly-silty medium-fine sand, few granules and small pebbles (2nd trial, no sample)   |
| 11         | 12                     | 247             | <pre>1-1/8" brownish-buff clayey silty   medium-fine sand over tough brownish   buff clayey silty medium-fine sand</pre>                               |
| 12         | 14.1                   | 270             | <pre>1-1/8" brownish-buff clayey silty   medium-fine sand over tough brownish   buff clayey silty medium-fine sand</pre>                               |
| 13         | 16.1                   | 280             | <pre>1/2" brownish-buff clayey silty medium fine sand over brownish-red slightly sandy clay, with shells; few small zones of black coated grains</pre> |
| 14         | 18                     | 330             | Soft, dark-gray sandy clayey silt over grayish-buff clayey silty medium-fine sand over firm, brownish red sandy clay                                   |
| 15         | 20                     | 347             | Soft, dark-gray sandy clayey silt over grayish-buff clayey silty medium-fine sand over firm brownish-red sandy clay                                    |

Line XVII; bearing 90° from W. shore near Winthrop Harbor

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|------------|------------------------|-----------------|---|
| 13         | 1.5                    | 46              | Medium-coarse sand (clean)  |
| 12         | 2.5                    | 72              | Grayish-buff silty very fine sand   |
| 11         | 3.8                    | 108             | Grayish-buff silty medium-fine sand with few pebbles  |
| 10         | 5.0                    | 143             | <pre>Grayish-buff silty medium-fine sand   over rusty-brown silty medium-fine   sand</pre>                  |
| 9          | 6.0                    | 154             | Grayish-buff silty medium-fine sand, few small pebbles  |
| 8          | 7.5                    | 172             | Grayish-buff silty medium-fine sand, few small pebbles  |
| 7          | 8.2                    | 190             | <pre>1/2" gray clayey silty medium-fine<br/>sand over brownish-buff clayey<br/>silty medium-fine sand</pre> |
| 6          | 10.0                   | 228             | <pre>1/2" gray clayey silty medium-fine<br/>sand over brownish-buff clayey<br/>silty medium-fine sand</pre> |
| 5          | 12.0                   | 260             | 3/4" gray clayey silty fine sand over brownish-buff clayey silty medium-fine sand                           |
| 4          | 14.0                   | 284             | <pre>1/4" gray clayey fine-sandy silt   over brownish-red clayey silty   fine sand</pre>                    |
| 3          | 16.2                   | 308             | <pre>1/4" gray clayey fine-sandy silt   over brownish-red clayey silty   fine sand</pre>                    |
| 2          | 18.5                   | 336             | 3/4" gray sandy silty clay over reddish-brown sandy silty clay  |
| 1          | 21.0                   | 358             | Gray sandy silty clay   |

Line XVIII; bearing 90° from W. shore at Waukegan

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 1          | 1                      | 38              | Very fine sand   |
| 2          | 2                      | 58              | Fine sand  |
| 3          | 3                      | 74              | Medium-fine sand   |
| 4          | 4                      | 90              | Grayish-buff slightly silty medium-<br>fine sand, few small shells   |
| 5          | 5                      | 108             | Grayish-buff silty medium sand   |
| 6          | 6                      | 125             | <pre>Grayish-buff silty medium sand   (l cinder)</pre>   |
| 7          | 7                      | 145             | Grayish-buff silty medium-coarse sand, few granules  |
| 8          | 8                      | 158             | Grayish-buff silty medium sand, few granules   |
| 9          | 9                      | 169             | Grayish-buff silty medium sand   |
| 10         | 10                     | 183             | Grayish-buff silty medium-fine sand  |
| 11         | 12                     | 225             | Reddish-brown clayey silty sand  |
| 12         | 14                     | 250             | 3/4" gray clayey silty sand over reddish-brown clayey silty sand   |
| 13         | 16                     | 265             | 3/4" gray clayey silty sand over reddish-brown clayey silty sand   |
| 14         | 18                     | 280             | 3/4" gray clayey silty sand over reddish-brown clayey silty sand   |
| 15         | 20                     | 303             | 3/4" gray clayey silty sand over reddish-brown clayey silty sand   |
| 16         | 25                     | 340             | Soft pink-brown clay with 1 cm gray patches  |
| 18         | 30                     | 420             | 1/8" brownish-gray silt over 1" black gritless silt over 3/4" brownish-gray soft clay over 3/4" gray soft clay over brownish-gray soft clay - all clay layers slightly sandy |
| 17         | 35                     | 420             | 1/4" gray silt over 1-1/2" sandy gray clay over softer red-brown sandy clay  |

Line XIX; bearing 90° from W. shore at Lake Forest, Illinois

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 14         | . 1                    | 35              | Gravel; up to 10 cm diameter   |
| 13         | 2                      | 40              | Gravel and coarse sand, few shells   |
| 12         | 3                      | 47              | Gravel and coarse sand, few shells, over compact gray sandy silty clay                                   |
| 11         | 4.1                    | 55              | Gravel (up to 12 cm) and coarse sand   |
| 10         | 5                      | 68              | Grayish-buff silty coarse sand, few pebbles, up to 8 cm diameter   |
| 9          | 6                      | 77              | Coarse sand, few pebbles up to 4 cm diameter   |
| 8          | 7.1                    | 93              | Gravel and very coarse sand; gravel up to 10 cm diameter   |
| 7          | 8.2                    | 103             | Gravel, up to 5 cm diameter  |
| 6          | 9                      | 116             | Grayish-buff silty fine sand   |
| 5          | 11.5                   | 120             | One cobble, 9 cm diameter, with black coating (organic?)   |
| 4          | 14                     | 154             | Grayish-buff silty fine-to-coarse sand, few small pebbles (to 1 cm)                                      |
| 3          | 16                     | 178             | Grayish-buff silty fine-to-coarse sand, few pebbles (to 5 cm)  |
| 2          | 18                     | 214             | Grayish-brown clayey silty sand over brownish-red silty sandy clay                                       |
| 1          | 20                     | 245             | Grayish-brown clayey silty sand  |
| 15         | 25                     |                 | 1/4" gray layer at top over soft brown sandy clay  |
| 16         | 30                     | 335             | <pre>1/8" brownish-gray silt over 2"   reddish-brown soft sandy clay over   firmer gray sandy clay</pre> |
| 17         | 35                     | 350             | Thin covering brownish-gray silt over soft very-slightly-sandy pink-brown soft clay                      |

Line XX; bearing 90° from W. shore near Glencoe, Illinois, to buoy, 8 miles then 85° from buoy

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Descriptions  |
|------------|------------------------|-----------------|---|
| 1          | 2                      | 40              | Gravel  |
| 2          | 3                      | 47              | Gravel  |
| 3          | 4                      | 50              | l granule in 3 trials   |
| 4          | 5                      | 55              | Gravel  |
| 5          | 6                      | 58              | l pebble in 2 trials  |
| 6          | 7                      | 66              | Gravel (including angular block 20 cm long, limestone and chert)                                      |
| 7 <b>*</b> | 8                      | 45              | Few grains coarse sand and gravel   |
| 8          | 9                      | 104             | lst trial: few sand grains<br>2nd trial: coarse sand, poorly sorted                                   |
| 9          | 10                     | 106             | Coarse sand and fine gravel   |
| 10         | 12                     | 140             | Grayish-buff silty fine sand  |
| 11         | 14                     | 163             | Grayish-buff slightly silty medium sand   |
| 12         | 16                     | 180             | Grayish-buff silty medium-fine sand, very few small pebbles   |
| 13         | 18                     | 213             | Reddish-brown clayey silty sand, few small pebbles  |
| 14         | 20                     | 265             | l" brownish-gray sandy silty clay<br>over sandy silty clay mottled<br>reddish-brown and brownish-gray |
| 15         | 25                     |                 | 1/4" sandy gray silt over reddish-<br>brown soft slightly-sandy clay                                  |

<sup>\*100</sup> yds. N. of buoy

Line XXI; bearing 85° from W. shore at Wilmette

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 14         | 2                      | 38              | No sample (rock bottom?)   |
| 13         | 3                      | 43              | 1 cobble, 25 cm long   |
| 12         | 4                      | 48              | Gravel   |
| 11         | 5                      | 66              | <pre>1/4" dark gray sandy silty clay over<br/>medium sand and fine gravel</pre>                                    |
| 10         | 6                      | 48              | Medium-coarse sand and fine gravel   |
| 9          | 7                      | 78              | Coarse sand and fine gravel  |
| 8          | 8                      | 90              | Coarse sand and gravel (1 pebble, 5 cm long)   |
| 7          | 9                      | 106             | Gravel, and rusty-oxide crust on till-like material  |
| 6          | 10                     | 118             | Medium-coarse sand, gravel   |
| 5          | 12                     | 137             | Grayish-buff slightly silty fine-<br>medium sand   |
| 4          | 14                     | 162             | Grayish-buff slightly silty fine-<br>medium sand   |
| 3          | 16                     | 200             | 3/4" gray silty fine sand over grayish-buff silty fine sand  |
| 2          | 18                     | 217             | <pre>l-1/2" brownish-gray sandy silty   clay over sandy silty clay mottled   reddish-brown and brownish-gray</pre> |
| 1          | 20                     | 228             | <pre>1-1/2" brownish-gray sandy silty clay   over sandy silty clay mottled   reddish-brown and brownish-gray</pre> |

Line XXII; bearing 79° from Wilson Avenue Crib, off Montrose Harbor

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|---------------|------------------------|-----------------|--|
| 1*            | 2                      | 42              | Sand, gravel, few shells   |
| 2             | 3.1                    | 41              | Medium-fine sand, few granules, very few shells                                  |
| 3             | 4                      | 48              | <pre>1-1/4" medium-coarse sand and fine<br/>gravel over gray clay</pre>          |
| 4             | 5                      |                 | l-1/4" medium-coarse sand and fine gravel over gray clay                         |
| 5             | 6                      |                 | Gravel, up to 7 cm diameter, small amount sand                                   |
| 6             | 7                      | 75              | Gravel, up to 5 cm diameter, small amount sand, very few shells                  |
| 7             | 8                      | 81              | Medium-coarse sand and fine gravel   |
| 8             | 9                      | 86              | Medium-fine sand, few granules   |
| 9             | 10                     | 100             | Fine gravel  |
| 10            | 12                     | 120             | Very coarse sand   |
| 11            | 14                     | 135             | Grayish-buff slightly-silty medium-<br>fine sand                                 |
| 12            | 16                     | 151             | Grayish-buff slightly-silty fine sand, few granules                              |
| 13            | 18                     | 166             | Grayish-buff slightly-silty fine sand, few granules                              |
| 14            | 20                     | 184             | 3/4" brownish-gray silty fine sand over slightly-sandy red clay, with few shells |
| B-1           | 18.5                   | 159             | Grayish-buff slightly-silty fine sand  |
| B-2           | 17.0                   | 135             | Gravel   |

<sup>\*</sup>Wilson Avenue Crib

Line XXIII; bearing 75° from N.E. corner outer breakwater, Chicago Harbor

| Sample No. | Miles<br>from<br>Breakwater | Depth<br>(feet) | Description  |
|------------|-----------------------------|-----------------|--|
| 1          | 1                           | 38              |  |
|            |                             | _               | Coarse sand, gravel                                |
| 2          | 2                           | 45              | Medium-fine sand                                   |
| 3          | 3                           | 46              | Gravel, over gray clay                             |
| 4          | 4                           | 47              | Medium-fine sand                                   |
| 5          | 5                           | 58              | Very coarse sand, gravel, pieces of ceramic tile   |
| 6          | 6                           | 67              | Gravel, cinders, rusty nails; over stiff gray clay |
| 7          | 7                           | 67              | Medium sand with few cinders                       |
| 8          | 8                           | 67              | Sand and pebbles over stiff gray clay              |
| 9          | 9                           | 80              | Medium-coarse sand                                 |
| 10         | 10                          | 88              | Gravel over soft grayish-brown clay                |
| 11         | 12                          | 109             | Medium-fine sand                                   |
| 12         | 14                          | 126             | Medium-fine sand                                   |
| 13         | 16                          | 139             | Coarse sand and gravel                             |
| 14         | 18                          | 152             | Coarse sand and gravel                             |
| 15         | 20                          | 166             | Brown slightly-silty fine sand                     |

Line XXIV; from offshore, 255°, to shore at Oakland Shoal

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description                           |
|------------|------------------------|-----------------|---------------------------------------|
| 15         | 1                      | 31              | Fine sand over gray clayey fine sand  |
| 14         | 2                      | 35              | Medium sand                           |
| 13         | 3                      | 39              | Fine sand over stiff gray clay        |
| 12         | 4                      | 45              | Silty coarse sand and granules        |
| 11         | 5                      | 50              | Gravel over gray stiff sandy clay     |
| 10         | 6                      | 45              | Medium-fine sand over stiff gray clay |
| 9          | 7                      | 58              | Medium-fine sand                      |
| 8          | 8                      | 60              | Coarse sand, few pebbles              |
| 7          | 9                      | 57              | Medium-fine sand                      |
| 6          | 10                     | 75              | Gravel, over gray stiff sandy clay    |
| 5          | 12                     | 87              | Well-sorted gravel, mainly fine       |
| 4          | 14                     | 97              | Medium sand                           |
| 3          | 16                     | 110             | Gravel, over gray stiff sandy clay    |
| 2          | 18                     | 120             | Medium-coarse sand                    |
| 1          | 20                     | 128             | Gravel                                |
|            |                        |                 |                                       |

Line XXV; bearing 70° from Calumet Harbor

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|---------------|------------------------|-----------------|---|
| 1             | 1                      | 33              | Gravel over gray stiff sandy clay (Foul odor.)      |
| 2             | 2                      | 40              | Medium sand   |
| 3             | 3                      | 44              | Gravel over gray stiff sandy gravelly clay (till?)  |
| 4             | 4                      | 43              | Coarse sand, few pebbles                            |
| 5             | 5                      | 45              | Medium-coarse sand, few granules and pebbles        |
| 6             | 6                      | 47              | Gravel over gray stiff sandy gravelly clay (till?)  |
| 7             | 7                      | 46              | Medium-fine sand                                    |
| 8             | 8                      | 43              | Medium-fine sand                                    |
| 9             | 9                      | 67              | Slightly-silty fine sand                            |
| 10            | 10                     | 72              | Gravel  |
| 11            | 12                     | 66              | Gravel, over stiff gray clay                        |
| 12            | 14                     | 86              | Gravel and coarse sand over stiff gray clay         |
| 13            | 16                     | 100             | Gravel, over gray stiff sandy gravelly clay (till?) |
| 14            | 18                     | 98              | Grayish-brown slightly-silty fine sand              |
| 15            | 20                     | 107             | Grayish-brown slightly-silty fine sand              |

Line XXVI; from offshore, 240°, to Indiana Harbor

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 13         | 1                      | 35              | Medium-fine sand, few small pebbles                            |
| 12         | 2                      | 35              | Gravel   |
| 11         | . 3                    | 30              | Medium-coarse sand, few granules                               |
| 10         | 4                      | 38              | Medium-fine sand   |
| 9          | 5                      | 40              | Fine sand  |
| 8          | 6                      | 56              | Fine sand with some organic matter, cinders, wood. Odor of oil |
| 7          | 7                      | 56              | Mottled gray and brown silty fine sand. Odor of oil            |
| 6          | 8                      | 66              | Mottled gray and brown silty fine sand. Odor of oil            |
| 5          | 9                      | 65              | Medium-fine sand   |
| 4          | 10                     | 70              | Gravel over gray stiff sandy clay                              |
| 3          | 12                     | 67              | Fine sand  |
| 2          | 14                     | 91              | Gray soft clayey sand over stiff gray clay                     |
| 1          | 16                     | 90              | Medium sand  |

Line XXVII; bearing 0° (N) from Gary, Indiana

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|------------|------------------------|-----------------|---|
| 1          | 1                      | 47              | Fine sand, with very coarse sand-<br>size fragments of Antrim Shale           |
| 2          | 2                      | 58              | Silty very fine sand  |
| 3          | 3                      | 53              | Fine sand, with coarse sand-size fragments of Antrim Shale                    |
| 4          | 4                      | 53              | Fine sand, with coarse sand-size fragments of Antrim Shale                    |
| 5          | 5                      | 48              | Coarse sand   |
| .6         | 6                      | 56              | Coarse sand. Odor of oil  |
| 7          | 7                      | 58              | Dark gray silty very fine sand with some vegetable matter. Strong odor of oil |
| 8          | 8                      | 52              | Medium sand, with few coarse sand-<br>size fragments of Antrim Shale          |
| 9          | 9                      | 61              | Medium-fine sand with few fragments of Antrim Shale                           |
| 10         | 10                     | 66              | Fine gravel, mainly well-sorted. (Median diameter about 3 mm)                 |

Line XXVIII; bearing 0° (N) from Burns Ditch

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description   |
|---------------|------------------------|-----------------|---|
| 1             | 1                      | 38              | Medium sand   |
| 2             | 2                      | 45              | Fine sand   |
| 3             | 3                      | 46              | Gravel, over gray stiff clay  |
| 4             | 4                      | 47              | Fine sand   |
| 5             | 5                      | 58              | Coarse sand - fine gravel over gray silty very fine sand. Odor of oil |
| 6             | 6                      | 67              | Gray slightly-silty fine sand   |
| 7             | 7                      | 67              | Medium-coarse sand, over stiff gray clay                              |
| 8             | 8                      | 67              | Medium-coarse sand  |
| 9             | 9                      | 80              | Medium-coarse sand, few pebbles, over soft gray clay                  |
| 10            | 10                     | 88              | Silty medium-fine sand over stiff gray clay                           |
| 11            | 12                     | 109             | Gravel and coarse sand  |
| 12            | 14                     | 126             | Gravel  |
| 13            | 16                     | 139             | Fine sand, with few granules, over gray stiff sandy clay              |
| 14            | 18                     | 152             | Silty very fine sand, with few small pebbles                          |
| 15            | 20                     | 166             | Slightly-silty medium-coarse sand, with few granules                  |

Line XXIX from offshore, 150°, to Michigan City, Indiana

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 15         | 1                      | 57              | Coarse sand  |
| 14         | 2                      | 58              | Medium sand  |
| 13         | 3                      | 60              | Medium-fine sand, over soft gray clay  |
| 12         | 4                      | 65              | Fine sand  |
| 11         | 5                      | 77              | Gray silty very fine sand  |
| 10         | 6                      | 80              | Gray silty very fine sand  |
| 9          | 7                      | 90              | Grayish brown silty medium-fine sand   |
| 8          | 8                      | 104             | Grayish brown silty medium-fine sand   |
| 7          | 9                      | 113             | Grayish brown silty medium-fine sand   |
| 6          | 10                     | 125             | Grayish brown silty medium-fine sand   |
| 5          | 12                     | 140             | Grayish brown silty medium-fine sand   |
| 4          | 14                     | 155             | Grayish brown silty medium-fine sand   |
| 3          | 16                     | 168             | Grayish brown silty medium-fine sand   |
| 2          | 18                     | 183             | Gray-brown soft clayey silty fine sand over brownish-buff firm clayey silty fine sand      |
| 1          | 20                     | 190             | Gray-brown soft clayey silty fine sand over brownish-buff firm clayey silty fine sand      |
| 16         | 31-1/2                 |                 | <pre>1/2" gray sandy silt over 1-1/2" brown-buff sandy silt over sandy soft red clay</pre> |

Line XXX; bearing 320° from shore at New Buffalo, Michigan

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|---------------|------------------------|-----------------|--|
| 1             | l                      | 47              | Medium-fine sand   |
| 2             | 2                      | 55              | Medium-fine sand, few granules                             |
| 3             | 3                      | 66              | Medium-fine sand, over dark gray clayey sand               |
| 4             | 4                      | 66              | Medium sand  |
| 5             | 5                      | 83              | Brownish-gray silty fine sand                              |
| 6             | 6                      | 95              | Brownish-gray silty very fine sand                         |
| 7             | 7                      | 107             | Brownish-gray silty very fine sand, few medium sand grains |
| 8             | 8                      | 121             | Brownish-gray silty very fine sand, few medium sand grains |
| 9             | 9                      | 136             | Gray very-fine-sandy silt                                  |
| 10            | 10                     | 149             | Gray very-fine-sandy silt                                  |
| 11            | 12                     | 175             | Gray very-fine-sandy silt                                  |
| 12            | 14                     | 197             | Gray very-fine-sandy clayey silt                           |
| 13            | 16                     | 218             | Gray sandy silty clay                                      |
| 14            | 18                     | 235             | Gray sandy silty clay                                      |
| 15            | 20                     | 244             | Gray sandy silty clay                                      |

Line XXXI from offshore, 135°, to shore near Sawyer, Mich.

| Sample<br>No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|---------------|------------------------|-----------------|--|
| 15            | 1                      | 54              | Medium sand over light brownish-gray silty medium-fine sand  |
| 14            | 2                      | 57              | Medium-fine sand   |
| 13            | 3                      | 67              | Fine sand over light brownish-gray silty fine sand   |
| 12            | 4                      | 76              | Medium sand  |
| 11            | 5                      | 87              | Brown medium-fine sand over brownish-<br>gray silty medium-fine sand   |
| 10            | 6                      | 97              | Grayish-brown silty very fine sand   |
| . 9           | 7                      | 115             | Brownish-gray (brown at surface) very fine-sandy silt  |
| 8             | 8                      | 140             | Gray very-fine-sandy silt  |
| 7             | 9                      | 157             | Brownish-gray slightly-sandy clayey silt   |
| 6             | 10                     | 173             | Brownish-gray slightly-sandy clayey silt   |
| 5             | 12                     | 195             | Brownish-gray slightly-sandy silty clay  |
| . 4           | 14                     | 222             | Brownish-gray slightly-sandy A silty clay with increasing Clay percentage  |
| 3.            | 16                     | 249             | Brownish-gray slightly-sandy silty clay with increasing clay percentage  Brownish-gray slightly-sandy silty clay with increasing clay percentage |
| 2             | 18                     | 267             | Brownish-gray slightly-sandy silty clay with increasing clay percentage  |
| 1             | 20                     | 280             | Brownish-gray slightly-sandy silty clay with smaller percentage of grayish-brown clay  |
| 16            | 32 <del>1</del>        |                 | 1/2" gray sandy silt over soft gritless reddish-tan clay   |

Line XXXII; bearing 300° from shore near Grand Marais Lakes

| Sample No. | Miles<br>from<br>Shore | Depth<br>(feet) | Description  |
|------------|------------------------|-----------------|--|
| 1          | 1                      | 45              | Medium-coarse sand   |
| 2          | 2                      | 65              | Medium-coarse sand   |
| 3          | 3                      | 77              | Medium-fine sand over brownish-gray silty fine sand          |
| 4          | 4                      | 85              | Grayish-brown silty very fine sand                           |
| 5          | 5                      | 100             | Brownish-gray very-fine-sandy silt                           |
| 6          | 6                      | 124             | Brownish-gray very-fine-sandy silt                           |
| 7          | 7                      | 153             | Gray very_fine_sandy clayey silt                             |
| 8          | 8                      | 178             | Gray clayey silt   |
| 9          | 9                      | 198             | Gray silty clay  |
| 10         | 10                     | 215             | Gray silty clay  |
| 11         | 12                     | 240             | Brownish-gray silty clay                                     |
| 12         | 14                     | 268             | Brownish-gray silty clay                                     |
| 13         | 16                     | 298             | Grayish-brown sandy silty clay over brownish-gray silty clay |
| 14         | 18                     | 312             | Grayish-brown sandy silty clay over brownish-gray silty clay |
| 15         | 20                     | 327             | Grayish-brown sandy silty clay over brownish-gray silty clay |

### Reference Stations

| Ref.              |   |                 |   |
|-------------------|---|-----------------|---|
| Station           |   | Depth           |   |
| No.               | Location  | (feet)          | Description   |
| I                 | 5.7 miles off-<br>shore. 3.0<br>miles, 117° from<br>Four Mile Crib,<br>Chicago                | 48              | Medium sand, few granules (clean)   |
| II                | 19.3 miles off-<br>shore. 17.1<br>miles, 55° from<br>Four Mile Crib,<br>Chicago               | 173             | 3/4" buff-gray slightly- silty fine-to-very-fine sand over 1-1/2" buff-gray silty fine-very-fine sand over brownish-buff clayey silty fine-very-fine sand with small pebbles. (all layers contain a few small shells) |
| Mid-way<br>II and | between<br>1 III  |                 | 1/4"-1/2" gritless gray<br>silt over buff sandy clay  |
| III               | 30 miles off-<br>shore. 29.5 miles<br>292° from Benton<br>Harbor pierhead<br>(D. R. position) | (340 <u>+</u> ) | Red clay. (Core sample 90 cm long; viewed through plastic liner, appears fine-grained and uniform for entire length)  |
| Mid-way<br>III ar | between<br>nd IV  |                 | 1/4" gray sandy silt over 1/8" buff silty fine sand over soft gray clay   |
| IV                | 34 miles off-<br>shore. 34 miles,<br>292° from South<br>Haven pierhead<br>(D. R. position)    | (470+)          | Gray clay. (Core sample 90 cm long; viewed through plastic liner, shows color bands of light gray and black, entire length)   |

| Sample         | Toodis                             | Depth  | Dogoniuti  |
|----------------|------------------------------------|--------|--|
| No.            | Location Chicago Outer Light       | (feet) | Description  |
| 63-1           | Chicago Outer Light 42°10', 87°20' | 237    | 1/4" gray slightly-sandy silty clay over red clay                                      |
| 63-2           | 2 mi 039° from 63-1                | 248    | <pre>1/2" gray slightly-sandy   silty clay over grayish-   buff sandy silty clay</pre> |
| 63-3           | 2 mi 039° from 63-2                | 261    | <pre>1/2" gray slightly-sandy   silty clay over grayish-   buff sandy silty clay</pre> |
| 63-5           | 4 mi 039° from 63-3                | 282    | Soft red clay  |
| 63-6           | 2 mi 039° from 63-5                | 295    | Gray silty clay  |
| 63-7           | 2 mi 039° from 63-6                | 307    | Gray silty clay  |
| 63-8           | 2 mi 039° from 63-7                | 327    | Gray silty clay  |
| 63-20          | 42°00' N., 87°00' W.               | 525    | Dark gray clay   |
| 63-21          | 42°00' N., 87°00' W.               | 525    | Dark gray clay   |
| 63-22          | 2.8 mi 015° from<br>63-21          | 527    | Dark gray clay   |
| 63-23          | 2.8 mi 015° from<br>63-22          | 508    | Dark gray clay   |
| 63 <b>-2</b> 5 | 5.6 mi 015° from<br>63-23          | 376    | Dark gray clay   |
| 63-26          | 2.1 mi 069° from<br>63-25          | 340    | Dark gray clay   |
| 63-27          | 2.1 mi 069° from<br>63-26          | 325    | Dark gray clay   |
| 63-28          | 2.1 mi 069° from<br>63-27          | 307    | Dark gray clay   |

# STUDIES ON WATER MOVEMENTS AND SEDIMENTS IN SOUTHERN LAKE MICHIGAN

Part III. Current Studies and Supplemental Sediment Studies

John C. Ayers Frank R. Bellaire

ORA Project 05466

Part III (Last Part) of the Final Report of H.E.W. Contract PH-86-63-60

GREAT LAKES RESEARCH DIVISION Special Report No. 19

INSTITUTE OF SCIENCE AND TECHNOLOGY
THE UNIVERSITY OF MICHIGAN
ANN ARBOR, MICHIGAN

July 1964



#### ERRATA, PART I OF FINAL REPORT

The section made on 24 June 1963 contained one leg which ran north-south; across this leg the transport was parallel to the sill and should not be considered as entering either basin. This transport (1208 m<sup>3</sup>/sec south) was removed in the detailed presentation on page 39, but was not subtracted in the summary on page 5. The following corrections should be made:

- p 5, line 8: substitute 2,675 for 3,883 line 10: substitute 54,971 for 56,179
- p 13, line 8 from bottom: substitute 2,700 for 3,800 and substitute 0.10 for 0.13
  - line 7 from bottom: substitute 0.11 for 0.14
  - line 6 from bottom: substitute 4182 for 3286, and substitute 4840 for 3803
  - line 3 from bottom: substitute 1/4840 for 1/3803
  - line 2 from bottom: substitute 0.00020 for 0.00026
- p 14, line 1: substitute -.00020 for -.00026 in the exponent
  - line 2: substitute -.00020 for -.00026
  - line 3: substitute 23,025 for 17,712 and 63.1 for 48.5
  - line 8: substitute 34 for 26
- p 16, line 7 from bottom: substitute 34 for 26
  line 2 from bottom: substitute "about" for "only"
- p 17, line 10: substitute 2,700 for 3,900

#### PREFACE TO THE ENTIRE REPORT

Several factors have dictated that this final report should be in separate parts.

The contract covered studies of different sorts. By the nature of the studies, the times required for work-up and analysis of data have varied widely, some parts being completed long before others could be finished. The different studies have required greatly varying amounts of ship-time and some, which required unexpectedly large amounts of ship-time, are being augmented by data obtained during cruises for other projects when vessels are in suitable regions. Finally, it is believed that assimilation by the reader is aided by brevity and unit reporting.

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#### INTRODUCTION TO PART III

This last portion of the final report on work performed under the contract includes a number of related studies carried out since the expiration of the contract. These related studies are in part studies that required more time than had been allowed under the contract; in part they are extensions of studies originally reported; and in part they are new studies not actually a part of the contract but which cover items known to be within the interest area of the USPHS Great Lakes-Illinois River Basin Project.

This report presents in final form the work done on current determination by "standard" methods at USPHS anchored buoy systems to enable cross-comparison of methods by USPHS.

It presents in final form the work done on the development and evaluation of radio-bearing current drogues as means for following currents for extended periods of time.

A limited amount of data on the annual regime of vertical temperature distribution in the waters off Chicago is included. These data were assembled and studied to ascertain whether density stratification in the local water-column was apt to result in a two-layered system in which bottom currents might be differently directed than the surface currents.

In two cases data obtained for other purposes have been suitable for crude estimates of the dilution rate inherent in the waters off Chicago.

The areal extent of the oily sediments off Gary, Indiana, (previously reported) has been determined and their probable

origin at least temporarily decided upon. A similar area off Milwaukee has been found.

A survey of the sediments of Milwaukee Embayment has been carried out with the discovery of pronounced eutrophic changes in sediment characteristics within Milwaukee Harbor. These are reported in preliminary form.

Two portions of the work originally proposed could not be carried out.

- A magnetometer could not be obtained, and the planned start on the determination of the magnetic anomalies of the southern basin of Lake Michigan could not be carried out.
- 2. Despite our best efforts we were unable to devise a current drogue that could be found after long periods and which still had so little windage effect that it would stay within the water-mass in which it was set. Consequently we were unable to achieve a study of the attrition of water masses.

Survey of the substructure of the basin of lower Lake Michigan by the sparking sub-bottom profiler was deliberately abandoned because the reduced ship-speed that it required would have used excessive amounts of ship-time. To have obtained even an incomplete sparker survey would have prevented the completion of the bottom sediment survey reported in Part II of this Final Report.

#### METHODS

Currents were determined by current drogue and by the dynamic height method of Ayers (1956) and Ayers and Bachmann (1957). Both these methods were used in part of the studies at USPHS anchored buoy systems; in others drogues alone were used.

Small citizens-band (ten-meter) radio transmitters were developed and used successfully for drogue drifts up to three days. The transmitters developed (Model ERC 127A manufactured by Electronic Research Corporation of Ann Arbor) were crystal-controlled at separate frequencies within the citizens band and emitted an unmodulated carrier transmission which was rendered audible by the beat frequency oscillator of the receiver, a Hammerlund Model HQ-180 all-band receiver. In use, the transmitters were wrapped in plastic sheet and lashed into the radar reflectors of the drogues.

Two 10-meter yagi antennae were mounted vertically on the yardarm of the ship's aftermast for reception of signals from the drogue transmitters. This antenna arrangement provided a strong lobe of reception from ahead of the ship and a weak lobe from aft; reception from abeam was almost nil. Under good conditions the drogues could be heard from about 15 miles ahead. The ship was "homed" aurally on the greatest strength of signal until radar contact was made.

Except where specifically noted, surface drogues used in these studies were influenced by the top 7-1/2 feet of the water. Except off Chicago, where depth was limited, deep

drogues were customarily set with their current drags beneath the thermocline.

Navigation during these studies was in large part by sextant fixes or radar fixes. In a few cases it was necessary to navigate by dead-reckoning.

#### RESULTS

## Current Studies

### Studies in the Chicago Region

Our studies in the Chicago region were in large part centered around 41°50.0' N, 87°30.0' W near the site of the diffuser proposed by the lakes states in the recent Chicago litigation. Their primary purpose was to provide information on the direction of currents under various winds.

<u>Drogue run, 28 April 1963 (Fig. 1)</u>: A surface drogue and a 44-foot drogue were set at 41°50.6', 87°29.5'. The deep drogue apparently went aground promptly, for it made no movement in two-plus hours. It is not shown in Figure 1.

The surface drogue moved due west a distance of 3200 feet in 2 hours 16 minutes, giving an indicated current velocity of 0.27 mph.

The wind regime of the 26th through the 28th was:

26 Apr. 10-12 knots E 27 Apr. SE AM 7 k PM NE 13 k 28 Apr. AM SE PM15 k ENE

Drogue run, 4-7 June 1963 (Fig. 2): Four radio drogues were set near the diffuser site on 4 June. During 5 June, while the ship was detained in Chicago harbor, the drogues could be heard distinctly. During the position fixing of 6 June and the recoveries on 7 June the ship homed on the drogues by radio and found them readily.

Drogues I and II were set at 0804, but drogue I (set for 43 feet in charted depths of 48 feet) did not move and was

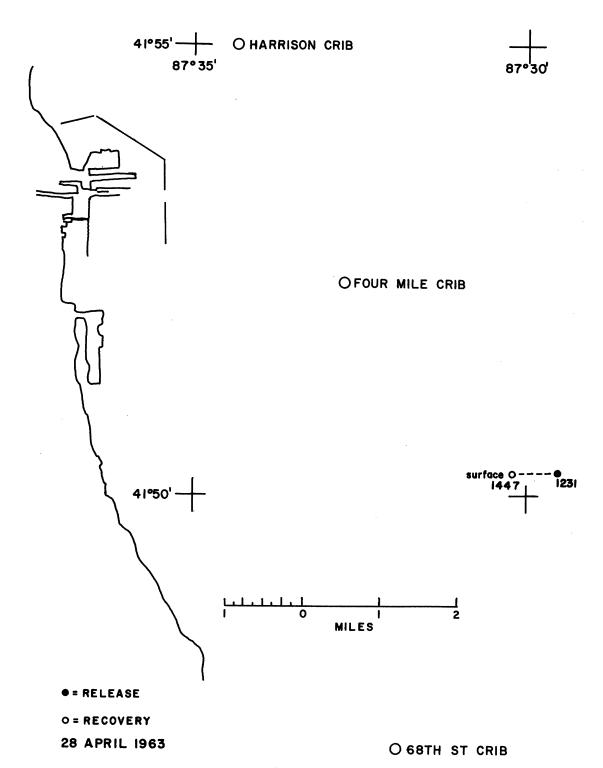


Figure 1

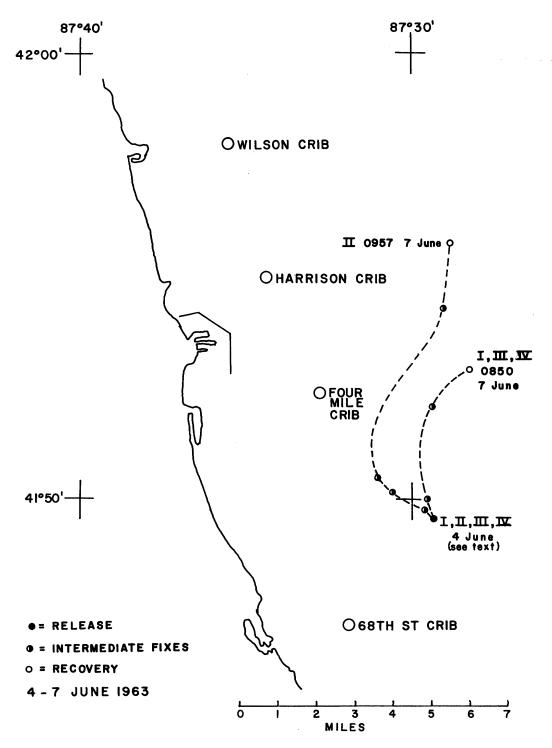


Figure 2

obviously aground from the time of setting. Drogue II (surface drogue) moved off toward the northwest immediately after setting.

At 1320 drogues III (22 feet) and IV (surface) were set alongside drogue I. Drogue I was lifted briefly, ten feet of suspension wire removed, and reset. When set at 33 feet drogue I did not go aground.

At 1320 drogues I, III, and IV were in a circle of about 50 feet diameter. At recovery on 7 June they were still together in a circle of about 200 feet diameter.

Drogue II, set earlier than the other three, maintained a separate course throughout the three days. It travelled an apparent 8.2 miles during its 73.9 hours adrift, giving an indicated speed of 0.11 mph.

Drogues I, III, and IV travelled an apparent 4.3 miles during their 67.5 hours adrift, giving an indicated speed of 0.06 mph.

The chronology of positions plotted in Figure 2 was:

```
4 June 0804 #II 41°49.6', 87°29.4' (set)

0927 #II 41°49.8', 87°29.7'

1300 #II 41°50.2', 87°30.7'

1320 #I, III, IV 41°49.6', 87°29.4' (set)

1645 #I, III, IV 41°50.0', 87°29.6'

1650 #II 41°50.4', 87°31.0'

6 June 1400 #I, III, IV 41°52.1', 87°29.4'

1432 #II 41°54.2', 87°29.0'

7 June 0850 #I, III, IV 41°52.9', 87°28.3' (recovery)
```

0957 #II 41°55.7', 87°28.8' (recovery)

The wind during this period was:

```
3 June S 4 = 8 knots

4 June NW 6 k to NE 5-12 k (W during the night)

5 June light sea breeze (W during the night)

6 June SW to SE 4 k to SW (turned N during the night)

7 June N 8-10 k
```

<u>Drogue run, 20-21 June 1963 (Fig. 3)</u>: This was a radio drogue run, carried out under severe conditions to assess the sturdiness of the drogue radio transmitters.

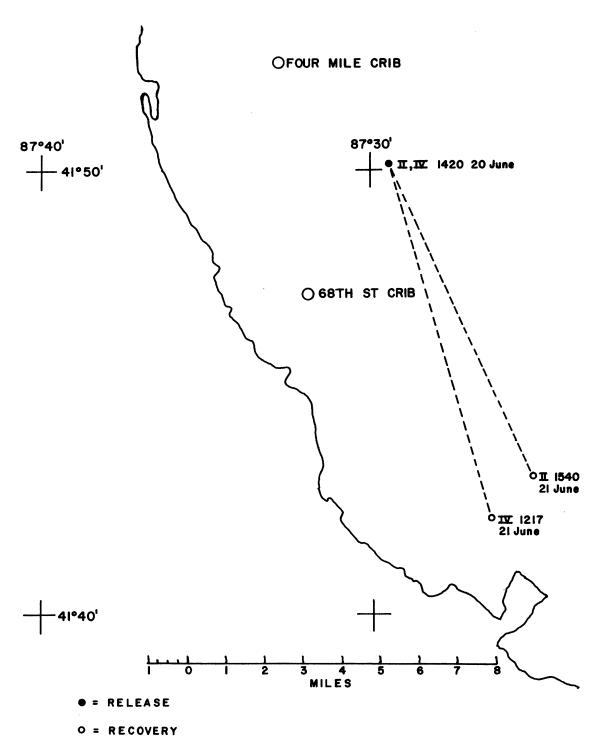
During the evening of 19 June a severe squall and frontal passage occurred at Chicago. During and after the frontal passage winds up to fifty knots were reported. During the night of the 19th the wind slowly tapered off, but large seas were built up. Wind and seas slowly moderated during the 20th and 21st.

At 1420 on 20 June two radio drogues, #II at 20 feet and #IV at the surface, were set at 41°50.1°, 87°29.5°. At the time of setting the wind was from the north at 16 knots and seas estimated to be six feet high were running.

After returning to Chicago harbor, the drogue transmitters were heard still functioning at 1620 and at 1820.

On 21 June search for the drogues was carried out under winds of 7-10 knots and in 3-4 foot seas. At this time drogue IV was transmitting a weak and fuzzy signal that was homed on with difficulty but which did lead us to the drogue. Recovery was made at 1217 just outside Indiana harbor at 41°42.2°, 87°26.3°.

Inspection of the recovered drogue showed that the transmitter's whip antenna had broken off; the transmission heard was from a stub of the antenna-feed wire.



20 - 21 JUNE 1963

Figure 3

No transmission from drogue #II was heard on 21 June. By blind hunting (sea-return rendered the radar almost useless) the drogue was found outside Indiana harbor. Recovery was made at 1540 at 41°43.0°, 87°25.2°. The antenna of this transmitter had also broken off and had pulled the feed-wire out with it.

After this day antenna break-off was prevented by taping a slender wooden block between the antenna and the drogue-staff top.

Drogue II had travelled an apparent 8.8 miles in 25.3 hours, going an indicated speed of 0.35 mph. Drogue IV travelled an apparent 9.5 miles during 21.95 hours, an indicated speed of 0.43 mph.

<u>Drogue run, 4-5 October 1963 (Fig. 4)</u>: This run was without radios; the drogues were hunted by radar and positioned by sextant fixes.

Surface drogues I, II, and III, plus drogues IV and V (both at 36 feet) were set at 41°51.2°, 87°29.0° at 1227 on 4 October.

Drogues IV and V moved 700 feet west in the interval between 1227 and 1800 when they were taken up. Drogue V showed evidences of hitting bottom (bends and gouges on the lower edge of the sheet metal drag). Drogue IV stayed with V during the entire period, but did not show evidence of hard grounding. Because grounding may have hindered the movement of these two drogues, they are considered suspect.

Drogues I, II, and III retained the same relative positions throughout the period of drift. At setting I and III were each about 50 feet from II. At 1730, when II was fixed, I and III

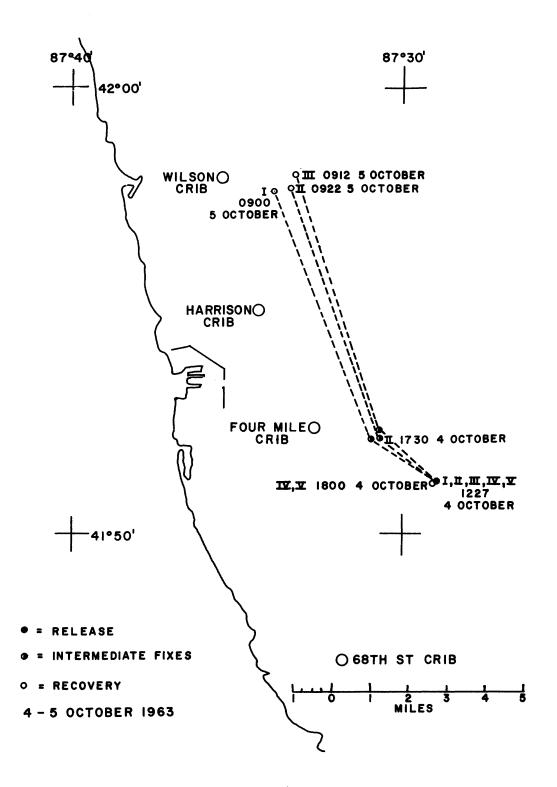


Figure 4

were estimated to be each about a quarter mile from II. At recovery on 5 October I was, by fix, 2500 feet from II and III was 2000 feet from II.

Drogue I travelled an apparent 9.2 miles during 20.55 hours—an indicated speed of 0.45 mph. Drogue II travelled an apparent 8.8 miles during 20.9 hours, for an indicated speed of 0.42 mph. Drogue III travelled an apparent 9.0 miles in 20.75 hours, giving an indicated speed of over 0.43 mph.

The chronology of fixes during this run was:

The wind regime for this run was:

```
3 Oct. NW 20 knots (on east side of lake) 4 Oct. SE 10-12 k
```

5 Oct. S 10 k (becoming 14 k later in day)

Drogue run, 9-10 October 1963 (Fig. 5): This run involved one radio drogue (IV) that was used to home the ship into radar range.

Drogues II, III, IV, and V were set at 0920 on 9 October; setting position, by radar fix, was 41°51.5', 87°29.3'. Drogues III and IV were normal surface drogues, each carrying a single sheet metal drag; drogue II carried two current drags in tandem. This configuration of drags was a test (reported later) to ascertain whether windage on the drogue floats was significant.

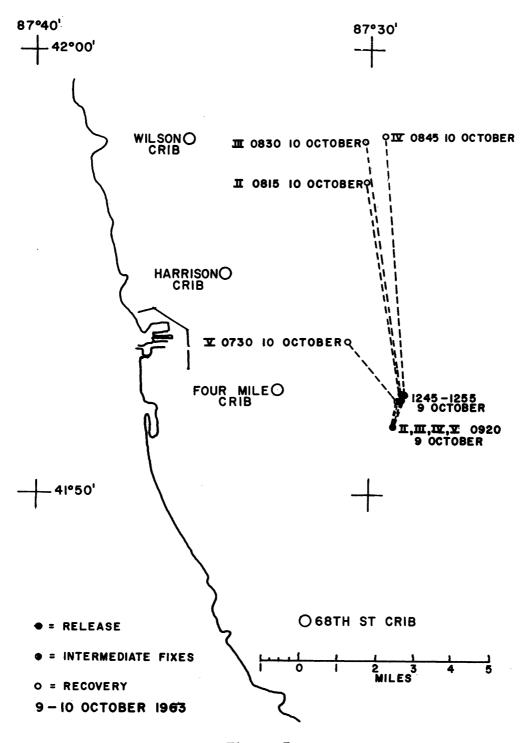


Figure 5

Drogue V was set at 36 feet; upon recovery it showed evidence of grounding. Its direction of movement and its rate of movement are suspect.

Drogues II, III, and IV retained the same relative positions during the drift. Set about 50 feet apart, the intervals between them had opened to about 1/8th mile by 1245-1255 on the 9th. At recovery IV was a half mile from III and II was a mile behind III.

Drogue II moved an apparent 6.7 miles in 22.9 hours—an indicated speed of 0.29 mph. Drogue III travelled an apparent 7.8 miles in 23.2 hours for an indicated speed of 0.34 mph. Drogue IV drifted an apparent 7.9 miles during 23.4 hours, giving an indicated speed of 0.34 mph.

The chronology of positions during this run was:

9 Oct. 0920 #II, III, IV, V 41°51.6', 87°29.3' (set, radar fix)

1245-1255 #II 41°52.2', 87°29.0' (sextant fix)

#III 41°52.3', 87°29.0' (sextant fix)

#IV 41°52.3', 87°28.9' (sextant fix)

#V 41°52.2', 87°29.2' (sextant fix)

10 Oct. 0730 #V 41°53.5', 87°30.7' (recovery, sextant fix)

0815 #II 41°57.0', 87°30.1' (recovery, sextant fix)

0830 #III 41°57.9', 87°30.2' (recovery, sextant fix)

0845 #IV 41°58.2', 87°29.6' (recovery, sextant fix)

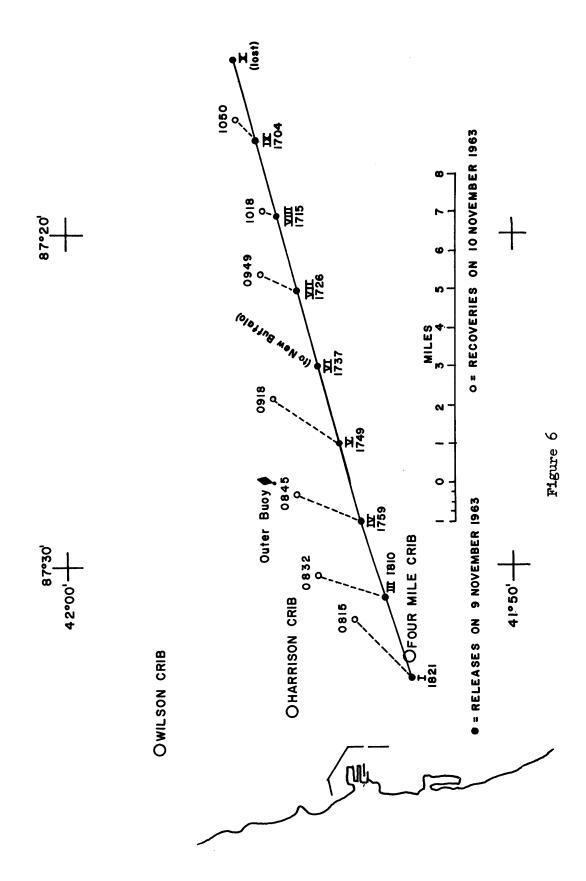
The wind regime for this run was:

8 Oct. (evening) SE 4 knots

9 Oct. SSW 6-10 k

10 Oct. (early AM) SSE 12-20 k

<u>Drogue run, 9-10 November 1963 (Fig. 6)</u>: This drogue run was carried out with all drogue floats being of low-windage



fish-net-buoy style. In this float the flotation is furnished by a series of ovo-cylindrical floats of five inches diameter. These floats are strung on the float staff until the current drag is carried but only the upper end of the uppermost plastic float extends through the water surface. The exposed portion of the uppermost float, a portion of the staff six feet long by 5/8 inch wide, and a 3/8 inch mesh wire radar corner reflector one foot in each dimension are the total of surfaces exposed to wind. Total windage exposure is 200 square inches, which is countered by an underwater exposure of 32 square feet. The new float eliminates 70 square inches of exposure to wind in comparison to the old-style float that is described under "Tests of Windage Effects on Drogues."

On 9 November a line of nine surface drogues was set as the ship approached Chicago from the east side of the lake. Drogues were set at about 2-mile intervals along a course running about 250° true from about 17 miles outside Four Mile Crib to a half mile inside the crib. All release positions involved in this run were radar fixes.

Drogue X is believed to have sunk; we find no record that it had been checked for adequacy of flotation against its current drag, and it disappeared from radar contact before the ship arrived at the position for setting drogue IX.

Drogue VI parted from its current drag (hit by steamer?). The float was found by the police of New Buffalo, Michigan, on the beach there on the morning of 2 December.

The seven drogues recovered had all moved various distances northward and their movements had various degrees of eastward

components. The greatest total movement was near the west (inshore) end of the line.

The positions of release on 9 November and recovery on 10 November, and indicated speeds of travel were:

| Drogue | Release            | Recovery            | Indicated Speed, mph |                      |  |  |  |  |  |
|--------|--------------------|---------------------|----------------------|----------------------|--|--|--|--|--|
| I      | 41°52.3', 87°33.4' | 41°53.7', 87°31.7'  | SF*                  | 0.15                 |  |  |  |  |  |
| III    | 41°52.9', 87°31.0' | 41°54.4', 87°30.3'  | SF                   | 0.13                 |  |  |  |  |  |
| IV     | 41°53.4', 87°28.7' | 41°54.8', 87°27.9'  | SF                   | 0.12                 |  |  |  |  |  |
| V      | 41°53.9', 87°26.4' | 41°55.4', 87°25.0'  | SF                   | 0.14                 |  |  |  |  |  |
| VI     | 41°54.3°, 87°24.0° | case caso caso caso |                      | 510 OUT 618 VIII     |  |  |  |  |  |
| VII    | 41°54.9', 87°21.7' | 41°55.7', 87°21.2'  | RF*                  | 0.07                 |  |  |  |  |  |
| VIII   | 41°55.3', 87°19.5' | 41°55.6', 87°19.3'  | RF                   | 0.02                 |  |  |  |  |  |
| IX     | 41°55.7', 87°17.2' | 41°56.3', 87°16.6'  | RF                   | 0.04                 |  |  |  |  |  |
| X      | 41°56.21, 87°14.81 | eas awa con one one |                      | most come about come |  |  |  |  |  |
|        | *SF = sextant fix  |                     |                      |                      |  |  |  |  |  |

\*RF = radar fix

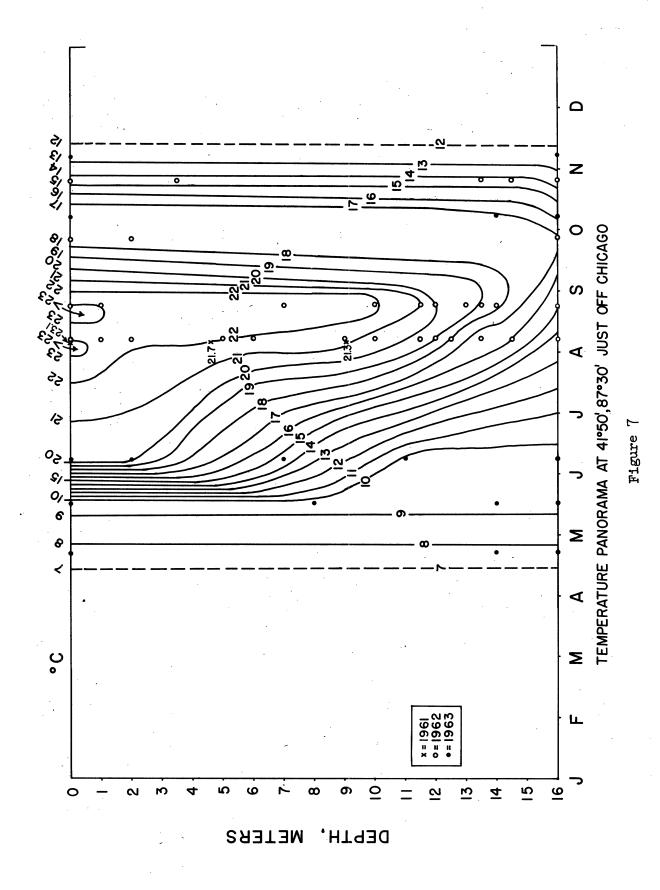
The wind regime pertaining to this run was:

18-20 knots (over east side of lake) 8 Nov. NW SSW 20 k (25 k further northeast in lake) 9 Nov. NW 10-13 k (up to recovery time) 10 Nov.

# The Panorama of Temperature off Chicago

One of the factors that could bear upon the nature of currents in the waters immediately off Chicago is the local annual regimen of temperature. Study of temperature (density) structure off Chicago in the warmer parts of the year might show whether conditions conducive to two-layered current flow would develop.

Figure 7 presents a synthesized panorama of water temperatures near 41°50', 87°30' for the months April to November.



Data from 1961 were from Chicago Outer Buoy; 1962 and 1963 data were taken at the diffuser position. The data of 1961 are reversing thermometer data; those of 1962 and 1963 are bathythermograph data. Dashed isotherms for 7° and 12° are estimates supported by data on only one side.

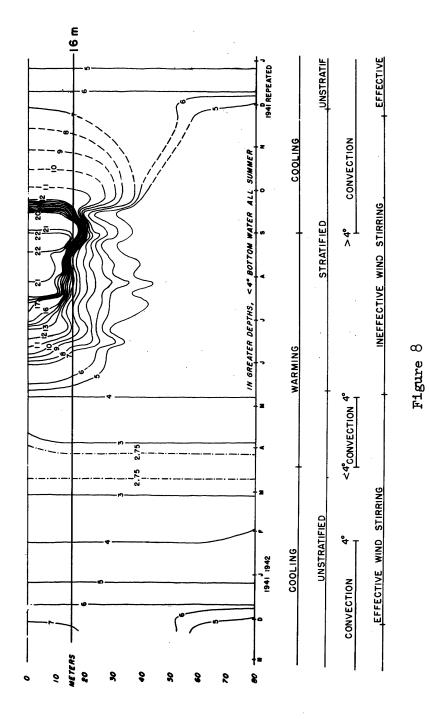
Figure 8, from Ayers (1962), has been provided to enable comparisons with deep-water conditions. A line indicating 16 meters of depth (the depth near the diffuser) has been drawn across this figure to aid in the assessment of depth as a factor in the local regimen.

As a test of the comparability of the years involved in Figures 7 and 8, (Chicago temperatures since 1960 being unavailable) we have compared the annual mean raw-water temperatures of the Milwaukee filtration plant for these years:

| 1941 | 7.06°C | 1961 | 6.06°C |
|------|--------|------|--------|
| 1942 | 6.56°C | 1962 | 6.56°C |
|      |        | 1963 | 6.78°C |

1941 and 1961 appear to have been somewhat warmer and cooler, respectively, than the other years, but 1942, 1962, and 1963 appear to be reasonably comparable. Since the latter three years comprise the bulk of both figures, comparisons between the figures seem justified.

Midsummer surface temperatures off Chicago attain higher values than those in the open lake. Both spring and fall temperatures are higher off Chicago than in midlake. More effective downward mixing of heat in spring is apparent off Chicago where the first isotherm to show a curvature indicative of developing stratification is that for 10° while in midlake the 5° isotherm develops a curvature above 16 meters, also in



May. Off Chicago the most intense thermal and density stratification occurs in late August and involves only the upper isotherms of the lake's thermocline, the rest of the thermocline being intercepted by the bottom.

The bottom water off Chicago in the period of greatest stratification is mid-thermocline water; in the absence of internal waves typical two-layered flow is unlikely at this period.

In June a two-layered water column exists temporarily while the thermocline is developing but has not yet reached bottom; this appears to be the time of year when significant directional differences between surface and bottom currents (in the absence of internal wave activity) might occur if local development of a two-layered water column were the most important factor.

Internal wave activity, by tilting the thermocline and intruding colder subsurface water into the area, can establish temporary two-layered conditions with possible differences in top and bottom current directions regardless of the condition in the undisturbed local water column.

In the absence of internal waves the general condition off Chicago appears to be that surface and bottom currents would move in more or less the same direction during nearly all the year. The movements of the few successful deeper drogues off Chicago are in agreement with this conclusion.

### Crude Estimates of Dilution off Chicago

While the drogue runs off Chicago were intended primarily

to give additional information as to the direction of current movement under different wind conditions, it has been possible to derive two crude estimates of the dilution rate inherent in the currents off Chicago. These estimates include error due to the windage effect on the drogue floats and are not considered to do more than indicate an order of magnitude.

The water off Chicago is relatively shallow and the bottom has but a gentle slope. The surface drogues of 4-5 October and of 9-10 October moved in relatively constant mean depths of 40 and 50 feet respectively.

If the two surface drogues farthest apart on these two occasions (Figs. 4 and 5) are considered to move along near the edges of an hypothetical plume of effluent originating at the bottom at the release position and extending upward through the water column, successive tentative cross-sectional areas of the plume can be computed.

Assuming that the progressive increases in cross-sectional area of the plumes are due to entrainment of diluting water from the environment, dilution can be expressed as ratios of plume cross-sectional areas at successive pairs of times. In constant depths the shape of the plume cross-section need not be known.

In the following, the width of the plume at the bottom at the origin is taken to be ten feet; its width at the surface at the origin is taken to be fifty feet (the distance apart of the drogues at setting). In the successive cross-sections the 5:1 ratio of plume width at surface to plume width at bottom is maintained (assumption of uniform dilution along the vertical

of the water column).

For the run of 4-5 October the separations of drogues I and III were: 50 feet at setting, and (by scaling from Fig. 4) 5/16 mile at 1730 on 4 October, and 7/10 mile at 0900-0912 on 5 October.

Keeping a five-to-one ratio of plume widths in constant mean depth of 40 feet, the successive plume cross-sectional areas are:  $1200 \text{ ft}^2$ ,  $39600 \text{ ft}^2$ , and  $88700 \text{ ft}^2$ . The successive ratios are: 39600/1200 or 33X and 88700/39600 or 2.2X. Crude estimate of total indicated dilution during the run:  $33 \times 2.2$  or about 73X.

For the run of 9-10 October the distances apart of drogues III and IV were: 50 feet at setting, and (by scaling from Fig. 5) 1/8 mile at 1245-1255 on 9 October, and 1/2 mile at 0830-0845 on 10 October. With a five-to-one ratio of plume widths and in constant mean depth of 50 feet, the plume cross-section areas are: 1500 ft<sup>2</sup>, 19800 ft<sup>2</sup>, and 79200 ft<sup>2</sup>. The successive ratios of areas are: 19800/1500 or 13.2X and 79200/19800 or 4X. Crude estimate of total indicated dilution during the run: 13.2 x 4 or 52.8X.

Whether the plume cross-sections are considered to be rectangles of equal surface and bottom widths, as trapezoids of unequal surface and bottom widths, or as triangles with observed surface widths and zero bottom widths makes no difference; the same ratios of cross-sectional areas emerge.

Though crude, the indicated dilutions of less than 100X in a day mean a limited ability of the local currents to dilute introduced materials.

## Studies at USPHS Buoy 14

ET and drogue run, 26 October 1963 (Figs. 9 and 10): On 26 October three drogues were set within a hundred yards of Buoy 14. Drogue I (130 feet) was set about 100 feet 075° true from the buoy; drogue II (tandem double drag, 0-12 feet) was set about 200 feet from the buoy on the same course; and drogue III (surface) was set about 300 feet from the buoy on the same course. The drogues were set (with the ship drifting rapidly) between 1220 and 1222; 1221 was accepted as the setting time of all three.

At recovery the drogues were all on a line bearing 018° true from the buoy. Recovery positions indicated are the positions of the drogues during a timed run along the line of their positions. After this run the ship returned and retrieved the drogues.

Drogue I had travelled an apparent 0.46 miles in 2 hours 39 minutes, giving an indicated speed of 0.17 mph for the current at 126-130 feet. Drogue II had moved an apparent 1.12 miles in 2 hours 35 minutes, indicating a speed of 0.43 mph. Drogue III covered an apparent 1.36 miles in 2 hours 34 minutes to indicate a velocity of 0.52 mph.

During the approach to the buoy, and after setting the drogues, the ship carried out a series of bathythermograph soundings on a course 098° true from a point 16 miles west of Buoy 14 to a point 12 miles east of the buoy. Figure 10 presents the components of current normal to the ship's course, as determined by dynamic heights computation. The curve for current components in the upper ten meters coincides with that for surface components over much of the figure; no attempt has

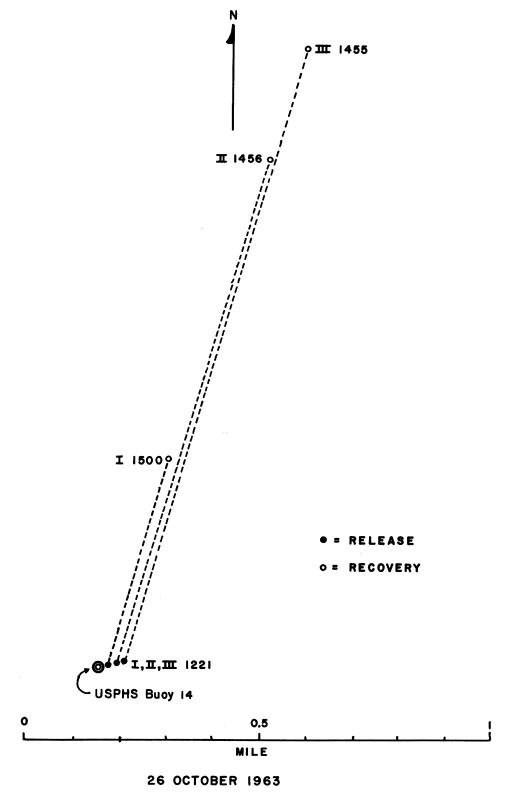
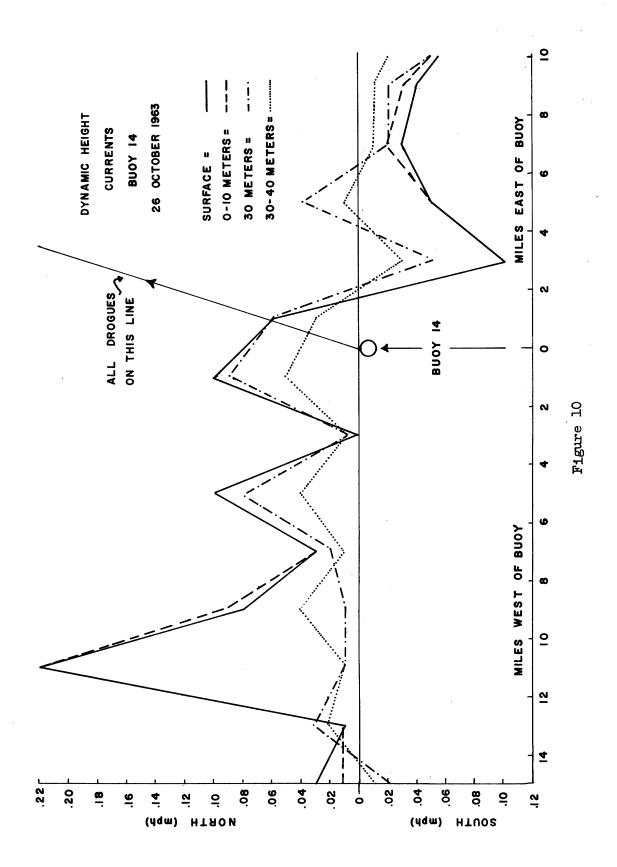


Figure 9



been made to indicate the superimposed portions.

Computed current direction changed from northward to south-ward about two miles east of the buoy. Major southward current was indicated between two and four miles east of the buoy. Major northward current was indicated to lie between 10 and 12 miles west of the buoy.

Current directions by dynamic height computation and by drogues were in agreement. Current velocity obtained by dynamic computation was 0.6 to 0.7 that given by the drogues.

The wind regime for this run was:

25 Oct. SSW 8-12 knots 26 Oct. S 13 k

## Studies off Milwaukee

Drogue run, 24 October 1963, near USPHS Buoy 17 (Fig. 11):
On 24 October a surface drogue (IV) and a deep drogue (I, 70 feet) were set at 0923 and at 1040, respectively, near the position of USPHS Buoy 17. Positions were by sextant fix.

Drogue IV travelled an apparent 5.6 miles in 8 hours 25 minutes for an indicated speed of 0.67 mph.

Drogue I moved an apparent 2.8 miles during 7 hours 36 minutes, giving an indicated velocity of 0.37 mph at the 66-70 foot level.

The chronology of positions during this run was:

0923 #IV 43°07.6', 87°50.5' (set)

1040 #I 43°07.8', 87°50.7' (set)

1140 #IV 43°08.9', 87°51.0'

1748 #IV 43°12.1', 87°52.4' (recovery)

1816 #I 43°10.0', 87°51.5' (recovery)

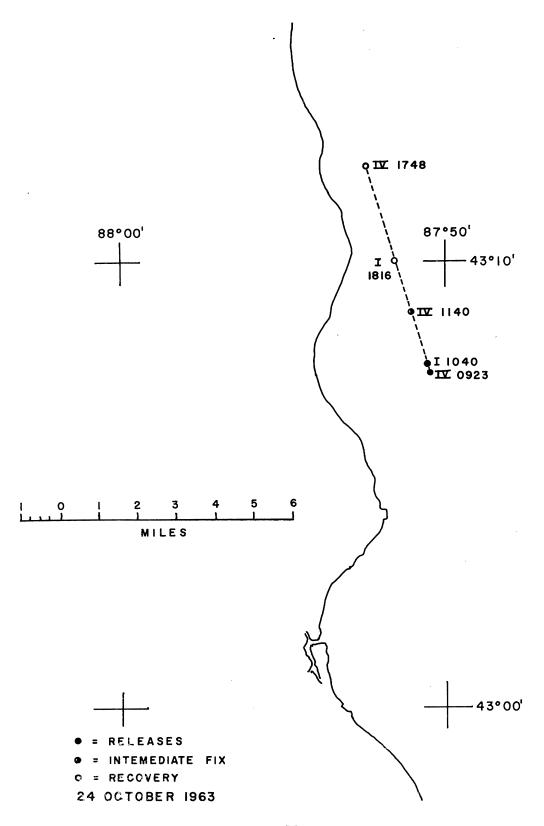


Figure 11

The wind regime related to this run was:

23 Oct. S 12 knots (diminishing during night) 24 Oct. S 9-12 k (18 k later in the day)

Drogue run, 24-25 October 1963, near USPHS Buoy 18 (Fig. 12):
On 24 October surface drogue V was set at 1253 about halfway
between USPHS buoys 17 and 18, and surface drogue III at Buoy 18
at 1400. The drogues were recovered on 25 October. During
this run positions were obtained by a combination of dead
reckoning and radar range and bearings on Buoy 18.

Drogue V drifted an apparent 5.4 miles during the 23 hours 37 minutes it was adrift, to give an indicated surface current velocity of 0.23 mph. Drogue III moved 4.8 miles in 21 hours 27 minutes, an indicated velocity of 0.22 mph.

The time-series of positions during this run was:

24 Oct. 1253 #V 43°07.9', 87°36.2' (set)

1400 #III 43°08.0', 87°24.4' (set, at Buoy 18)

25 Oct. 1127 #III 43°11.3', 87°21.0' (recovery)

43°09.5', 87°30.1'

(recovery)

The wind regime applicable to this run was:

23 Oct. S 12 knots (diminishing during night)

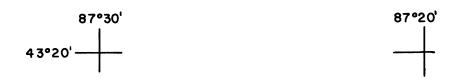
24 Oct. S 9-18 k

25 Oct. SSW 8-12 k

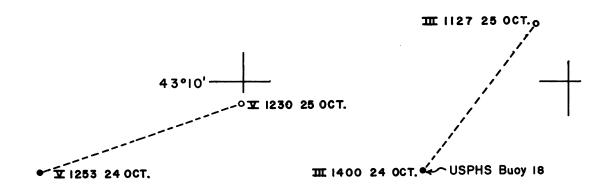
# Studies off Grand Haven and Muskegon

1230 #V

<u>Drogue run, 24-25 June 1963 (Fig. 13)</u>: This run was designed to be a further test of the radio-drogue as well as a test of the relative directions of deep and surface currents off Grand Haven. Fresh batteries had not been put in the transmitters, with the result that the transmitters ran down. Fortunately, a blind radio-call to the entire east side of the



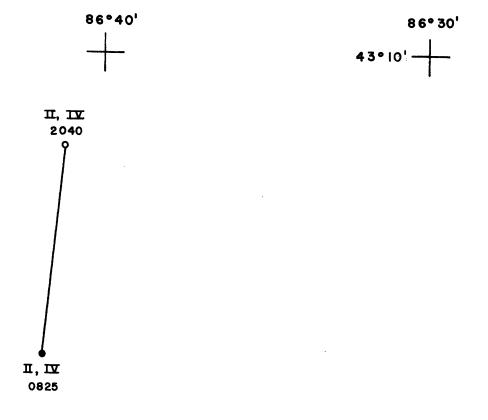


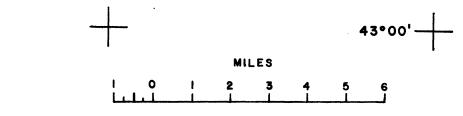


• = RELEASES ON 24 OCTOBER 1963

o = RECOVERIES ON 25 OCTOBER 1963

Figure 12





• = RELEASES ON 24 JUNE 1963 O = RECOVERIES ON 25 JUNE 1963

Figure 13

lake elicited the information that the MILWAUKEE CLIPPER had seen the drogues; from her directions we were able to recover them. Positions were by radar fix.

Drogues II (surface) and IV (125 feet) were set at 43°03.3', 86°41.8', 22.3 miles west of Grand Haven at 0825 on 24 June. On 25 June the two, still together, were recovered at 2040 at 43°07.9', 86°41.2' 18 miles 252° true from Muskegon. There was no separation of these drogues during their 36 hours 15 minutes adrift. They had travelled an apparent 5.4 miles, giving an indicated current speed at both depths of 0.15 mph.

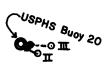
The wind regime for this run was:

24 June SSE 4-8 knots 25 June SE 6-8 k (going calm in afternoon)

Drogue run, 27-28 October 1963, at USPHS Buoy 20 and Weather Tower (Fig. 14): On 27 October surface drogue I was set alongside the USWB-USLS-USPHS-UM weather tower off Mona Lake inlet at 0934. Deep drogue II (130 feet) and surface drogue III were set beside USPHS Buoy 20 at 1059 and 1104 respectively. Recovery positions of II and III were by timed run to Buoy 20; positioning of I was by sextant fix.

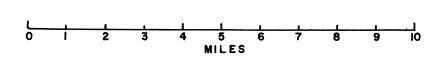
Drogue II was recovered at 1350 after moving 0.34 mile toward 098° true--an indicated speed of 0.12 mph. Drogue III was retrieved at 1355 after moving 0.58 mile toward 074° true at an indicated speed of 0.20 mph.

Drogue I was positioned at 1640 at a point 1.6 miles 164° true from the tower, having moved at an indicated speed of 0.23 mph. This drogue was left adrift overnight and was



I 0934 27 OCTOBER

1620 27th



86030' 43000'

86.50,

- = RELEASE
- = INTERMEDIATE FIX
- O = RECOVERY

27 - 28 OCTOBER 1963

I 1401 28 OCTOBER 0

Figure 14

recovered on 28 October at 1401 at 42°55.3°, 86°14.5°, about two miles 317° true from the channel at Port Sheldon. From release to recovery this drogue moved 16.8 miles in 28 hours 27 minutes for an overall indicated speed of 0.59 mph. Between the intermediate and final positions this drogue moved 15.2 miles at an indicated rate of 0.7 mph.

The regime of winds applicable to this run was:

26 Oct. SSW 8-12 knots

27 Oct. S 8-13 k

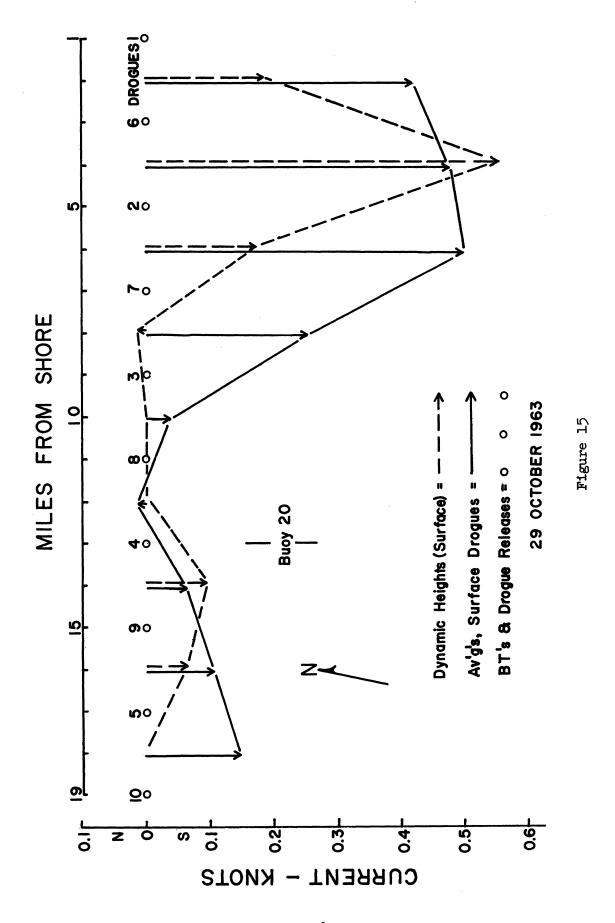
28 Oct. NW 18-23 k

BT and drogue run, 29 October 1963, at USPHS Buoy 20 (Fig. 15): This section presents a comparison of currents obtained by dynamic computation to currents indicated by surface drogues. The drogue run has been reported previously in Part I of this Final Report.

To enable comparison to the computed currents, the normal components of the movements of adjacent drogues have been averaged and the average plotted between the drogue positions.

The comparison is hampered by the fact that higher-windage floats had to be used on half the drogues. The averaging process included a higher-windage drogue in each pair. The comparison would have been further facilitated if the bathythermograph soundings had been in between the drogues. Each computed current component would then have been directly comparable to the normal component of the movement of a single drogue.

While the mechanics of the comparisons leave a good deal to be desired, there was at least directional agreement in five of the nine comparisons. In three of the four remaining



comparisons movements of drogues were paired with no-current indicated by dynamic heights. In only one of the nine was there direct disagreement in direction between the computed current and that indicated by drogue. In five of the nine comparisons current velocity indicated by the two methods was in order-of-magnitude agreement.

The comparison was carried out under north winds of 10-18 knots which began during the early forenoon and continued through the day. Winds of the 28th had been northwest 18-23 knots.

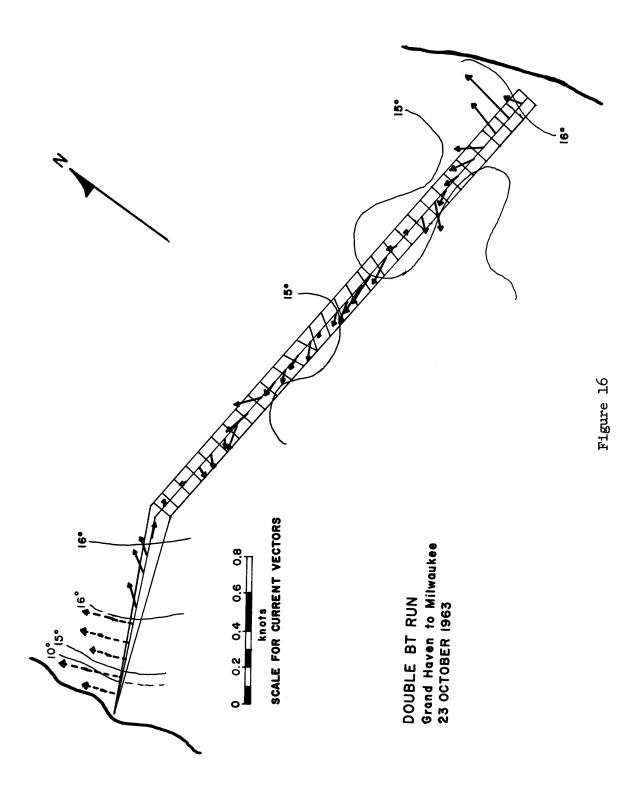
# Double BT Run, Grand Haven to Milwaukee (Fig. 16)

On 23 October 1963 the vessels INLAND SEAS and MYSIS carried out what was supposed to be a parallel run of bathy-thermograph soundings between Grand Haven and Milwaukee.

Inexperience with such runs is credited with the boats' steering north of the course, and then converging after course-correction. Corrective measures have been taken.

Figure 16 presents the results of this run. The two outer lines represent the paths of the two ships. Cross-lines intersect the two ships' courses at the points where BT soundings were taken. The center line connects the middle-points of the "squares" which have BT soundings on each corner.

Current directions and velocities have been determined by application of the dynamic height method: 1) along the track of each ship, and 2) transversely to the ships' tracks along the short cross-lines. Components of current: 1) normal to the ships' tracks, and 2) parallel to the ships' tracks were thus



obtained. Mean components were computed from the mean slopes of the surface; slopes along the ships' tracks being averaged and slopes transverse to the tracks being averaged. The two components thus obtained for each "square" were summed vectorially to produce the current vector that is drawn from the midpoint of each "square."

Isotherms of 15° and 16°C are entered in the figure in the places where they were encountered by the two ships.

In the last ten miles of the short converging leg of the crossing, only the current components normal to the ships tracks were computed. The averages of these are shown as dashed arrows.

The wind regime under which these crossings were made was:

22 Oct. S 20-25 knots

23 Oct. S 12 k (diminishing during night)

Although the 2-mile spacing between the ships! tracks is too small to delineate clearly the nature of the current structure, it is sufficient to suggest that eddies of different sizes and of both right-hand and left-hand rotation were present and probably moving within an overall drift. Single transects across such a structure would produce the appearance of "streaks" of oppositely directed current as reported in Part I.

# Tests of Windage Effects on Drogues

Test of 9-10 October 1963 (Old Floats, Old Drags): The old-style drogue floats consisted of a styrafoam float 16-1/2 inches square and six inches deep. Through the center of the styrafoam there was a 10-foot aluminum pipe of 5/8th inch

outside diameter. This pipe (staff) extended 6-1/2 feet above the top of the styrafoam and three feet below it. The lower end of the aluminum staff was weighted with three one-pound iron fish-net sinkers, and four guy-wires ran from the bottom of the staff through the corners of the styrafoam to 15 inches from the top of the staff. At the top of the staff was mounted a wire-mesh radar corner reflector measuring one foot in each dimension.

In the usual use these floats exposed to the wind the radar reflector, the upper portion of the staff, the guy wires, a rope bridle for recovery, and one side of the styrafoam float  $(16-1/2 \times 4 \text{ inches exposed})$ . Total area exposed to the effects of wind was 270 square inches.

Figure 5 presents the details of this test. Drogues III and IV were normal surface drogues; each carried at the lower end of its staff a 4-foot x 8-foot sheet of galvanized iron rolled and bolted into an open-ended cylinder and suspended by a light chain bridle. These drogues were influenced by the upper 7-1/2 feet of water. Drogue II carried two current drags (cylinders) in tandem and was effected by the upper 12 feet of water. The tandem drag configuration was used on the assumption that windage on the float would not be able to tow it to any significant degree.

As shown in Figure 5, drogues II, III, and IV retained about the same relative positions to each other from the "noon" fixes of the 9th until recovery on the morning of the 10th.

Drogue II travelled 6.7 miles during its total period adrift; this gives an apparent mean speed of 0.29 mph. Drogues

III and IV both moved at apparent mean speeds of 0.34 mph.

If the difference in indicated speeds is taken to be the result of windage on the drogue float, then the windage errors are 0.05/0.29 or 17.5%.

Test of 26 October 1963 (Old Floats, Old Drags): In this test drogue II again carried two current drags in tandem and was compared to drogue III, a surface drogue.

Drogue II travelled at an indicated speed of 0.43 mph; drogue III moved at an indicated speed of 0.52 mph.

Again taking the difference in indicated speeds as a measure of the towing effect of wind pressure on the drogue float, we have 0.09/0.43 or 20.9% windage error.

#### NOTE

The indicated speeds of drogues that are given in the preceding sections have not been corrected in any way for windage error.

#### Supplemental Sediment Studies

# Oily Sediments off Gary, Indiana

In May 1964 the areal extent of the oily sediments off Gary, Indiana, which were reported in Part II of this Final Report, was worked out in detail by R/V MYSIS.

Figure 17 gives the extent of these sediments. They occupy an area about four miles long by about 1-1/2 miles wide oriented in a northwest-southeast direction and lying to the east and south of Buoy R2 off Gary.

These sediments are primarily of oily silty sand. They do not show any continuation to the shore. The nature of these sediments is very similar to that of sediments collected from a known spoil-dumping area off Milwaukee at 42°59.5', 87°47.0'.

We now believe that the sediments off Gary are also spoil (dredgings) from harbor dredging operations along the southern end of the lake. As spoil, these sediments represent a manmade modification of the lake environment but not one that can be attributed to the eutrophication process in the sense in which that term is usually used.

### Foul-Odored Sediments off Calumet Harbor

In May 1964, also, the MYSIS made a detailed search for the foul-odored sediments which had previously been found off Calumet Harbor, and which were reported in Part II.

No evidence of these foul-odored sediments was found. The condition that was present during the bottom survey reported in Part II was, then, a temporary condition for which no cause can be given.







Figure 17

### Milwaukee Embayment Survey

In June 1964 the R/V INLAND SEAS carried out a detailed sediment survey in the embayment on which the city of Milwaukee is located.

In no part of the embayment outside of the seawall was there any physical evidence of eutrophic modification of bottom sediments.

The effluent from the Milwaukee sewage disposal plant is dumped directly into Milwaukee harbor, inside the seawall, by an outfall at the east end of the disposal plant property. The sediments behind the seawall from North Entrance to South Entrance and Shore Park Breakwater Light (USLS Chart No. 743) are all black; all are heavily organic; and all appear rich in worms.

Behind the seawall the water is discolored and turbid. Its uncorrected conductivity values run 30 to 50 percent higher than those of water outside the seawall. Water in the vicinity of the outfall is nearly black and smells of hydrogen sulphide. Streams of discolored high-conductivity water blow downwind out through the openings in the seawall and can be traced visually for considerable distances into the open lake.

Limitations of draft prevented the INLAND SEAS from exploring the sediments and water behind the seawall south of Shore Park Breakwater Light.

### CONCLUSIONS

Local currents in the shallow waters off Chicago appear to move essentially in downwind directions. This was also true for the one run of drogues at USPHS Buoy 14 in midlake off Racine, for the one run near the position of USPHS Buoy 17, and for two runs off Grand Haven.

Local currents between USPHS Buoys 17 and 18 and at USPHS Buoy 18 (only one run each) appeared to contain direction components transverse to the wind direction.

Local currents at USPHS Buoy 20 usually were not directed downwind. It is believed that set-up and other effects of shore and nearby sloping bottom were in part responsible.

The annual regimen of temperature (density) in the waters off Chicago indicates that a typical two-layered water column is not apt to occur there. In the absence of temporary two-layered conditions caused by internal wave activity, surface and bottom currents off Chicago may be expected to move in more or less the same directions.

The general tendency for downwind movement of currents off Chicago, and one case of observed westward current under onshore wind, are taken to indicate that effluents from the proposed diffuser would be able to reach the intakes and beaches of Chicago under onshore winds.

Crude estimates of apparent dilution in the waters off
Chicago indicate that the region is one of poor inherent ability
to dilute introduced materials.

Definite eutrophic change in the nature of bottom sediments

exists in Milwaukee harbor where sewage effluent is discharged behind the seawall. Except in harbors, there now appears to be no place in lower Lake Michigan where typical eutrophic modification of bottom sediments is taking place.

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